# FOOTING DESIGN CALCULATIONS FOR 9'-0" SPAN X 4'-8" RISE CONTECH ALUMINUM BOX STRUCTURE AT

12<sup>TH</sup> STREET CULVERT REPLACEMENT

SPALDING COUNTY
GEORGIA

**JUNE 12, 2017** 

SUBMITTED BY:

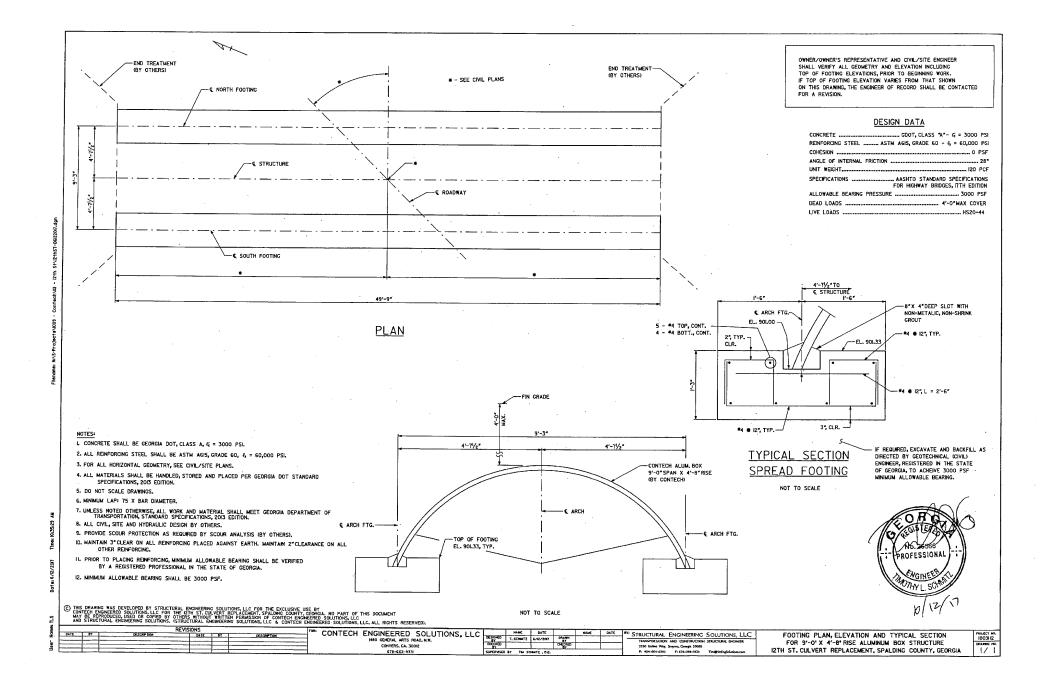
CONTECH ENGINEERED SOLUTIONS, LLC 1480 GENERAL ARTS ROAD, NW.

CONYERS, GA 30012

BY:

STRUCTURAL ENGINEERING SOLUTIONS, LLC 3260 ISOLINE WAY SMYRNA, GA 30080





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# STRUCTURAL ENGINEERING SOLUTIONS, LLC

A TRANSPORTATION AND CONSTRUCTION STRUCTURAL ENGINEER

SHEET \_\_\_\_\_\_OF \_\_\_\_
PROJECT NO .\_\_\_\_\_DATE \_\_\_\_

PROJECT\_ 12m of Alum Box SUBJECT: DES TO S Снк DRM = 9'SPAN + 4-5" RISE Awnia. Box 903.70 & RUADMAY BLEV. -901-00 STRUCTURE - 4,67 3-11 => VS & AFT HT. OF LOVER

# STRUCTURAL ENGINEERING SOLUTIONS, LLC

Project	12 St - Spalding County	Computed	tis	Date	6/9/2017
Subject	Alum Box Culvert	Checked		Date	
Task	20' x 6.33' with 3' cover	Sheet		Of	

## **BOX CULVERT FOOTING DESIGN**

GIVEN: Span Rise Max Cover Arch Area Angle Unit Wt Max All Bearing =	9.0 ft 4.67 ft 4.0 ft 35.0 ft^2 5.0 deg 120.0 pcf - soil 3.0 ksf	3.66582	6 < AASHTO 12.8.4.4	<b>1</b> 17th edi		
Pu = DL + LL						
C =	3.7 klf		Shear Check b= Key = d = fc = phi*Vc =	12 in 4 in 8 in 3000 psi 8939 lbs	OV.	
Ring Compression	n:		Vu =	2383 lbs	OK	
C = Vertical = Horizontal =	3.7 klf 3.7 klf 0.3 klf					
Footing						
Self Wt Arch =	0.3 klf					
C total = C + self w	eight of plate arch		Sliding Check			
Ctotal =	4.0 klf		Angle of inclination Coefficient of friction		5.0 degrees 0.4	
Footing Width =	1.3 ft	Min 3 feet wide	Angle of int friction		30 degrees	
Use W =	3.00 ft		Horiz Comp of C Vert Comp of C		0.3 klf 4.0 klf	
Ftg Thickness = Footing Weight =	1.25 ft 0.56 klf		Weight of Fill Weight of Footing K <sub>p</sub>		0.8 klf 0.6 klf 3.0	
Eccentricity	0.0 ft					
Weight of Fill	0.8 klf	0.589847	Slip Force Factored Slip Force		0.3 klf 0.5 klf	(1.5 factor)
Total Load	5.3 klf		•	oivo)	2.1 klf	(1.0 100101)
F act =	1.77 ksf		Soil Resistance (pass Frictional Resistance Total Resistance		2.1 klf 2.1 klf 4.2 klf	
Bending =	P/8 * (L/2)		F " 014.0			
Use = Mu =	2.0 kf/f 2.0 kf/f 2.6 kf/f		Footing OK ? ====>	0	ιK	
Use	4 @	12.0 inches	TRANS			

#4 @ 13.3 in Long Reinforcing

Project 12	St - Spalding County	Computed	tls	Date	6/9/2017
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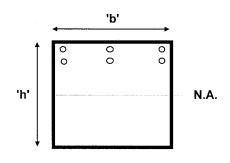
# Concrete Design of a Plate Arch Strip Footing

#### **SPREADSHEET ASSUMPTIONS & LIMITATIONS**

- 1. Reinforced concrete design in accordance with AASHTO 1996.
- 2. No more than three (3) rows of steel with equal amounts of steel in each row can be used.
- 3. Spreadsheet currently does not handle torsion, minor axis bending, side steel, or shear friction.

## **INPUT PARAMETERS**

#### **SECTION & MATERIAL PROPERTIES:**



Shear	Critical Se	ction	Flexure (	Critical Section	n
Dim 'b'	12	in	Dim 'b'	12	in
Dim 'h'	15	in	Dim 'h'	15	in

Distance from tension face to center of Layer #1 3.50 in Distance from center of layer #1 to center of layer #2 0.00 in Distance from center of layer #2 to center of layer #3 in

Concrete:

Rebar:

$$f'_{c} = 3000$$
  
 $f_{y} = 60$ 

psi ksi

#### FLEXURAL REINFORCEMENT:

Flexural Bar Size, # 4 ====>

0.2 in²/ bar 0.50 in diameter

No. of flexural bars 1.0

1 <== # of bars required by flexural analysis

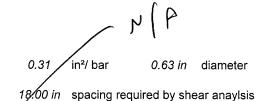
1 or 2 rows?

Are bars bundled? (YES/NO) no

#### SHEAR REINFORCEMENT:

Stirrup Bar Size, # =====> No. of legs <====

1



#### MOMENT & SHEAR:

About Neutral Axis

Factored Moment, Mu= 3.34 kip-ft Factored Shear, Vu= kips

Service Moment, Ms= 2.00 kip-ft Job No.

#REF!

No

4

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#### **FLEXURAL DESIGN**

**AASHTO 8.16.3** 

$$M_u \leq \phi M_n$$

$$M_u = 3$$
 kip-ft

#### Solve for required amount of flexural reinforcement.

Assuming 1 row(s) with no bundled bars, and for b = 12 inches and h = 15 inches

let d = 15 inches less 3.5 inches clear to upper layer

AASHTO 8.17.1 requires the reinforcement provided be adequate to develop a moment at least 1.2 × the cracking moment. This requirement is waived if the reinforcement provided at a section is at least one-third greater than that required by analysis, based on Load Combinations.

1.2 
$$M_{cr} = 1.2 \times 7.5 \text{ sqrt } f_c \times (bh^3 / 12) / (h / 2)$$
  
= 18 Kip-ft

$$\phi M_n = \phi A_s f_y (d - a / 2), \emptyset = 0.90$$
  
= 3.34 kip-ft

using the quadratic equation, [-b  $\pm$  sqrt (b<sup>2</sup> - 4ac)]/2a, solve for A<sub>s</sub>:

$$1.2M_{cr} = \phi A_s f_y (d - a/2)$$
, where  $\phi = 0.90$ 

$$a = 52.9E+3 As^2$$

$$b = -621.0E + 3 A_s$$

$$c = 221.8E+3$$
 kip-in

reinforcement, 
$$A_s = 0.37$$
 in<sup>2</sup>

$$\phi M_n = \phi A_s f_y (d - a/2)$$
, where  $\phi = 0.90$ 

$$a = 52.9E+3 A_s^2$$

$$b = -621.0E+3 A_s$$

$$c = 40.1E + 3 in - k$$

reinforcement, 
$$A_s = 0.06$$
 in<sup>2</sup>

the required minimum amount of steel reinforcement is

(Using 1.33 Design Moment)

the amount of steel reinforcement provided is 0.20 in

 $A_s$  provided >=  $A_s$  required, therefore **OK** 

#### Verify Moment Capacity for A s provided

$$\varphi M_{\text{n}}$$
 =  $\varphi$  As fy ( d - a / 2 ), where  $\varphi$  = 0.90

$$a = Asfy = 0.39 in$$

$$0.85F'cb$$

$$\phi M_n = 10$$
 kip-ft

$$\phi M_n >= Mu$$
, therefore  $OK$ 

#### Balanced Reinforcement Ratio

**AASHTO 8.16.3.2.2** 

$$\rho_b = \frac{0.85 b_1 t'c}{fy} \frac{(87000)}{(87000 + fy)} = 0.0214$$
  $b_1 = 0.85$  for 4000 psi concrete

$$\rho_{provided}\text{=}\phantom{-}0.0014$$
 <= 0.0160 = 0.75  $\rho_{b}$ 

Job No.

#REF!

No.

5

Project	12 St - Spalding County	Computed	tls	Date	6/9/2017
Subject	t Alum Box Culvert	Checked		Date	
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#### **FLEXURAL DESIGN (continued)**

**AASHTO 8.16.3** 

#### Distribution of Flexural Reinforcement

**AASHTO 8.16.8.4** 

in²

For 1 - #4 bars in 1 row(s) with no bundled bars, reinforcement,  $A_s = 0.20$ 

f<sub>s</sub>= stress in reinforcement at service load, ksi

$$f_s = z$$
 <=0.6fy z<= 130 kips/in for severe exposure

$$M_s$$
= service load moment = 2 kip-ft

$$E_c$$
= 3122 ksi  $E_s$ = 29000 ksi

Modular Ratio, n= 
$$\frac{E_s}{E_c}$$
 = 9.29

$$m = n As = 0.0135$$

$$k = (m^2 + 2m)^{1/2} - m = 0.151$$

$$j = 1 - 1/3 k = 0.949667$$

$$f_s = \frac{M_s}{A_s \ j \ d}$$
 = 10.99 ksi <= 0.6fy = 36.00 ksi

d<sub>c</sub>= distance measured from extreme tension fiber to centroid of closest bar.

d<sub>c</sub>= 2.25 in, For calculation purposes, cover shall be taken as less than 2"

A= effective tension area, in square inches, of concrete surrounding the flexural tension reinforcement and having the same centroid as that reinforcement, divided by the number of bars.

$$z=f_s(d_cA)^{1/3}=$$
 54.3 Note: The quantity 'z' is less than the allowable value of 170 kip/in

Job No. #REF!

6/

Project 12 St - Spalding County	Computed tls	Date 6/9/2017
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#### **SHEAR DESIGN**

**AASHTO 8.16.6** 

$$V_u \le \phi V_n \quad \phi = 0.85$$

$$V_n = V_c + V_s$$

$$V_u = 1.0$$
 kips

#### Solve for required amount of shear strength, Vs

Assuming 1 row(s) with no bundled bars, and bw = 12 inches and h = 15 inches.

let d =15 inches less 3.5 inches to upper layer

$$V_c = 2 \text{ sqrt (f'c) b}_w \text{ d} = 15.1 \text{ kips}$$

$$V_s = \underbrace{Vu - fVc}_{f} <= 8 \text{ sqrt (f'c)} 60.5 \text{ kips}$$

$$V_s = \underbrace{0.0 \text{ kips}}_{f} <= 8 \text{ sqrt (f'c) bw d}$$
OK

Shear strength Vs is less than 4 sqrt(fc) bw d, spacing shall not exceed maximum spacing shown below.

### Solve for required stirrup spacing

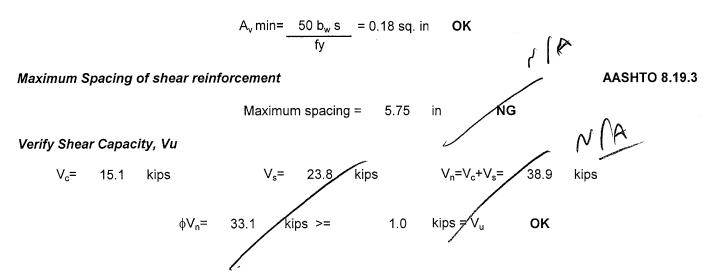
A<sub>v</sub>= area of shear reinforcement within a distance 's'.

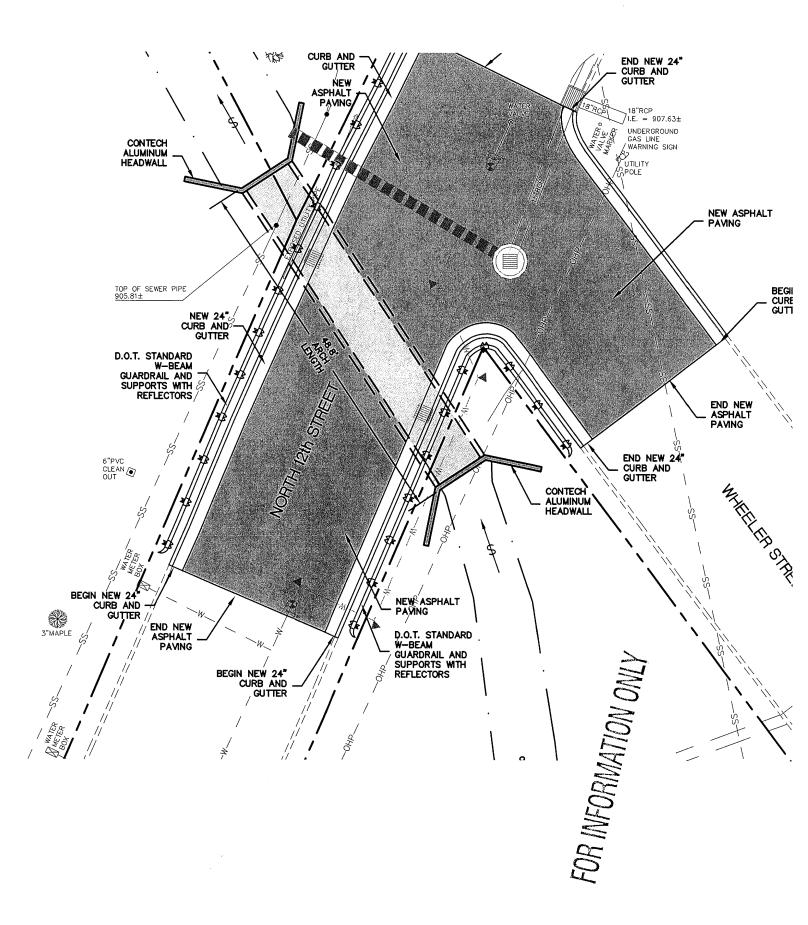
$$A_v$$
= 0.62 assuming 2 legs #5 stirrups  
 $s = Av fy d$  = 18 inch spacing

Therefore, use 2 legs #5 stirrups at 18 inch spacing

#### Minimum of shear reinforcement

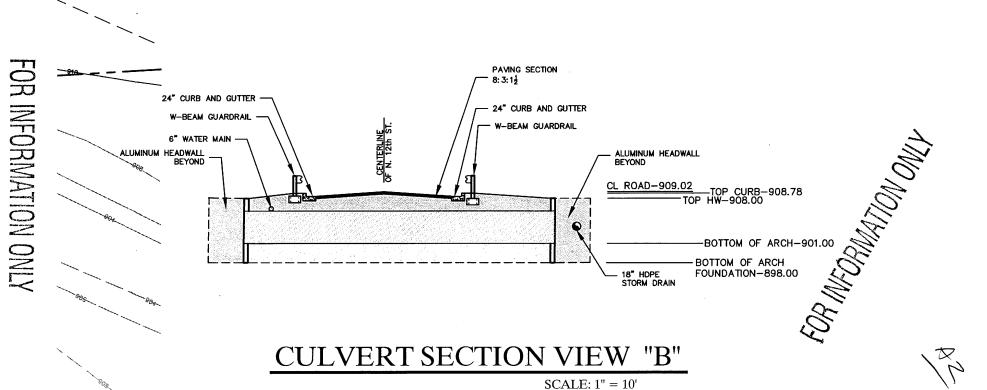
**AASHTO 8.1.2** 

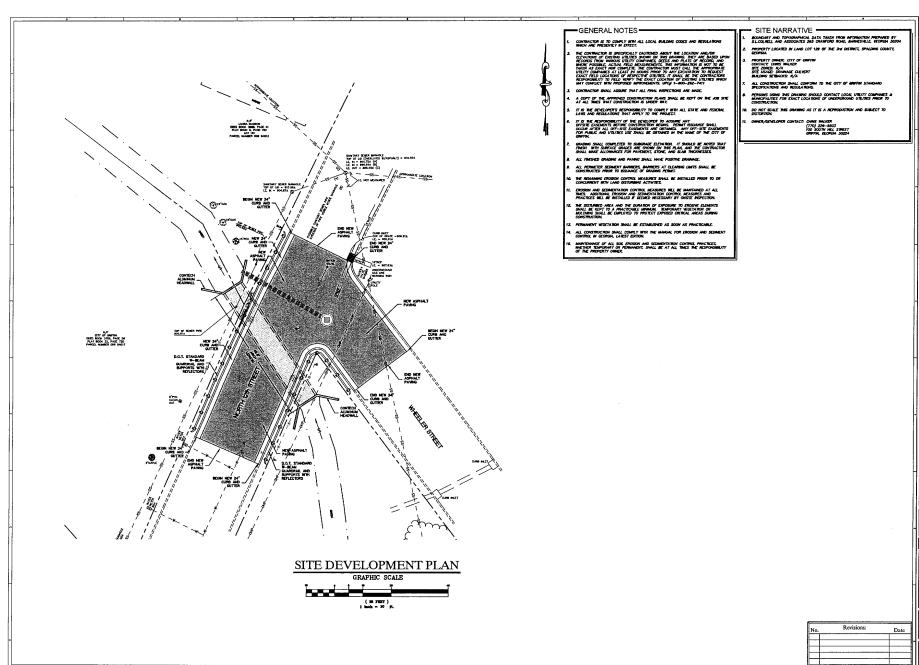




# **CULVERT SECTION VIEW "A"**

SCALE: 1'' = 10'





PARAG CONSULTING

/ERT

12th STREET CULVERT REPLACEMENT

client acknowledges that these downwests the work papers of Europea Consulting up, los, and nor their instruments a customal service.

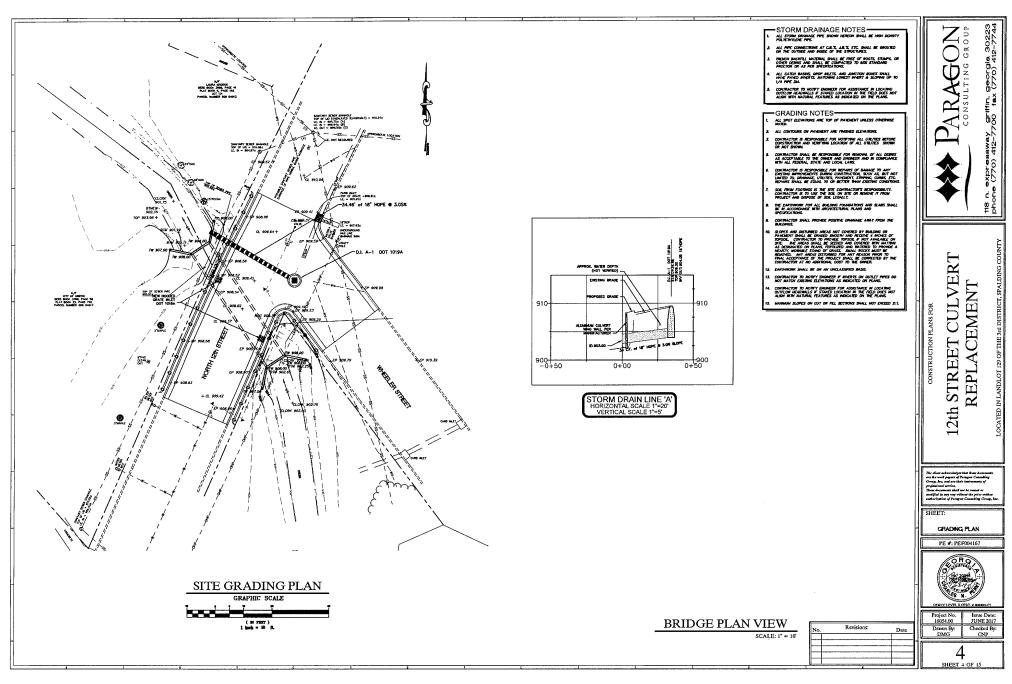
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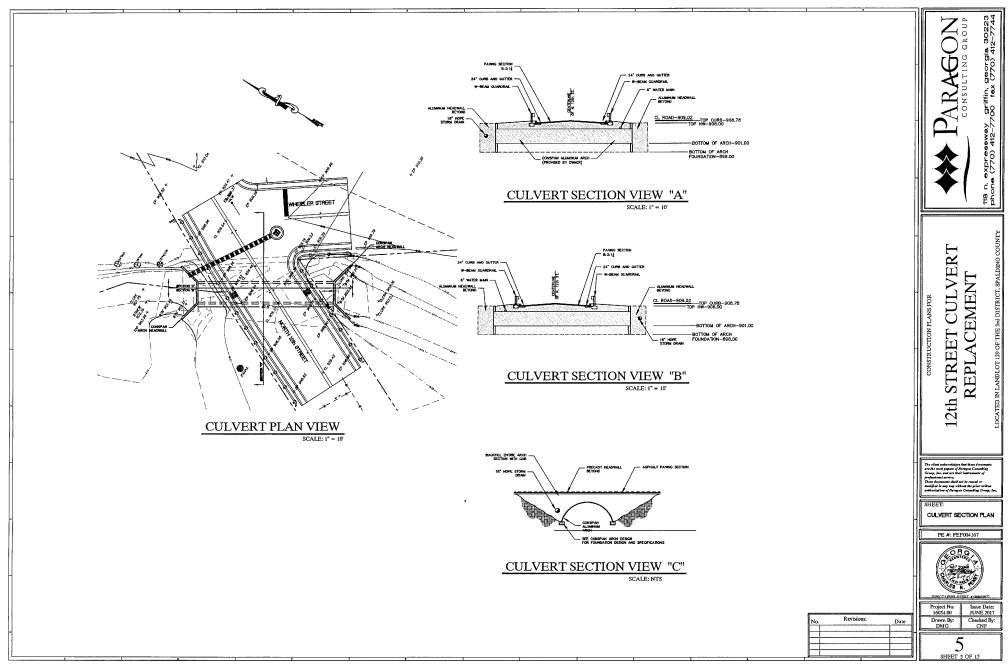
GILTER



Project No.	Issue Date:
16054.00	JUNE 2017
Drawn By:	Checked By:
DMG	CNP

3 SHEET 3 OF 15





# CONSTRUCTION MATERIALS SERVICES, INC.

105 Park 42 Drive Suite A; Locust Grove, GA 30248-2545

Phone: (770) 914-1744 Fax: (770) 914-0412

Email: info@cmsnatl.com

Geotechnical Engineering - Materials Testing - Asphalt Mix Design - Soil Surveys - Environmental

November 28, 2016

Mr. Charles Penny Paragon Consulting Group 118 North Expressway Griffin, Georgia 30223-2050

RE: Preliminary Geotechnical Subsurface Investigation 12<sup>th</sup> St. Wheeler Rd. Culvert CMS # 16-189

#### Dear Mr. Penny:

Construction Materials Services, Inc. (CMS) has completed a preliminary geotechnical study for the above subject project. All borings were located in the field by our personnel. A boring location sketch is attached which indicates the approximate location of our test borings. If needed, we recommend our boring locations be confirmed by your surveyor and placed on the final site plan. As part of this study, two (2) borings were made at the selected test locations. Rock, in the form of auger refusal, was encountered at two (2) locations at the depths drilled as indicated below:

Boring Location	Depth to Rock from Existing Surface (ft)	Attempted Depth of Boring from Surface (ft)
B-1	12.5	15.0
B-2*	6.5/ 5.0	15.0

<sup>\*</sup>Two attempts made at this location

Immediate ground water table (GWT) was not measured in each boring. The ground water elevation can be expected to fluctuate with the season of the year, the surrounding ground surface conditions, subsurface conditions, and recent rainfall amounts. Thus, ground water elevations should be considered valid only for the date of observation.

Basic boring logs have been prepared and are attached which provide a visual classification of the soils encountered during this study.

Due to the shallow presence of rock at this site, we recommend that the foundation be extended to and keyed into the encountered rock formations. If you desire, we can prepare your foundation design.

However, at this time, we recommend additional testing which will include rock coring to determine in situ rock quality.

If additional information, sampling, and/or testing is required, once final site plan is established and approved, please contact us.

Qualifications of Our Findings: The recommendations offered in this report are based on our interpretation of the data obtained from our investigation. It should be noted soil conditions may vary from boring to boring and in areas where borings were not made. With this in mind, we recommend site preparation and foundation construction be closely monitored. If the soil conditions deviate from those presented in this report, we will be glad to furnish any additional analysis and/or recommendations that may be needed.

This report was made to determine the geotechnical properties of the site and is not intended to serve as a wetland survey or an environmental site assessment. No effort has been made to delineate or designate any area as wetlands or an area of environmental concern or contamination. Any reference to low areas, poorly drained areas, etc. is related to geotechnical applications. Any recommendations regarding drainage and earthwork are made on the basis that such work can be permitted and performed in accordance with current laws pertaining to wetlands, storm water runoff, and environmental contamination.

If you have any questions, please contact me at (770) 914-1744.

Respectfully submitted.

Andrew Johnson, P. E.

President

Construction Materials Services, Inc.

AJ:au

Attachment

Borehole #: 1 NBL (35' South of Culvert)

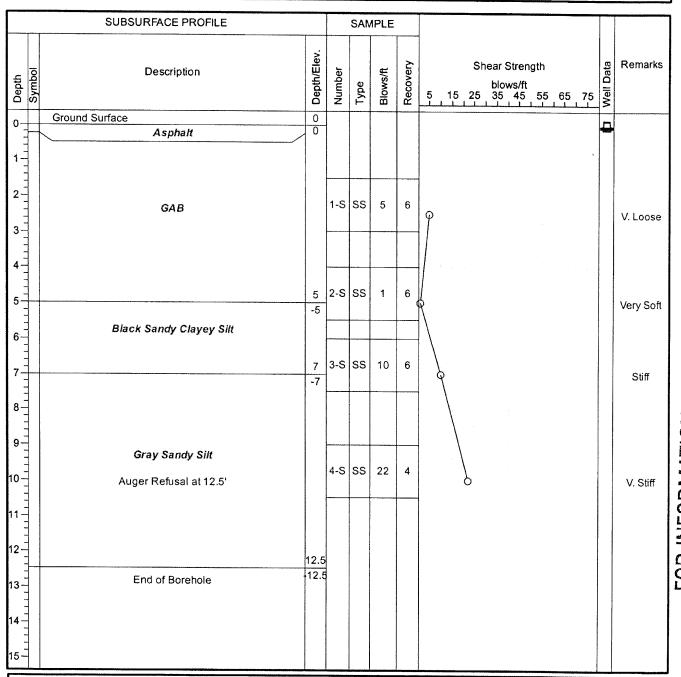
Project: 12th Street / Wheeler Road Culvert

Client: Paragon Consulting

Location: Griffin, Spalding County, Georgia

**Enclosure:** 

Engineer: Andrew Johnson



Drilled By: PS, JP, CW

Drill Method: 4" Auger

Drill Date: 11/21/16

Construction Materials Services, Inc. 105 Park 42 Drive, Suite A Locust Grove, GA 30248-2545 Hole Size: 4"

Datum:

Sheet: 1 of 1

Borehole #: 2 SBL (2 Attempts)

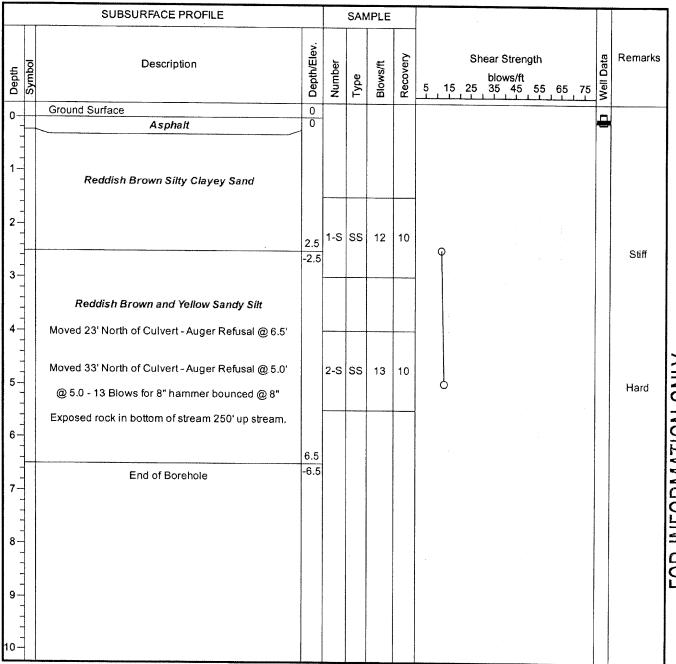
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Engineer: Andrew Johnson



Drilled By: PS, JP, CW

Drill Method: 4" Auger

Drill Date: 11/21/16

Construction Materials Services, Inc. 105 Park 42 Drive, Suite A Locust Grove, GA 30248-2545

Datum:

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Sheet: 1 of 1

Hole Size: 4"