

# DUDA WATER STORAGE IMPROVEMENTS (WSI) FINAL GEOTECHNICAL REPORT

Wood Project #600550X04 Date: June 2020



#### DUDA WATER STORAGE IMPROVEMENTS (WSI) FINAL GEOTECHNICAL REPORT

**Prepared for:** 



St. Johns River Water Management District (SJRWMD) Palatka, Florida

#### Prepared by

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Wood Project No. 600550x04

June 30, 2020





**Engineering Certification** 

I hereby certify that I am a registered professional engineer in the State of Florida practicing with Wood Environment & Solutions, Inc., 1101 Channelside Drive, Suite 200, Tampa, FL 33602, a corporation authorized to operate as a business providing engineering consulting services (5392) by the State of Florida Department of Professional Regulation, Board of Engineers. I further certify that I, or others under my direct supervision, have prepared the geotechnical engineering evaluations, findings, opinions, calculations, conclusions or technical advice hereby represented in this report.

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Report Title:St. Johns River Water Management DistrictDuda Water Storage Improvements (WSI) FINAL Geotechnical Report

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#### 1.0 INTRODUCTION

The Duda Water Storage Improvements (WSI) Project will be located on Duda Property which has approximately 2,900 acres, and is located at the boundaries between Lake County, and Orange County, and north of Lake Apopka, as shown in **Figure 1**. In October of 2018, Wood prepared a preliminary geotechnical investigation for pumps, structure and levee improvements. According to information provided by the St. Johns River Water Management District (Owner), for this final report, Wood Environment & Infrastructure Solutions (Wood) understands that there are plans to install 15-inch to 48-inch aluminum culvert pipes (ACP), berm plugs, risers, walkways and slide gate structures on the site. The locations of these proposed structures are presented in **Figure 2**.

Wood was tasked with performing a subsurface geotechnical exploration for the proposed site development and structures. The results of this geotechnical exploration were used to develop geotechnical recommendations for the construction of the proposed culverts, berm plug, sumps and walkways.

The field works were completed on February 27<sup>th</sup>, 2020, and included the following:

- Coordinating an underground utility locate.
- Performing five (5) Standard Penetration Test (SPT) borings in general accordance with ASTM D 1586. The depth of the borings varied between 40 feet and 50 feet. At each boring the top 5 feet were sampled using hand augers, between 5 feet and 15 feet the soils were sampled continuously, and thereafter, at 5-foot intervals. These borings were labeled as "2020-SPT-X".
- Collecting piston tube samples at two locations within Lake Level Canal. These piston tubes were labeled as "2020-PT-X".
- Classifying the soil types in accordance with the United Soil Classification System (USCS) designations (ASTM D 2487).
- Preparing this report including figures, boring logs, seasonal high groundwater level determination, laboratory test results and recommendations.

#### 2.0 PROJECT SITE CHARACTERISTICS

#### 2.1 Lake County and Orange County Soil Survey

Soils data from the Soil Survey of the site produced by the United States Department of Agriculture Natural Resource Conservation Service (USDA-NRCS) were reviewed as part of the exploration. The soil units identified within the project area are described below:

• Gator Muck, frequently ponded, 0 to 1 percent slopes (map symbol 18), are very poorly



drained soils with depressions on marine terraces. The soil unit consists of muck on the top 18 inches, then sandy clay loams between 18 and 55 inches below surfaces and fine sands up to 80 inches below surface. The water table is between 0 and 6 inches below surface. The available water storage capacity is very high, and permeability is moderately low to moderately high, ranging from 0.06 to 0.20 in/hr.

- Everglades Muck, depressional (map symbol 27), are very poorly drained soils with depressions on marine terraces. The soil unit consists of muck on the top 11 inches, then mucky peat up to 80 inches below surface. The water table is at the ground surface. The available water storage capacity is very high, and permeability is high, ranging from 2 to 6 in/hr.
- Wauchula Sand (map symbol 49), are poorly drained soils with rises on marine terraces. The soil unit consists of sands up to a depth of 38 inches below surface, then sandy clay loams up to a depth of 80 inches below surface. The water table is between 6 and 18 inches below ground surface. The available water storage capacity is moderately, and permeability is moderately high to high, ranging from 0.6 to 2 in/hr.

The proposed structures at Duda Property will be installed on Gator muck and Everglades muck.

These USDA-NRCS classifications are based on their interpretation of aerial photographs and widely spaced hand auger borings. Borders between mapping units are approximate, and the transition between soil types may be gradual. Areas of dissimilar soils can occur within a mapped unit. However, the soil survey provides a reasonable basis for an initial evaluation of surficial soil conditions in the area and can provide an indication of changes that may have occurred due to land filling, excavation, and other activities at the site. The soil survey information for the site is presented in **Appendix A**.

#### 2.2 Geology

The Lake Apopka site is located on the western boundary of Orange County and the eastern boundary of Lake County, west of the town of Apopka, Florida. Local geology near the project site is characterized by surface and near-surface sediments consisting of quartz sand, clay, and limestone, ranging in age from late Eocene to Holocene. The first recognizeable lithostratigraphic unit occuring below these near-surface sediments is the Cypresshead Formation, of the Pliocene age. The Cypresshead Formation can reach thicknesses of up to 200 feet, and is composed of very fine to very coarse grained clean to clayey sands.

Underlying the Cypresshead Formation is the Hawthorn Group, Coosawhatchie Formation of the Miocene age. The Coosawhatchie Formation is characterized by poorly consolidated clayey and phosphatic sand, silty clay, and occasional dolostone and limestone.

Underlying the Hawthorn Group, Coosawhatchie Formation is the Ocala Limestone of the Eocene age. The limestone formations of the Ocala Group reach thicknesses of 90-150 feet, and



primarily consist of white, to cream, to dark brown, granular to chalky, fossiliferous, poorly to well indurated limestone and dolomite, known for its very high permeability (USGS, 2018). The regional geology of both Orange County and Lake County in the general vicinity of Lake Apopka is presented below in **Table 1.** Some of the stratigraphic units can be missing in some areas.

Geologic Age	Stratigraphic Unit	Approximate Thickness (ft)	General Lithologic Character (starting from land surface)
Holocene (Recent)	Holocene Sediments	0-5	Quartz sands, carbonate sands and muds, and organics.
Pleistocene/ Holocene	Undifferentiated Sediments	0-100	Fine to coarse sands with silts, clay, and marl.
Pleistocene/ Holocene	Beach Ridge and Dunes	0-20	Fine to medium grained quartz sand.
Pleistocene/ Pliocene	Shelly Sediments	0-20	Quartz sands, clayey sands, sandy clays, limestone, fossiliferous.
Pleistocene/ Holocene	Reworked Cypresshead Sediments	0-20	Fine to coarse grained quartz sands with gravel and clay.
Pliocene	Cypresshead Formation	100-200	Very fine to very coarse grained clean to clayey sands.
Miocene	Hawthorn Group, Coosawhatchie Formation	0-50	Clayey sands, phosphatic sands, silty clays, dolostone, limestone.
Eocene	Ocala Limestone	100	Porous, marine limestone, soft, granular to chalky, highly fossiliferous.

#### **TABLE 1 - Generalized Stratigraphic Units**

#### 3.0 SUBSURFACE EXPLORATIONS

#### 3.1 Standard Penetration Test Borings

Five Standard Penetration Test (SPT) borings were performed in general accordance with ASTM D 1586 (Standard Test Method for Standard Penetration Test). The field work was completed on February 27, 2020. The locations of the SPT borings are shown in **Figure 2**. These 2020 borings were labeled as "2020-SPT-X" whereas the 2018 borings were labeled as "2018-SPT-X". The soils encountered in the borings were visually classified and logged in the field in accordance with ASTM D 2488. Groundwater levels, at the end of drilling each boring, were recorded. Representative portions of the samples were transported to Wood's materials testing laboratory in Jacksonville, Florida for further classification and testing. The logs were then updated based upon the results of the laboratory classification tests (see **Section 4.0**), using the Unified Soil Classification System (USCS) in accordance with ASTM D 2487.



The subsurface conditions encountered in the SPT borings are presented on the soil boring logs in **Appendix B.** At the same time, **Appendix B** includes the borings performed in 2018. The boring logs represent our interpretation of the subsurface conditions encountered in the field and the visual examination of field samples by our technical staff. The lines designating the interfaces between various strata on the boring logs represent the approximate interface locations. Actual transitions between strata may be gradual. All the water levels shown in the logs represent the conditions at the time of our exploration. On completion, the boring locations were surveyed to determine the coordinates using a handheld Garmin GPS 72H model with a horizontal accuracy of +/- 2 feet. The ground surface elevations were obtained based on the "St. Johns River Water Management District, Upper Ocklawaha River Basin, Lake Apopka Duda Water Storage Improvements, 60% drawings".

The 2020 SPT borings were performed by AmDrill, Inc., of Brooksville, Florida. The drilling was completed using a truck mounted drill rig. The SPT borings were conducted in general accordance with ASTM D 1586 using mud-rotary drilling methods and advanced to depths between 40 and 50 feet. At each location, the top 5 feet were completed using hand augers to avoid possible shallow utilities. Between 5 and 15 feet the SPT were conducted continuously and thereafter at 5 feet intervals. Soil samples were collected from the borings using a 1.5-inch inner diameter split-spoon sampler driven with an automatic 140-pound slide hammer falling a distance of 30-inches. The soils from the recovered split spoon samples were logged. Four SPT borings (2020-SPT-1 to 2020-SPT-4) were advanced to a depth of 40 feet, and 2020-SPT-5 was advanced to a depth of 50 feet. At the end of drilling each borehole was backfilled with the remaining auger cuttings and plugged with bentonite chips.

#### 3.2 Piston Tube Sampling

Piston tube sampling was completed on Lake Level Canal at 2 locations as shown on **Figure 2**. The piston tube sampling works were performed on February 27th, 2020 by a Wood field crew. The piston tube samples were collected from a 16-foot long Jon Boat.

The piston tube sampler is comprised of a stainless steel thin-walled, 2-inch diameter by 18-inch long sampling tube with 5-foot long threaded rod extensions. The sampler is advanced by hand and typically cannot penetrate a relatively dense muck or sand layer given the diameter and length of the sampling tube. All samples were placed into sealed jars and labeled with sample identification numbers and depths.

Upon completion, the boring locations were surveyed to determine the as-built coordinates using a handheld Garmin GPS 72H model with a horizontal accuracy of +/- 2 feet. The ground surface elevations were obtained based on the "St. Johns River Water Management District, Upper Ocklawaha River Basin, Lake Apopka Duda Water Storage Improvements, 60% drawings".

Table 2 includes a list of the Standard Penetration Tests and Piston Tubes performed at the



#### Duda Area.

Boring / Piston Tube ID	Date	Northing (ft) <sup>(1)(2)</sup>	Easting (ft) <sup>(1)(2)</sup>	Ground Elevation (ft) <sup>(3)(6)</sup>	Boring Termination Depth (ft, bgs) <sup>(5)</sup>
2018 - SPT - 1	9/24/2018	1586255.4	440013.2	+64.0	20
2018 - SPT - 2	9/24/2018	1586255.2	441985.0	+64.0	25
2018 - SPT - 3	9/24/2018	1586082.6	442291.9	+64.0	20
2018 - SPT - 4	9/24/2018	1586292.7	442427.7	+68.0	20
2018 - SPT - 5	9/24/2018	1586170.8	442763.7	+63.5	25
2018 - SPT - 6	9/24/2018	1586219.4	447804.0	+63.5	20
2018 - SPT - 7	9/24/2018	1587097.4	452900.7	+67.7	20
2018 - SPT - 8	9/24/2018	1587087.4	452721.7	+67.0	20
2020 - SPT - 1	02/25/2020	1584070.0	438097.9	+64.0	40
2020 - SPT - 2	02/25/2020	1585074.1	437990.4	+68.0	40
2020 - SPT - 3	02/26/2020	1586275.5	442248.9	+63.5	40
2020 - SPT - 4	02/27/2020	1586239.1	442241.6	+63.5	40
2020 - SPT - 5	02/27/2020	1586247.9	452626.0	+67.0	50
2020 - PT – 1	02/27/2020	1586297.9	452763.5	+56.0 (4)	2.0 (5)
2020 - PT - 2	02/27/2020	1586171.7	452766.6	+56.0 (4)	0.7 (5)

# TABLE 2 - Summary of SPT Borings (2018 and 2020) and Piston Tubes at the DudaProperty

Notes:

(1) Coordinates were measured using a Garmin GPS 72H model.

(2) Coordinates are referenced to the US State Plane, Florida East Zone (901).

(3) Ground surface elevations are referenced to vertical datum NAVD88 and were estimated from "St. Johns River Water Management District, Upper Ocklawaha River Basin, Lake Apopka Duda Water Storage Improvements, 60% drawings".

- (4) Refers to bottom of canal elevation.
- (5) Below bottom of canal.

(6) For the 2018 borings, Ground surface elevations are referenced to vertical datum NAVD88 and were estimated using the LIDAR.

#### 4.0 LABORATORY TESTING

The soil samples collected during the subsurface exploration program were taken to Wood's materials laboratory in Jacksonville, Florida. Selected samples were tested for natural Moisture Content (ASTM D 2216), percent of material finer than the #200 sieve (ASTM D1140), Atterberg limits (ASTM D 4318), and Organic Content (ASTM D 2974). Soils were classified in general accordance with ASTM D 2487. Laboratory test results are presented in **Appendix C**. **Appendix C** also presents the laboratory test results of the 2018 borings. The laboratory test results are generally consistent with field descriptions. Detailed discussion of the strata is presented in



#### Section 5.

#### 5.0 SUBSURFACE CONDITIONS

Based on the findings of the investigation and laboratory testing, five generalized strata were identified within the project site. **Appendix B** shows the boring logs along the existing berms. The strata are distinguished by soil characteristics, typically grain size, cohesion, plasticity and organic content. These units, in descending order from ground surface, are described in the following:

Stratum 1	FILL: SAND (SP) to Clayey Sand (SC) to Silty SAND (SM) to Sandy Clay (CL) to SAND with clay (SP-SC) to SAND with silt (SP-SM) with rock fragments, dark brown to brown to light brown to light greenish gray .
Stratum 2	Organic Sandy Silt (OL) to Silty Sand (SM), dark brown to brown, spongy, fibrous, less than 30% fibers.
Stratum 3	SAND (SP) to Clayey SAND (SC) to SAND with clay (SP-SC), light gray to light greenish gray to light brown to brown.
Stratum 4	Sandy Clay (CL to CH), light greenish to greenish gray to white.
Stratum 5	Sand with Silt (SP-SM) light gray to light brown to brown.

*Stratum 1* consists of variable fill material to depths of up to approximately 3 feet below ground surface. This stratum was encountered in all the SPT borings and consisted of dark brown to brown to light brown to light greenish gray sands, clayey sands, silty sands, sandy clays and sands with clays with rock fragments. This stratum presented moisture contents between 12% and 28% and fines content between 20% and 72%.

*Stratum 2* consists of dark brown to brown organic sandy silts (OL) to silty sands (SM). The stratum was identified as very soft, spongy, with less than 30% fibers, varying in color from dark brown to brown. The stratum was observed between 2 and 11 feet below the ground surface. This organic stratum was typically encountered underneath stratum 1, varying in thickness from 6 to 9 feet. The organic contents ranged between 7% and 91%. This stratum is interpreted to be the top of the original natural ground surface.

*Stratum 3* consists of very loose to medium dense sands light gray to light greenish gray to light brown to brown clayey sands and sands with clays. This layer varied in thickness from 2 to 14 feet, extending to depths of up to 50 feet below ground surface. The moisture content ranged from 20% to 51%, fines content ranged between 4% and 31%, and organic contents varied between 2 and 17%.

*Stratum 4* is composed of soft to firm light greenish to greenish gray to white sandy clays (CL and CH), underlain typically by strata 2 and 3. This layer extends from 9 to 17 feet, below ground



surface, varying in thickness from 2 to 6 feet. Moisture content was 33%, fines content 79%, and plasticity index varied between 63 and 149.

*Stratum 5* is composed of light gray to light brown to brown sand with silts (SP-SM). This stratum was encountered at 13 feet below ground surface, varying in thickness between 10 and 13 feet. The consistencies of the sands with silts varied from very loose to medium dense. The moisture content varied between 17% and 32%, and fines contents was 6%.

#### General Strata Observations

Some key observations on the sediment stratigraphy includes:

- All the borings encountered the organic sandy silt or silty sand (SM) layer (Stratum 2) which varied in thickness between 6 and 9 feet.
- In the bottom of the Lake Level Canal, the piston tubes did not encounter an organic sandy silt or silty sand layer (Stratum 2).

#### 6.0 **GROUNDWATER CONDITIONS**

The initial portions of the borings were advanced by dry-auger methods to depths of 5 ft. Groundwater was not observed during these initial dry-auger borings. Following the hand augers, the rotary mud drilling was utilized to boring termination depth. Due to the wet method of drilling and since the boreholes were grouted after explorations were completed, the location of the phreatic line was not determined.

#### 7.0 SEASONAL HIGH GROUNDWATER TABLE

The seasonal high groundwater table (SHGWT) is defined as the highest groundwater level sustained for a period of 2 to 4 weeks during the "wet" season, for existing site conditions, in a year with average normal rainfall amounts.

Based on historical data, the wet season in Central Florida is typically between late May and mid-October. In order to estimate the seasonal high groundwater level at the boring locations, many factors may be considered, such as the following:

- Measured groundwater table
- Drainage characteristics of existing soil types
- Season of the year (wet/dry season)
- Current & historical rainfall data (recent and year-to-date)
- Natural relief points (such as lakes, rivers, swamp areas, etc.)



- Man-made drainage systems (ditches, canals, etc.)
- Vegetative indicators
- Review of available published literature including USDA Soil Survey, Potentiometric Maps, etc.
- Stratigraphy including the presence of hydraulically restrictive layers
- Redoximorphic features (i.e. soil mottling, color, etc.)

Based on the ground conditions encountered during the field explorations, our site observations, and information in the National Resource Conservation Service (NRCS) soil survey data, the estimated SHGWT at the site is presented in **Table 3**.

## TABLE 3 - Seasonal High Groundwater Table (SHGWT) Conditions based on the 2018 and2020 borings

SPT NO.	USDA-NRCS Soil Type	USDA-NRCS Estimated SHGWT (ft, bgs) <sup>(1)</sup>	Estimated Groundwater depth During Drilling (ft, bgs)	SHGWT Indicator depth (ft, bgs)	Estimated SHGWT depth range (ft, bgs)
2018 - SPT-1	Everglades Muck, depressional	2.0	N/E <sup>(2)</sup>	N/A <sup>(3)</sup>	
2018 - SPT-2	Everglades Muck, depressional	2.0	10.0	N/A <sup>(3)</sup>	
2018 - SPT-3	Everglades Muck, depressional	3.0	4.0	3.0 (4)	
2018 - SPT-4	Everglades Muck, depressional	4.0	4.0	4.0 (4)	
2018 - SPT-5	Everglades Muck, depressional	4.0	2.5	4.0 (4)	
2018 - SPT-6	Wauchula Sand	0.5	2.0	2.5 <sup>(4)</sup>	2.0 - 8.0
2018 - SPT-7	Gator Muck, frequently ponded, 0 to 1 percent slopes	8.0	8.0	8.0 (4)	
2018 - SPT-8	Gator Muck, frequently ponded, 0 to 1 percent slopes	6.0	N/E <sup>(2)</sup>	N/A <sup>(3)</sup>	
2020 - SPT-1	Everglades muck, depressional	3.0	N/E <sup>(2)</sup>	3.0 (4)	
2020 - SPT-2	Everglades muck, depressional	2.0	N/E <sup>(2)</sup>	5.0 <sup>(4)</sup>	



SPT NO.	USDA-NRCS Soil Type	USDA-NRCS Estimated SHGWT (ft, bgs) <sup>(1)</sup>	Estimated Groundwater depth During Drilling (ft, bgs)	SHGWT Indicator depth (ft, bgs)	Estimated SHGWT depth range (ft, bgs)
2020 - SPT-3	Everglades muck, depressional	3.0	N/E <sup>(2)</sup>	3.0 (4)	
2020 - SPT-4	Everglades muck, depressional	2.0	N/E <sup>(2)</sup>	2.0 (4)	
2020 - SPT-5	Gator muck, frequently ponded, 0 to 1 percent slopes	2.0	N/E <sup>(2)</sup>	2.0 (4)	

Notes:

(1) Considers existing berm fill height. Refer to boring logs in **Appendix B**.

(2) N/E = Not Encountered. No indicators were encountered during the exploration.

(3) N/A = Not Available.

(4) Based on recovered samples.

The recovered soil samples showed visible signs of SHGWT such as the organic sandy silt (OL and silty sand (SM) layers. Based on the information in the NRCS Soil Survey data, the soil types and properties identified in the borings, Wood estimates that the typical SHGWT at this site will be approximately between 2.0 to 8.0 ft below the top of the existing berms.

#### 8.0 ENGINEERING PROPERTY OF MATERIALS

#### <u>Walkways</u>

Engineering properties of materials for the proposed walkways were selected for evaluating the lateral loads and axial capacities of the steel pile profile proposed to support these structures. Using boring 2020-SPT-4 as the worst-case scenario and previous geotechnical experience with similar soil conditions and site characteristics, properties were assigned to the strata on which the proposed walkways will be installed. **Table 4** presents the properties assigned to each stratum.

Stratum No.	Description	SPT-N Range	Unit Weight (pcf)	Effective Weight (pcf)	Undrained Shear Strength, S <sub>u</sub> (psf)	Effective Internal Friction Angle (φ')	Strain Factor ε <sub>50</sub>
2	Organic Sandy Silt (OL) to Silty Sand (SM)	2-5	80	17.6	200	0	0.02
3	SAND (SP) to Clayey SAND (SC) to SAND with clay (SP-SC),	5	115	52.6	0	28	-



Stratum No.	Description	SPT-N Range	Unit Weight (pcf)	Effective Weight (pcf)	Undrained Shear Strength, Su (psf)	Effective Internal Friction Angle (φ')	Strain Factor ٤ <sub>50</sub>
4	Sandy Clay (CL to CH)	3 - 5	120	57.6	200	0	0.02
	Sand with Silt (SP- SM), Loose	4 – 8	115	57.6	0	28	-
5	Sand with Silt (SP- SM), Medium Dense	23	115	57.6	0	30	-
	Sand with Silt (SP- SM), Very Dense	56	115	57.6	0	35	-

#### 9.0 ENGINEERING ANALYSIS

According to information provided by the SJRWMD, the proposed walkways will be built for pedestrian use, therefore the loads are expected to be low. Any work requiring heavy equipment would be performed from the berms. The proposed lengths of the gate access walkways vary between 25 and 28 feet, as shown in **Figures 3**, **5** and **6**. These figures also show the cross sections of the North-West, South-East and South-West walkways.

The engineering analyses considered the following parameters:

- Maximum Water elevation: +64.0 ft (NAVD88)
- Platform support steel piles: HP8X36
- Yield Stress (f'<sub>y</sub>) of steel: 50,000 psi

These proposed piles will support only the walkways. In this report, Wood considered a typical pile analysis at the junction of Marsh Rabbit Road and the North South Road using the information from 2020-SPT-4 as the worst-case scenario. 2020-SPT-4 is located on the north-west corner of this intersection.

#### 9.1 Steel pile lateral capacity analysis

A lateral load analysis for the supports of the proposed walkways was performed in order to verify if the steel supports are adequate to withstand the design loads. The maximum water elevation considered for this analysis is at +64.0 ft (NAVD88). **Figures 5** and **6** show elevations of the proposed pile support system which will support the proposed walkways.

When the berm is raised with additional fill to its final elevation of 64.78 ft (NAVD88), there will be some additional settlement (i.e., lateral and vertical deformation) of the berm due to consolidation of the underlying organic layer. If the filling is done after the steel pile and



walkway structures are installed, this movement will induce additional stresses on the pile support systems and structures. The additional loads and stresses that would occur on the piles and walkways have not been considered for this analysis. The final design of the structure and steel pile system can be refined to account for the potential additional stresses.

A lateral load analysis was performed for the proposed steel pile profile HP8X36 using the computer program LPILE v2016, by Ensoft. The subsurface conditions from boring 2020-SPT-4 were used to develop our analysis profile. For modelling purposes, a free length of 9 ft was considered.

Also, for the lateral load analysis, our analyses considered the worst-case scenario which was for the steel piles at the edge of the proposed walkways as they are the farthest from the berm.

#### **Boundary Conditions**

The analysis was performed for a two pile-head loading condition:

- 1. Shear and Moment: A shear force of 1,250 lbs, 0 kips-in bending moment and an applied axial compression load of 4,000 lbs.
- 2. Shear and Slope: A shear force of 1,250 lbs, 0 radians slope and an applied axial compression load of 4,000 lbs.

The soil undrained shear strength, unit weight, friction angle, and coefficient of lateral subgrade reaction (k) values used in the *LPILE v2016* analyses were estimated based on our experience, published empirical correlations, and available field and laboratory test data. A summary of the results of lateral load analysis conditions for the proposed HP8X36 steel pile is presented in **Table 5**. The complete *LPILE v2016* outputs from each computer run are presented in **Appendix D**.

Pile-Head Loading condition	Pile top elevation (NAVD88, ft)	Pile tip elevation (NAVD88 , ft)	Embedment Length (ft)	Applied Shear Load (lbs)	Applied Bending Moment (kips-in)	Slope (rad)	Applied Axial Load (Kips)	Max Bending Moment (kips-in)	Pile Head Deflection (in)
Shear and Moment	- +64.3	. 24. 2	31.0 1,2	1 250	0	-	4,000	180	1.0
Shear and Slope		+24.3		1,250	-	0	4,000	67	0.23

TABLE 5 - Summary of Pile Lateral Load Analysis. Steel Pile HPX36

**Table 6** presents the comparison between the lateral analysis results and the properties of theHP8X36 profile provided by the American Institute of Steel Construction (AISC).



Steel Profile	Yield Stress (f' <sub>y</sub> ) (psi)	Section Modulus (in <sup>3</sup> )	Reduction Factor, φ <sub>red</sub>	M <sub>red</sub> (kips-ft)	Computed M <sub>max</sub> capacity (kips-ft)	Comments
HP8X36	50,000	29.80	0.6	10,728	2,160	Steel Section is Acceptable

#### TABLE 6 - Profile properties comparison vs computed results.

Based on the results of lateral analysis, the lateral analysis provides the most critical pile embedment depth (30 feet minimum) in order to resist the design loads. Final recommendations are provided in the recommendation section for walkways.

#### 9.2 Steel pile axial and uplift capacity analysis

The axial capacity of the proposed steel pile supports was estimated following the guidelines by United States Department of Transportation of Federal Highway Administration (FHWA) – Design and Construction of Driven Pile Foundations – Volume 1. For cohesive soils we used the "alpha" method approach and for cohesionless soils we based our calculations on the Nordlund Method. **Table 7** presents the estimated axial capacity and depth for the proposed steel profile HP8X36. An axial load factor of safety (FS) of 2 was considered for these calculations.

As mentioned before, the subsurface conditions from boring 2020-SPT-4 were used to develop our analysis profile.

Pile Type	Pile Top Elevation (ft, NAVD88)	Pile Tip Elevation (ft, NAVD88)	Embedment Depth (ft)	Total Pile length from Bottom of Platform (ft)	Estimated Unfactored Axial Capacity (kips)	Estimated Allowable Axial Capacity (Q <sub>all</sub> ) (kips) (FS =2)
Steel Pile	+64.3	+24.3	31.0	40	36.0	18.0

#### TABLE 7 - Summary of Axial Capacity Estimates for steel pile profile HP8X36

The uplift capacity analysis for single steel piles was based on the guidelines provided by United States Department of Transportation of Federal Highway Administration (FHWA) – Design and Construction of Driven Pile Foundations – Volume 1. For cohesive soils and using the "alpha" method approach, this manual recommends an uplift reduction factor  $\varphi_{up}$  of 0.25. On the other hand, for cohesionless soils, using the Nordlund Method, this manual recommends an uplift reduction factor  $\varphi_{up}$  of 0.35 of the ultimate friction resistance. **Table 8** presents the summary table of the estimated uplift capacity for the proposed steel pile. **Appendix E** includes the axial and uplift resistance calculations.



#### TABLE 8 - Summary of Uplift Capacity for steel pile profile HP8X36

Pile top elevation (ft, NAVD88)	Pile Tip Elevation (ft, NAVD88)	Embedment Depth (ft)	Total pile Length from bottom of platform (ft)	Estimated Factored Uplift Resistance (Rup) (kips)
+64.3	+24.3	31	40	11.5

#### **10.0 CONSTRUCTION RECOMMENDATIONS**

#### **10.1 Proposed Aluminum Culvert Pipes (ACP)**

**Table 9** presents a summary of the bearing strata (as described in section 5) at which the average invert elevations of these culverts will be located. **Figures 4** and **5** indicate the proposed ACP average invert elevations.

ACP No.	Proposed ACP Location	Proposed ACP Diameter (in)	Figure No. <sup>(1)</sup>	Proposed Average Invert Elevation (ft) (NAVD88) <sup>(2)</sup>	Associated Boring	Bearing Strata (3)	Description
1	Duda West Road, STA 22+04	15	4	+58.8	2020-SPT-1	2	Organic Sandy Silt (OL) to Silty Sand (SM)
2	Duda West Road, STA 31+22	15	4	+59.3	2020-SPT-2	3	SAND (SP) to Clayey SAND (SC) to SAND with clay (SP- SC)
2	Marsh Rabbit Road, STA 44+51.49 (South End)	48	5	+57.0	2020-SPT-3	2	Organic Sandy Silt (OL) to Silty Sand (SM)
3	Marsh Rabbit Road, STA 44+51.49 (North End)	48	5	+57.0	2020-SPT-4	2	Organic Sandy Silt (OL) to Silty Sand (SM)

#### TABLE 9 - Current bearing strata on proposed ACPs

Notes:

(1) From the "St. Johns River Water Management District, Upper Ocklawaha River Basin, Lake Apopka Duda Water Storage Improvements, 60% drawings".

(2) Average invert elevation between inlet and outlet.



(3) Refer to boring logs in Appendix B and Section 5.

As described in section 5, the organic sandy silts (OL) and silty sands (SM) encountered in strata 2 have organic contents between 7% and 91%. Soils with organic content in excess of 5%, by weight, are considered non-adequate as bearing strata.

**Table 10** presents recommendations of bottom of ground improvement elevations for the proposed ACPs at Duda Property.

## TABLE 10 - Recommended Bottom of Ground Improvement Elevations for the ProposedACPs at Duda Property

ACP No.	Location of Proposed ACP	Associated Boring	Figure No.	Proposed Average Invert Elevation (ft, NAVD88)	Recommended Bottom Elevation of Removal and replacement (ft, NAVD88)
1	Duda West Road, STA 22+04	2020-SPT-1	4	+58.8	+55.0
2	Duda West Road, STA 31+22	2020-SPT-2	4	+59.3	+57.0
2	Marsh Rabbit Road, STA 44+51.49 (South End)	2020-SPT-3	5	+57.0	+54.5
3	Marsh Rabbit Road, STA 44+51.49 (North End)	2020-SPT-4	5	+57.0	+55.0

Wood's recommendations are as follows:

- Install a stable trench support system down to the bottom of excavation depth.
- Dewater at least 2 feet below the bedding layer in order to facilitate proper placement and compaction of this layer and to provide adequate bedding for the pipes.
- The contractor is responsible for the design of the trench shoring. The design should be performed under the direction of a licensed professional engineer. Signed and sealed design documents and plans should be submitted to the engineer for review and approval prior to beginning construction.
- For the proposed ACPs 1 and 3, Wood recommends ground improvement works by removing the organic soils (Stratum 2) underneath the proposed culverts and replacement by a competent bearing material. Refer to **Table 10**.
- Material to be used as replacement of the organic soils will be a compacted quality fill. The compacted fill will likely consist of fine-grained quartz sands with variable silty to clayey fines generated from site excavations or imported. A minimum fines content (percent by dry weight of soil passing No. 200 Sieve) of 7% and a maximum 3-inch



particle size should be specified. The Compacted Fill should be mechanically placed in a controlled manner and compacted to a minimum of 95% of its Standard Proctor maximum dry density. This compacted fill should be placed in loose lifts of 6-inch-thick maximum

- For the proposed ACP No. 2, Wood recommends removing the existing clayey sands and compacting the existing material to be used as bearing soil for the proposed ACP.
- In areas where there is not enough room for the compaction equipment, the backfill material should be compacted using proper means.
- The Contractor should notify the Owner when fill operations associated with these works are to commence 24 hours prior to the start of fill placement for inspection and verification. Since ground conditions vary throughout the site, it is also recommended to have a qualified inspector on site at the time of performing these activities as organic soil depths might vary and excavation elevation targets might be different from the ones proposed in Table 12.

#### 10.2 Proposed Corrugated Metal Pipe (CMP) Risers

There are 2 proposed CMP risers: the NW Riser and the SW Riser, both north and south of Marsh Rabbit Road, as shown in **Figures 2 and 3**. The CMP risers are going to have a metal bottom.

Wood's recommendations are as follows:

• The foundation of CMP risers should be dry and firm, and dewatered if necessary (at least 2 feet below grade). The foundations should be free of organic materials and debris. The fill will likely consist of fine-grained quartz sands with variable silty to clayey fines generated from site excavations or imported. A minimum fines content (percent by dry weight of soil passing No. 200 Sieve) of 7% and a maximum 3-inch particle size should be specified. The fill should be mechanically placed in a controlled manner in loose lifts of 6-inch-thick maximum and compacted to a minimum of 95% of Standard Proctor maximum dry density.

#### 10.3 Proposed Walkways

Four walkways will be constructed for pedestrian access purposes. These proposed walkways will vary in length between 25 and 28 feet, as shown in **Figures 3**, **5** and **6**. According to the SJRWMD, the walkways will be only used for pedestrian purposes, therefore the expected loads are small. SJRWMD plans to use steel profiles HP8X36. As mentioned in section 9, the pile recommendations were based on the boring that provided the worst-case scenario (2020-SPT-4) at the intersection between Marsh Rabbit Road and North South Road. **Table 11** summarizes our recommendations related to using HP8X36 for these walkways:



#### TABLE 11 – Recommendations for proposed HP8X36 profiles for Walkways.

Pile Profile	Proposed top elevation (ft, (NAVD88)	Proposed tip elevation (ft, NAVD88)Proposed Pile Length (ft)Pile Embedment depth (ft)		Yield Stress (f' <sub>y</sub> ) (psi)	
HP8X36	+64.3	+24.3	40.0	31	50,000

Wood's recommendations are as follows:

#### Proposed steel piles:

- During production steel pile driving, a Saximeter pile driving analyzer (PDA) shall be used to record the blow counts and corresponding hammer stroke (drop) heights on the pile driving logs.
- The Contractor shall notify the Inspector 24 hours prior to the start of operations associated with these works for inspection and verification.

#### **10.4 Proposed 48-inch ACP in Berm Plug**

The proposed berm plug details are shown in **Figures 7** and **8**. The proposed berm plug will be built at the intersection between Marsh Rabbit Road and Lake Level Canal Road, at the Lake Level Canal. Underneath the berm, there will be a proposed 48-inch ACP, 70 feet long, that will connect the water bodies of Lake Level Canal from north and south of the proposed berm.

Boring 2020-SPT-5 and Piston Tubes 2020-PT-1 and 2020-PT-2, below the existing canal bottom elevation (+56.0 ft), did not encounter organic sandy silts (OL) and silty sands (SM) (Stratum 2).

Wood's recommendations are as follows:

- Dewater at least 2 feet below the bedding layer in order to facilitate proper placement and compaction of this layer and to provide a solid bedding for the 48-inch pipe.
- Remove the existing clayey sands and sands with clays to a depth of 2 feet below bottom of ditch and compact the existing material to be used as bearing soil for the proposed 48-inch ACP.
- Material to be used as replacement of the organic soils will be a compacted quality fill. The compacted fill should consist of medium to fine-grained quartz sands with variable silty to clayey fines generated from site excavations or imported. A minimum fines content (percent by dry weight of soil passing No. 200 Sieve) of 7% and a maximum 3-



inch particle size should be specified. The Compacted Fill should be mechanically placed in a controlled manner and compacted to a minimum of 95% of its Standard Proctor maximum dry density. This compacted fill should be placed in loose lifts 6-inch-thick maximum.

- In areas where there is not enough space for compaction equipment, the backfill material should be compacted using proper means.
- The Contractor should notify the Owner when fill operations associated with these works are to commence 24 hours prior to the start of fill placement for inspection and verification. Since ground conditions vary throughout the site, it is also recommended to have a qualified inspector on site at the time of performing these activities as soil conditions may vary from the ones reported in **Appendix B**.

#### 10.5 Proposed Berm Plug

Boring 2020-SPT-5, between 2 and 11 feet below ground surface, encountered organic sandy silts (OL) (Stratum 2), between elevations +65 feet and +56 feet. There was no boring performed on the East side of Lake Level Canal, therefore Wood cannot conclude if this organic layer could be encountered on that side of the canal. A section of the proposed berm plug is presented in **Figure 8**.

Wood's recommendations are as follows:

- Clear and grub the footprint of the proposed berm plug as shown in **Figure 7**.
- Remove the organic silt (OL) or silty sand (SM) layer of the footprint where the berm plug will be built (**Figure 7**).
- The bottom of the proposed berm plug should be dry and firm, and dewatered if necessary. The foundations of this berm plug should be free of organic materials and debris. The compacted fill should consist of medium to fine-grained quartz sands with variable silty to clayey fines generated from site excavations or imported. A minimum fines content (percent by dry weight of soil passing No. 200 Sieve) of 7% and a maximum 3-inch particle size is recommended. The compacted fill should be mechanically placed in a controlled manner and compacted to a minimum of 95% of its Standard Proctor maximum dry density. This compacted fill should be placed in loose lifts 6-inch-thick maximum.
- In order to provide adequate bond between the existing berm and the new berm material, the new fill will be keyed into the existing slope. Details of the key should be provided by the contractor during the construction phase.
- The Contractor should notify the Owner 24 hours prior to the start of fill placement for inspection and verification. Since ground conditions vary throughout the site, it is also



recommended to have a qualified inspector on site at the time of performing these activities as the soil conditions may vary from the ones reported in **Appendix B**.

- The earthwork activities associated with the proposed berm plug and the 48-inch ACP should be performed simultaneously.
- The stability design of the proposed berm is beyond the scope of work of this project.



#### 11.0 REPORT LIMITATIONS

The conclusions and recommendations presented in this report assume that site conditions are not substantially different than those exposed by the explorations. If during construction, subsurface conditions are observed or appear to be different from those encountered in the explorations, Wood should be advised promptly so that those conditions can be reviewed, and recommendations reevaluated, where necessary.

The boring log represents the subsurface conditions at the specific location at the time of the exploration. The subsurface conditions at other locations or at different times may differ, and no warranty as to the subsurface conditions elsewhere or at different times is expressed or implied by the data presented herein. Furthermore, the depths on the boring log designating the interface between the various soils and rocks may only be approximate boundaries where the transition is gradual or could not be detected by the boring operations. In addition, the depth of the groundwater table, if encountered, is only indicative of the conditions at the time of the borings as groundwater level may fluctuate significantly because of various factors.

The recommendations provided in this report are based on the scope of the exploration and testing program. In addition, this report does not reflect the subsurface conditions below the tested depths.

The evaluation of conditions that may be encountered in construction requires engineering judgment and interpretation. For this reason, we recommend that Wood remain involved with this project during the construction process, particularly during foundation construction and general earthwork operations. If we are not retained during construction, we cannot assume responsibility for misinterpretation of our recommendations, or for unfavorable foundation and pavement performance as a result of judgments rendered by others.



#### 12.0 <u>REFERENCES</u>

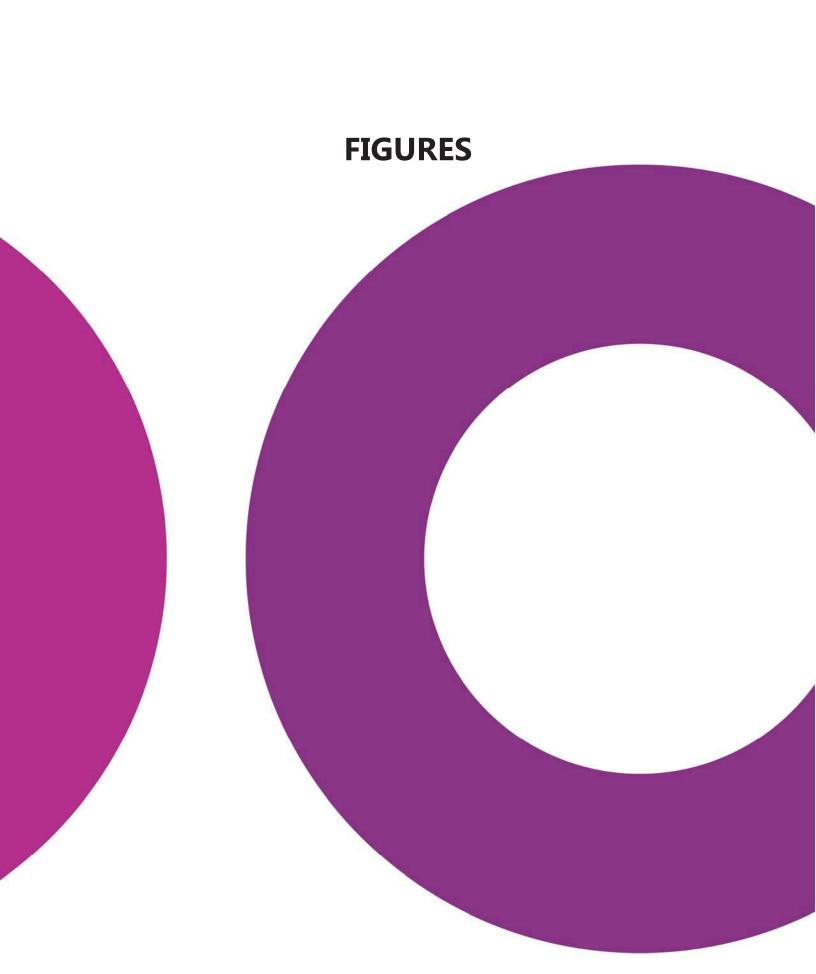
United States Geological Survey (USGS), *Geologic Units in Lake County, Florida,* March 15, 2020; USGS Website: <u>https://www.usgs.gov/</u>

United States Geological Survey (USGS), *Geologic Units in Orange County, Florida,* March 15, 2020; USGS Website: <u>https://www.usgs.gov/</u>

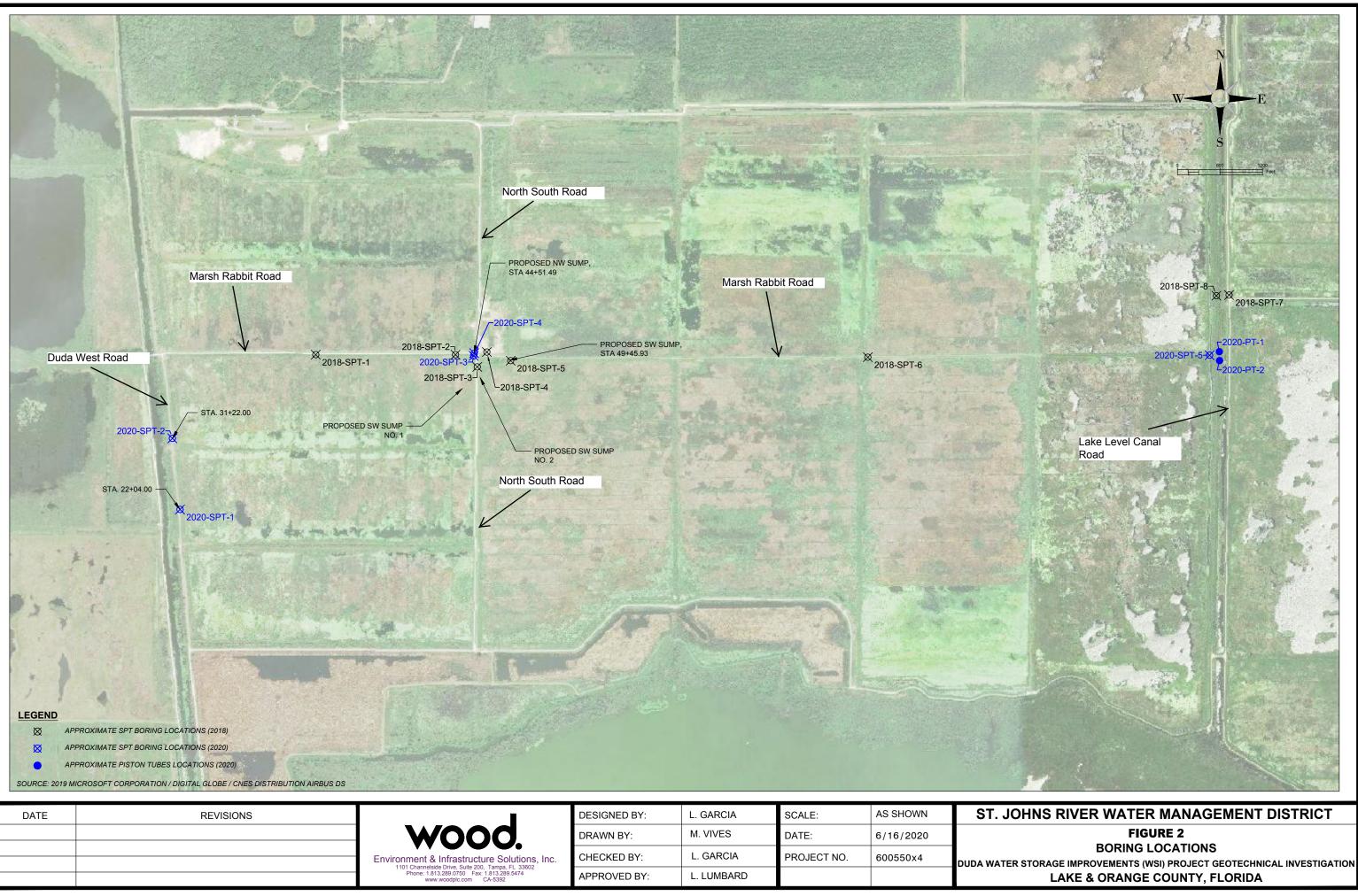
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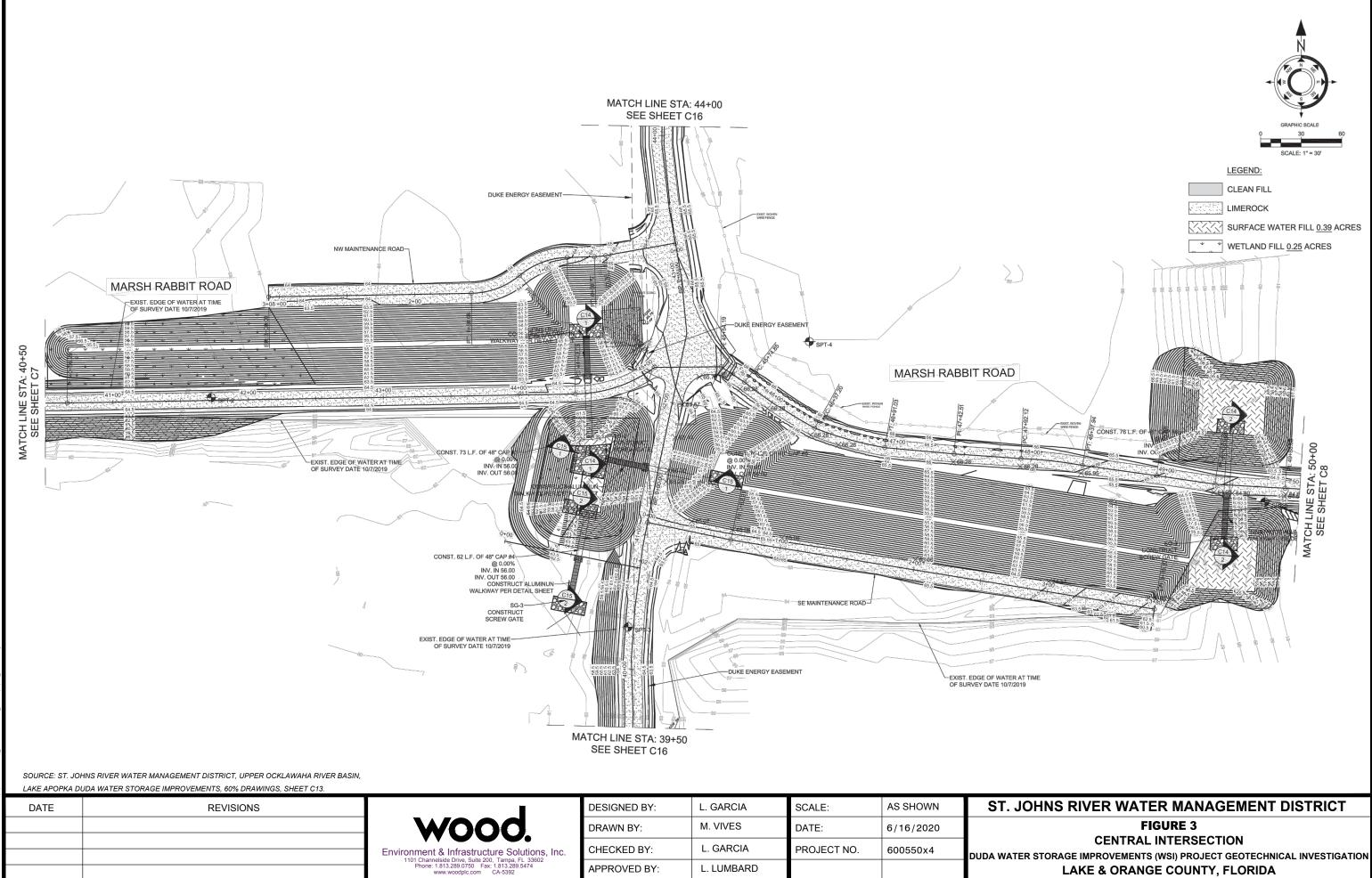
Lake Apopka Duda Area Pumps, Structure and Levee Improvements Preliminary Geotechnical Report, October 2018.

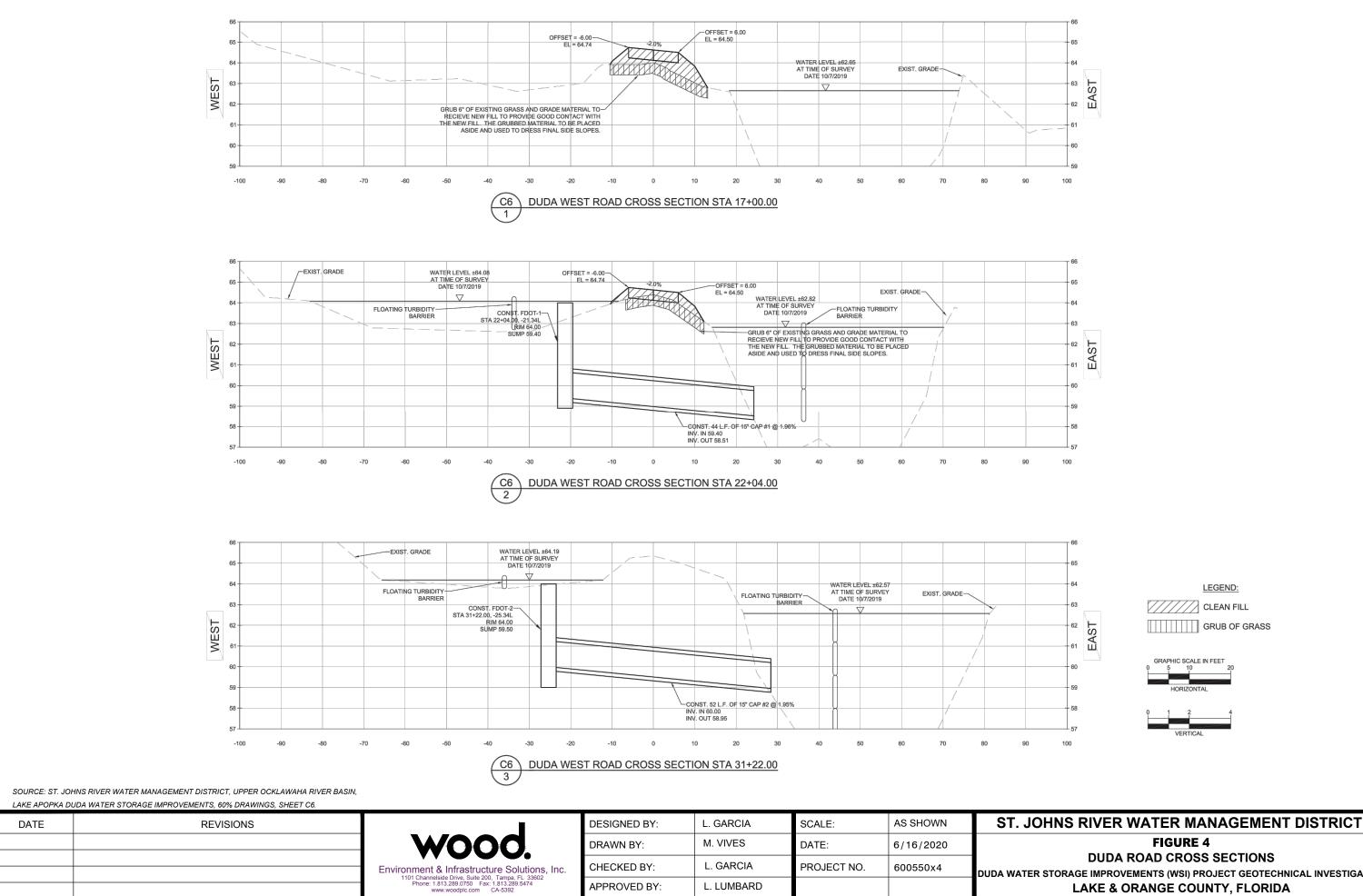




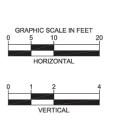






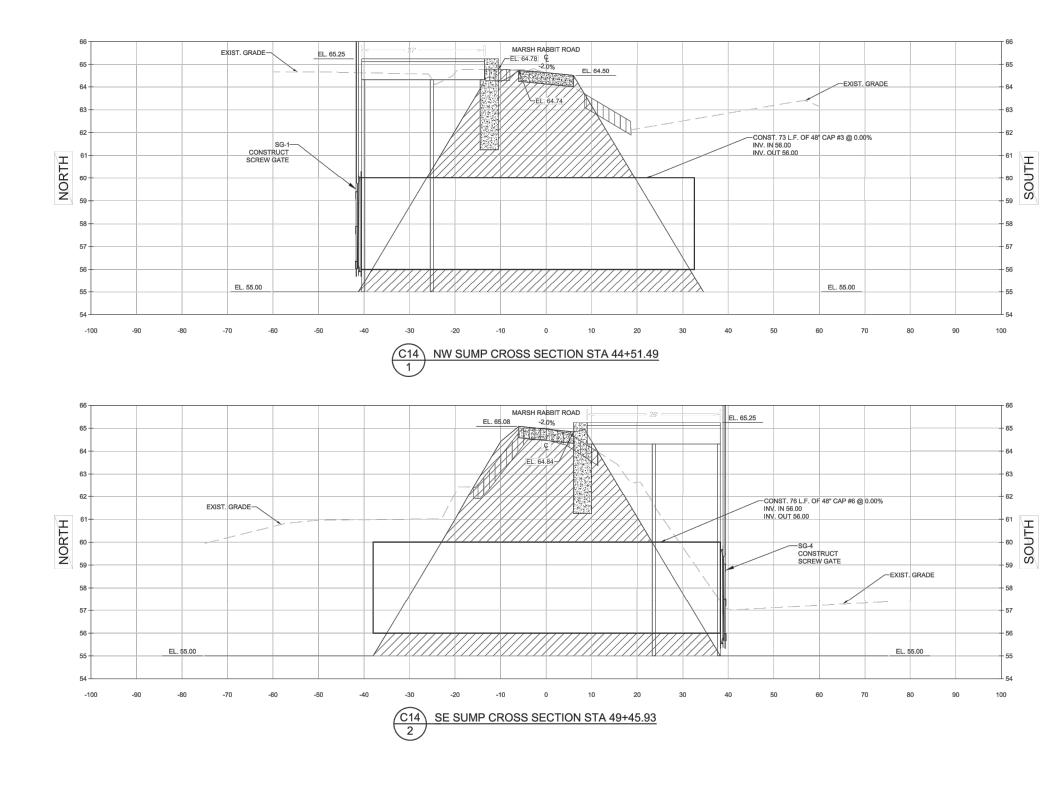


#### FIGURE 4 DUDA ROAD CROSS SECTIONS DUDA WATER STORAGE IMPROVEMENTS (WSI) PROJECT GEOTECHNICAL INVESTIGATION LAKE & ORANGE COUNTY, FLORIDA



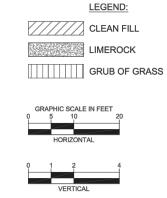


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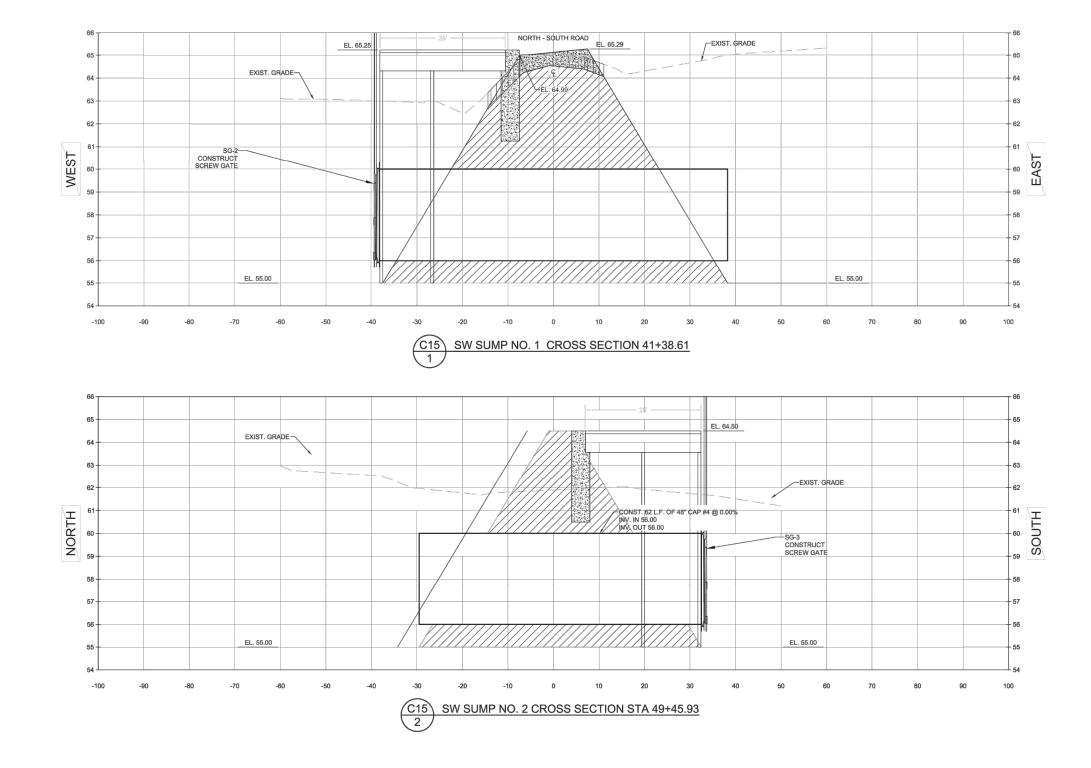
SOURCE: ST. JOHNS RIVER WATER MANAGEMENT DISTRICT, UPPER OCKLAWAHA RIVER BASIN,

LAKE APOPKA DUDA WATE	R STORAGE IMPROVEMENTS, 60% DRAWINGS, SHEET C14.						
DATE	REVISIONS		DESIGNED BY:	L. GARCIA	SCALE:	AS SHOWN	ST.
		WOOD.	DRAWN BY:	M. VIVES	DATE:	5/21/2020	
		Environment & Infrastructure Solutions, Inc.	CHECKED BY:	L. GARCIA	PROJECT NO.	600550x4	DUDA WA
		1101 Channelside Drive, Suite 200, Tampa, FL 33602 Phone: 1.813.289.0750 Fax: 1.813.289.5474 www.woodplc.com CA-5392	APPROVED BY:	L. LUMBARD			



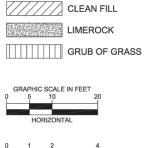
JOHNS RIVER WATER MANAGEMENT DISTRICT FIGURE 5 CENTRAL INTERSECTION CROSS SECTIONS ATER STORAGE IMPROVEMENTS (WSI) PROJECT GEOTECHNICAL INVESTIGATION

LAKE & ORANGE COUNTY, FLORIDA



SOURCE: ST. JOHNS RIVER WATER MANAGEMENT DISTRICT, UPPER OCKLAWAHA RIVER BASIN,

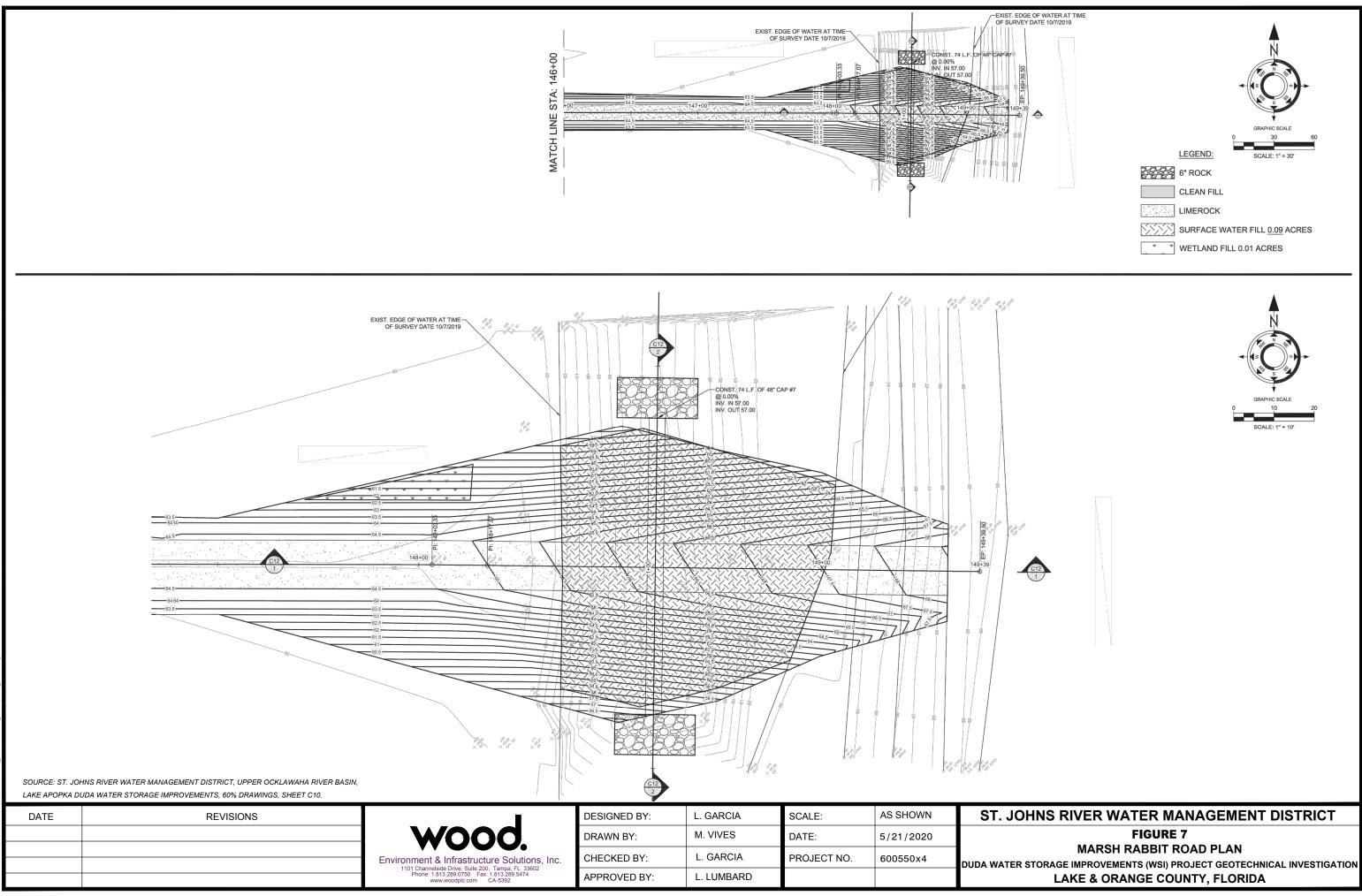
LAKE APOPKA DU	JDA WATER STORAGE IMPROVEMENTS, 60% DRAWINGS, SHEET C15.						
DATE	REVISIONS		DESIGNED BY:	L. GARCIA	SCALE:	AS SHOWN	ST.
		WOOD.	DRAWN BY:	M. VIVES	DATE:	5/21/2020	
		Environment & Infrastructure Solutions, Inc.	CHECKED BY:	L. GARCIA	PROJECT NO.	600550x4	
		1101 Channelside Drive, Suite 200, Tampa, FL 33602 Phone: 1.813.289.0750 Fax: 1.813.289.5474 www.woodplc.com CA-5392	APPROVED BY:	L. LUMBARD			

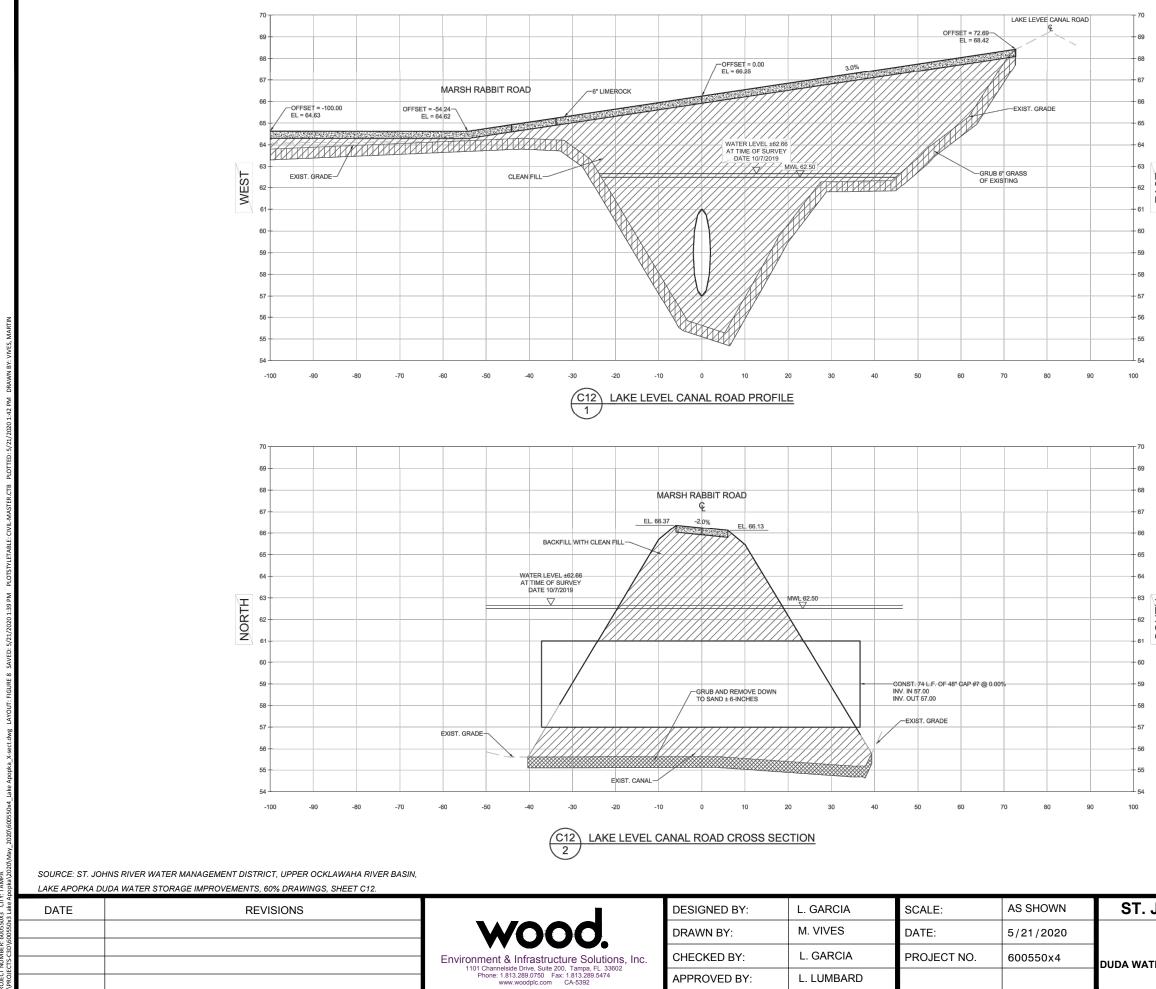


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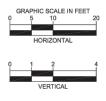
FIGURE 6 CENTRAL INTERSECTION CROSS SECTIONS TER STORAGE IMPROVEMENTS (WSI) PROJECT GEOTECHNICAL INVESTIGATION LAKE & ORANGE COUNTY, FLORIDA

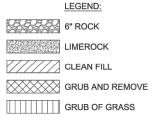
# JOHNS RIVER WATER MANAGEMENT DISTRICT





#### ST. JOHNS RIVER WATER MANAGEMENT DISTRICT FIGURE 8 PROPOSED 48" ACP AND BERM PLUG SECTION DUDA WATER STORAGE IMPROVEMENTS (WSI) PROJECT GEOTECHNICAL INVESTIGATION LAKE & ORANGE COUNTY, FLORIDA





SOUTH

EAST

### **APPENDIX A**



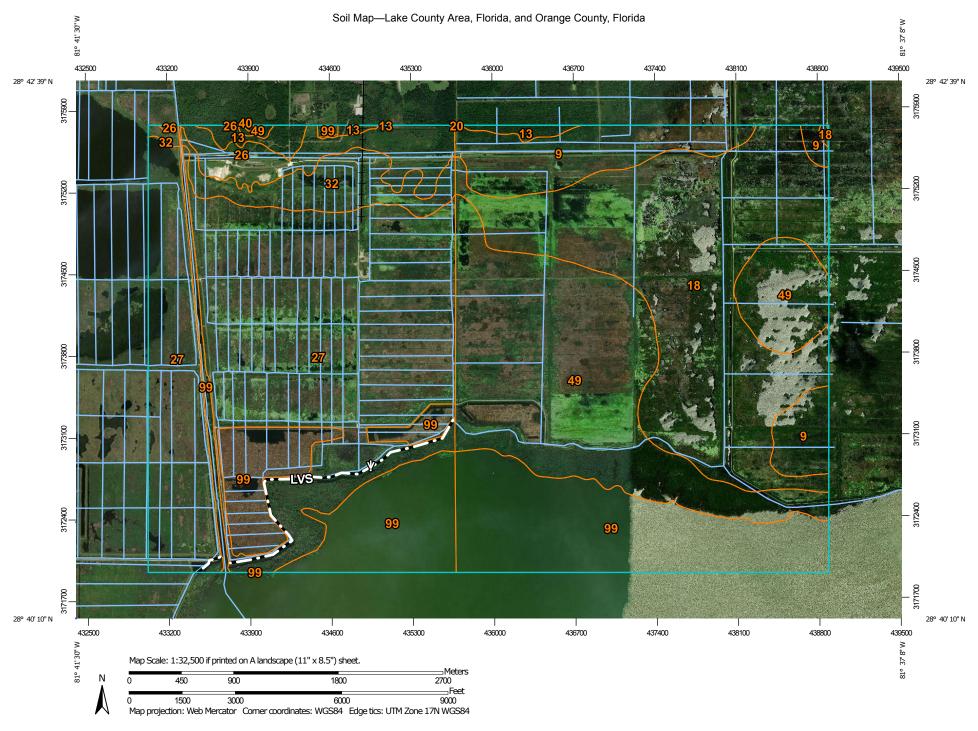
United States Department of Agriculture

Natural Resources Conservation

Service

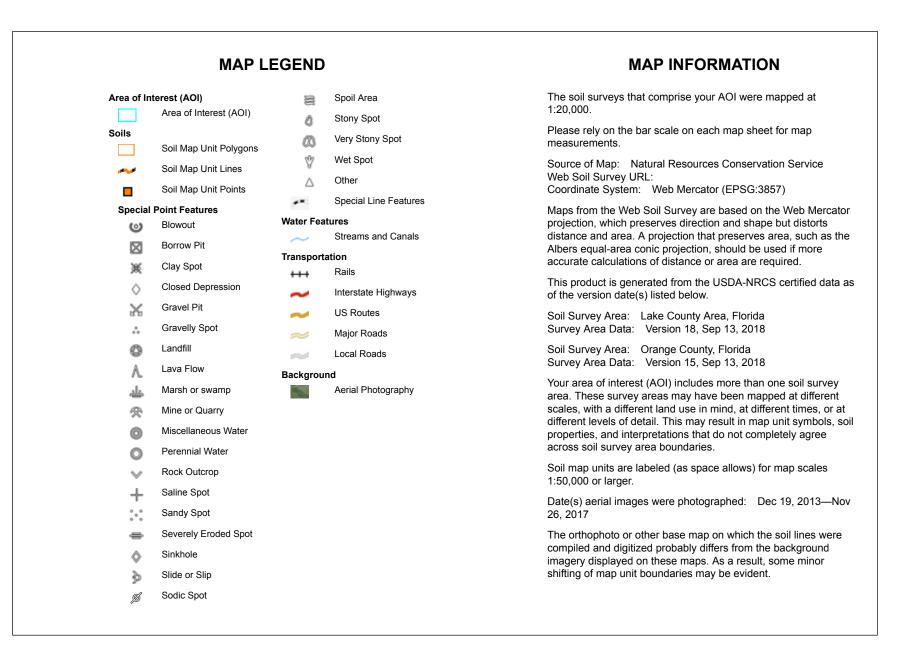
A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants Custom Soil Resource Report for Lake County Area, Florida, and Orange County, Florida





USDA Natural Resources

Conservation Service





# Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
13	Emeralda fine sand	38.9	0.7%
20	Immokalee sand	0.1	0.0%
26	Manatee fine sand, depressional	177.4	3.2%
27	Everglades muck, depressional	1,625.6	29.2%
32	Oklawaha muck	182.1	3.3%
40	Placid and Myakka sands, depressional	0.8	0.0%
49	Wauchula sand	5.3	0.1%
99	Water	483.8	8.7%
Subtotals for Soil Survey A	rea	2,514.0	45.1%
Totals for Area of Interest		5,569.7	100.0%

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
9	Canova muck	327.0	5.9%
13	Felda fine sand, 0 to 2 percent slopes	18.4	0.3%
18	Gator muck, frequently ponded, 0 to 1 percent slopes	1,125.3	20.2%
20	Immokalee fine sand	0.1	0.0%
49	Terra Ceia muck, frequently ponded, 0 to 1 percent slopes	1,038.7	18.6%
99	Water	546.2	9.8%
Subtotals for Soil Survey A	rea	3,055.7	54.9%
Totals for Area of Interest		5,569.7	100.0%

USDA

# Lake County Area, Florida

### 13—Emeralda fine sand

#### **Map Unit Setting**

National map unit symbol: 1qt66 Elevation: 30 to 100 feet Mean annual precipitation: 46 to 54 inches Mean annual air temperature: 68 to 75 degrees F Frost-free period: 340 to 365 days Farmland classification: Not prime farmland

#### **Map Unit Composition**

*Emeralda and similar soils:* 90 percent *Minor components:* 10 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Emeralda**

#### Setting

Landform: Depressions on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Parent material: Clayey marine deposits

#### **Typical profile**

A - 0 to 6 inches: fine sand Eg - 6 to 11 inches: fine sand Btg - 11 to 56 inches: sandy clay BCkg - 56 to 66 inches: sandy clay

#### **Properties and qualities**

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: Frequent
Frequency of ponding: None
Calcium carbonate, maximum in profile: 15 percent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Moderate (about 8.5 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6w Hydrologic Soil Group: C/D Forage suitability group: Loamy and clayey soils on stream terraces, flood plains, or in depressions (G154XB345FL) Other vegetative classification: Freshwater Marshes and Ponds (R154XY010FL) Hydric soil rating: Yes

#### **Minor Components**

#### Felda

Percent of map unit: 5 percent Landform: Flats on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Linear Across-slope shape: Linear Other vegetative classification: Slough (R154XY011FL) Hydric soil rating: Yes

#### Martel

Percent of map unit: 5 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Other vegetative classification: Freshwater Marshes and Ponds (R154XY010FL) Hydric soil rating: Yes

#### 26—Manatee fine sand, depressional

#### Map Unit Setting

National map unit symbol: 1nrvz Elevation: 30 to 100 feet Mean annual precipitation: 46 to 54 inches Mean annual air temperature: 68 to 75 degrees F Frost-free period: 340 to 365 days Farmland classification: Not prime farmland

#### Map Unit Composition

Manatee, depressional, and similar soils: 90 percent Minor components: 10 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Manatee, Depressional**

#### Setting

Landform: Depressions on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Parent material: Sandy and loamy marine deposits

#### **Typical profile**

A - 0 to 10 inches: fine sand Btg - 10 to 40 inches: fine sandy loam BCg - 40 to 48 inches: loamy fine sand Cg - 48 to 60 inches: loamy fine sand

#### **Properties and qualities**

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)
Depth to water table: About 0 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Calcium carbonate, maximum in profile: 15 percent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Moderate (about 8.1 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7w Hydrologic Soil Group: B/D Forage suitability group: Loamy and clayey soils on stream terraces, flood plains, or in depressions (G154XB345FL) Other vegetative classification: Freshwater Marshes and Ponds (R154XY010FL) Hydric soil rating: Yes

#### Minor Components

#### Martel

Percent of map unit: 10 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Other vegetative classification: Freshwater Marshes and Ponds (R154XY010FL) Hydric soil rating: Yes

#### 27—Everglades muck, depressional

#### Map Unit Setting

National map unit symbol: 1qt6n Mean annual precipitation: 46 to 54 inches Mean annual air temperature: 68 to 75 degrees F Frost-free period: 340 to 365 days Farmland classification: Not prime farmland

#### Map Unit Composition

*Everglades, depressional, and similar soils:* 90 percent *Minor components:* 10 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Everglades, Depressional**

#### Setting

Landform: Depressions on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave

#### **Typical profile**

Oa - 0 to 11 inches: muck Oe - 11 to 80 inches: mucky peat

#### Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 5.95 in/hr)
Depth to water table: About 0 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Very high (about 27.3 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 3w
Hydrologic Soil Group: A/D
Forage suitability group: Organic soils in depressions and on flood plains (G154XB645FL)
Other vegetative classification: Freshwater Marshes and Ponds (R154XY010FL)
Hydric soil rating: Yes

#### **Minor Components**

#### Oklawaha, freq. flooded

Percent of map unit: 10 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Linear Across-slope shape: Linear Other vegetative classification: Freshwater Marshes and Ponds (R154XY010FL) Hydric soil rating: Yes

### 32—Oklawaha muck

#### Map Unit Setting

National map unit symbol: 1nrw5 Mean annual precipitation: 46 to 54 inches Mean annual air temperature: 68 to 75 degrees F Frost-free period: 340 to 365 days Farmland classification: Not prime farmland

#### Map Unit Composition

*Oklawaha, freq. flooded, and similar soils:* 90 percent *Minor components:* 10 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### Description of Oklawaha, Freq. Flooded

#### Setting

Landform: Depressions on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Linear Across-slope shape: Linear Parent material: Herbaceous organic material over loamy and clayey marine deposits

#### **Typical profile**

*Oa - 0 to 9 inches:* muck *Oe - 9 to 25 inches:* mucky peat *Cg1 - 25 to 31 inches:* sandy loam *Cg2 - 31 to 54 inches:* sandy clay

#### **Properties and qualities**

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)
Depth to water table: About 0 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: High (about 9.2 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w Hydrologic Soil Group: D  Forage suitability group: Organic soils in depressions and on flood plains (G154XB645FL)
 Other vegetative classification: Freshwater Marshes and Ponds (R154XY010FL)
 Hydric soil rating: Yes

#### Minor Components

#### Brighton, depressional

Percent of map unit: 10 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Other vegetative classification: Freshwater Marshes and Ponds (R154XY010FL) Hydric soil rating: Yes

#### 40—Placid and Myakka sands, depressional

#### Map Unit Setting

National map unit symbol: 1nrwf Elevation: 10 to 60 feet Mean annual precipitation: 46 to 54 inches Mean annual air temperature: 68 to 75 degrees F Frost-free period: 340 to 365 days Farmland classification: Not prime farmland

#### Map Unit Composition

*Placid and similar soils:* 55 percent *Myakka and similar soils:* 35 percent *Minor components:* 10 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Placid**

#### Setting

Landform: Depressions on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Parent material: Sandy marine deposits

#### **Typical profile**

*A* - 0 to 18 inches: sand *C* - 18 to 80 inches: sand

#### **Properties and qualities**

Slope: 0 to 2 percent Depth to restrictive feature: More than 80 inches Natural drainage class: Very poorly drained Runoff class: Negligible

#### **Custom Soil Resource Report**

Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: About 0 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Moderate (about 6.2 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7w
Hydrologic Soil Group: A/D
Forage suitability group: Sandy soils on stream terraces, flood plains, or in depressions (G154XB145FL)
Other vegetative classification: Slough (R154XY011FL)
Hydric soil rating: Yes

#### **Description of Myakka**

#### Setting

Landform: Depressions on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Parent material: Sandy marine deposits

#### **Typical profile**

A - 0 to 6 inches: sand E - 6 to 20 inches: sand Bh - 20 to 36 inches: sand C - 36 to 80 inches: sand

#### **Properties and qualities**

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 5.95 in/hr)
Depth to water table: About 0 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Low (about 5.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7w
Hydrologic Soil Group: A/D
Forage suitability group: Sandy soils on stream terraces, flood plains, or in depressions (G154XB145FL)
Other vegetative classification: Slough (R154XY011FL)
Hydric soil rating: Yes

#### **Minor Components**

#### Wabasso, hydric

Percent of map unit: 5 percent Landform: Flats on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Other vegetative classification: South Florida Flatwoods (R154XY003FL) Hydric soil rating: Yes

#### Ellzey, hydric

Percent of map unit: 5 percent Landform: Flats on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Linear Across-slope shape: Linear Other vegetative classification: South Florida Flatwoods (R154XY003FL) Hydric soil rating: Yes

#### 49—Wauchula sand

#### Map Unit Setting

National map unit symbol: 1nrwq Mean annual precipitation: 46 to 54 inches Mean annual air temperature: 68 to 75 degrees F Frost-free period: 340 to 365 days Farmland classification: Not prime farmland

#### **Map Unit Composition**

Wauchula, non-hydric, and similar soils: 70 percent Wauchula, hydric, and similar soils: 20 percent Minor components: 10 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Wauchula, Non-hydric**

#### Setting

Landform: Rises on marine terraces Landform position (three-dimensional): Rise Down-slope shape: Convex Across-slope shape: Linear Parent material: Sandy and loamy marine deposits

#### Typical profile

*A* - 0 to 6 inches: sand *E* - 6 to 22 inches: sand *Bh* - 22 to 35 inches: sand *E*' - 35 to 38 inches: sand Btg - 38 to 80 inches: sandy clay loam

#### **Properties and qualities**

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)
Depth to water table: About 6 to 18 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Moderate (about 7.7 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 3w
Hydrologic Soil Group: B/D
Forage suitability group: Sandy over loamy soils on flats of hydric or mesic lowlands (G154XB241FL)
Other vegetative classification: South Florida Flatwoods (R154XY003FL)
Hydric soil rating: No

#### **Description of Wauchula, Hydric**

#### Setting

Landform: Flats on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Linear Across-slope shape: Linear Parent material: Sandy and loamy marine deposits

#### **Typical profile**

A - 0 to 6 inches: sand E - 6 to 22 inches: sand Bh - 22 to 35 inches: sand E' - 35 to 38 inches: sand Btg - 38 to 80 inches: sandy clay loam

#### **Properties and qualities**

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Moderate (about 7.7 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 3w
Hydrologic Soil Group: B/D
Forage suitability group: Sandy over loamy soils on flats of hydric or mesic lowlands (G154XB241FL)
Other vegetative classification: South Florida Flatwoods (R154XY003FL)
Hydric soil rating: Yes

#### **Minor Components**

#### Immokalee, non-hydric

Percent of map unit: 10 percent Landform: Flatwoods on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Other vegetative classification: South Florida Flatwoods (R154XY003FL) Hydric soil rating: No

### 99—Water

Map Unit Composition Water: 100 percent Estimates are based on observations, descriptions, and transects of the mapunit.

# **Orange County, Florida**

## 9—Canova muck

#### **Map Unit Setting**

National map unit symbol: bv90 Mean annual precipitation: 45 to 53 inches Mean annual air temperature: 70 to 77 degrees F Frost-free period: 350 to 365 days Farmland classification: Not prime farmland

#### **Map Unit Composition**

Canova, drained, and similar soils: 56 percent Canova, undrained, and similar soils: 30 percent Minor components: 14 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### Description of Canova, Drained

#### Setting

Landform: Depressions on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Parent material: Loamy marine deposits

#### **Typical profile**

Oa - 0 to 6 inches: muck

A - 6 to 16 inches: fine sand

- B 16 to 37 inches: sandy clay loam
- C 37 to 80 inches: sandy clay loam

#### **Properties and qualities**

Slope: 0 to 1 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 5.95 in/hr)
Depth to water table: About 0 to 36 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Calcium carbonate, maximum in profile: 15 percent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Moderate (about 7.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w Hydrologic Soil Group: A/D Forage suitability group: Organic soils in depressions and on flood plains (G155XB645FL) Hydric soil rating: Yes

#### **Description of Canova, Undrained**

#### Setting

Landform: Depressions on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Parent material: Loamy marine deposits

#### **Typical profile**

Oa - 0 to 6 inches: muck

- A 6 to 16 inches: fine sand
- B 16 to 37 inches: sandy clay loam
- C 37 to 80 inches: sandy clay loam

#### **Properties and qualities**

Slope: 0 to 1 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 5.95 in/hr)
Depth to water table: About 0 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Moderate (about 7.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7w Hydrologic Soil Group: A/D Forage suitability group: Organic soils in depressions and on flood plains (G155XB645FL) Hydric soil rating: Yes

#### **Minor Components**

#### Gator

Percent of map unit: 7 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

#### Okeelanta, undrained

Percent of map unit: 7 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

## 13—Felda fine sand, 0 to 2 percent slopes

#### Map Unit Setting

National map unit symbol: 2tzvy Elevation: 0 to 180 feet Mean annual precipitation: 40 to 60 inches Mean annual air temperature: 70 to 77 degrees F Frost-free period: 350 to 365 days Farmland classification: Not prime farmland

#### Map Unit Composition

*Felda and similar soils:* 85 percent *Minor components:* 15 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### Description of Felda

#### Setting

Landform: Drainageways on marine terraces, flatwoods on marine terraces Landform position (three-dimensional): Tread, dip, talf Down-slope shape: Linear Across-slope shape: Linear, concave Parent material: Sandy and loamy marine deposits

#### **Typical profile**

A - 0 to 4 inches: fine sand Eg - 4 to 35 inches: fine sand Btg - 35 to 43 inches: fine sandy loam Cg - 43 to 80 inches: extremely paragravelly fine sand

#### **Properties and qualities**

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 6.00 in/hr)
Depth to water table: About 3 to 18 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 4 percent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Low (about 5.2 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w Hydrologic Soil Group: A/D
Ecological site: Slough (R155XY011FL)
Forage suitability group: Sandy over loamy soils on flats of hydric or mesic lowlands (G155XB241FL)
Other vegetative classification: Slough (R155XY011FL)
Hydric soil rating: Yes

#### **Minor Components**

#### Wabasso

Percent of map unit: 6 percent Landform: Flatwoods on marine terraces Landform position (three-dimensional): Tread, talf Down-slope shape: Linear, convex Across-slope shape: Linear Other vegetative classification: South Florida Flatwoods (R155XY003FL) Hydric soil rating: No

#### Oldsmar

Percent of map unit: 5 percent Landform: Flatwoods on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Convex, linear Across-slope shape: Linear Other vegetative classification: South Florida Flatwoods (R155XY003FL) Hydric soil rating: No

#### Valkaria

Percent of map unit: 4 percent Landform: Drainageways on flatwoods on marine terraces Landform position (three-dimensional): Tread, talf, dip Down-slope shape: Linear Across-slope shape: Linear, concave Other vegetative classification: Slough (R155XY011FL) Hydric soil rating: Yes

### 18—Gator muck, frequently ponded, 0 to 1 percent slopes

#### **Map Unit Setting**

National map unit symbol: 2tzwz Elevation: 0 to 100 feet Mean annual precipitation: 42 to 56 inches Mean annual air temperature: 70 to 77 degrees F Frost-free period: 350 to 365 days Farmland classification: Not prime farmland

#### Map Unit Composition

Gator and similar soils: 83 percent Minor components: 17 percent Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Gator**

#### Setting

Landform: Depressions on marine terraces Landform position (three-dimensional): Tread, dip Down-slope shape: Concave Across-slope shape: Concave Parent material: Herbaceous organic material over sandy and loamy marine deposits

#### **Typical profile**

Oa - 0 to 18 inches: muck

Cg1 - 18 to 36 inches: sandy clay loam

Cg2 - 36 to 55 inches: fine sandy loam

Cg3 - 55 to 80 inches: fine sand

#### **Properties and qualities**

Slope: 0 to 1 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Very high (about 13.1 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w Hydrologic Soil Group: C/D Forage suitability group: Organic soils in depressions and on flood plains (G155XB645FL) Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL) Hydric soil rating: Yes

#### **Minor Components**

#### Terra ceia

Percent of map unit: 5 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Tread, dip Down-slope shape: Concave, convex Across-slope shape: Concave, linear Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL) Hydric soil rating: Yes

#### Chobee

Percent of map unit: 4 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Tread, dip Down-slope shape: Concave Across-slope shape: Concave Ecological site: Freshwater Marshes and Ponds (R155XY010FL) Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL) Hydric soil rating: Yes

#### Tequesta

Percent of map unit: 4 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Tread, dip Down-slope shape: Concave Across-slope shape: Concave Other vegetative classification: Freshwater Marshes and Ponds (R156BY010FL) Hydric soil rating: Yes

#### Felda

Percent of map unit: 3 percent Landform: Flatwoods on marine terraces, drainageways on marine terraces Landform position (three-dimensional): Tread, talf, dip Down-slope shape: Linear Across-slope shape: Linear, concave Ecological site: Slough (R155XY011FL) Other vegetative classification: Slough (R155XY011FL) Hydric soil rating: Yes

#### Pompano

Percent of map unit: 1 percent Landform: Drainageways on marine terraces Landform position (three-dimensional): Tread, dip Down-slope shape: Linear Across-slope shape: Linear, concave Other vegetative classification: Slough (R155XY011FL) Hydric soil rating: Yes

## 49—Terra Ceia muck, frequently ponded, 0 to 1 percent slopes

#### Map Unit Setting

National map unit symbol: 2svzl Elevation: 0 to 130 feet Mean annual precipitation: 45 to 62 inches Mean annual air temperature: 68 to 79 degrees F Frost-free period: 335 to 365 days Farmland classification: Not prime farmland

#### **Map Unit Composition**

*Terra ceia and similar soils:* 80 percent *Minor components:* 20 percent *Estimates are based on observations, descriptions, and transects of the mapunit.* 

#### **Description of Terra Ceia**

#### Setting

Landform: Depressions on marine terraces Landform position (three-dimensional): Tread, dip Down-slope shape: Concave, convex Across-slope shape: Concave, linear Parent material: Herbaceous organic material

#### **Typical profile**

Oa1 - 0 to 15 inches: muck Oa2 - 15 to 44 inches: muck Oa3 - 44 to 80 inches: muck

#### **Properties and qualities**

Slope: 0 to 1 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Very high (about 23.9 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 7w
Hydrologic Soil Group: A/D
Forage suitability group: Organic soils in depressions and on flood plains (G155XB645FL)
Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL)
Hydric soil rating: Yes

#### **Minor Components**

#### Okeelanta

Percent of map unit: 6 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Tread, dip Down-slope shape: Concave Across-slope shape: Concave Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL) Hydric soil rating: Yes

#### Gator

Percent of map unit: 5 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Tread, dip Down-slope shape: Concave Across-slope shape: Concave Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL) Hydric soil rating: Yes

#### Tomoka

Percent of map unit: 3 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Talf, dip Down-slope shape: Concave Across-slope shape: Concave Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL) Hydric soil rating: Yes

#### Okeechobee

Percent of map unit: 2 percent Landform: Marshes on marine terraces Landform position (three-dimensional): Tread, dip Down-slope shape: Concave Across-slope shape: Concave Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL) Hydric soil rating: Yes

#### Anclote

Percent of map unit: 1 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Tread, dip Down-slope shape: Convex, concave Across-slope shape: Linear, concave Hydric soil rating: Yes

#### Chobee

Percent of map unit: 1 percent Landform: Depressions on flatwoods on marine terraces Landform position (three-dimensional): Tread, dip, talf Down-slope shape: Concave, linear Across-slope shape: Concave, linear Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL) Hydric soil rating: Yes

#### Placid

Percent of map unit: 1 percent Landform: Depressions on marine terraces, drainageways on marine terraces Landform position (three-dimensional): Tread, dip Down-slope shape: Concave Across-slope shape: Concave Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL) Hydric soil rating: Yes

#### Pompano

Percent of map unit: 1 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Tread, dip Down-slope shape: Concave Across-slope shape: Concave Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL) Hydric soil rating: Yes

## 99—Water

Map Unit Composition Water: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

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# **APPENDIX B**

#### BORING NUMBER 2018-SPT-1 PAGE 1 OF 1 CLIENT St. Johns River Water Management District (SJRWMD) **PROJECT NAME** Prel. Design - Duda Pumps, Structures, and Levee Imp PROJECT NUMBER 600550X3 PROJECT LOCATION Lake County and Orange County, FL DATE STARTED 9/24/18 **COMPLETED** 9/24/18 GROUND ELEVATION 64 ft HOLE SIZE 2.75 inches DRILLING CONTRACTOR AmDrill, Inc. LOCATION N1586255.35, E440013.24 GROUND WATER LEVEL AT TIME OF DRILLING ----DRILLING METHOD Standard Penetration / Mud Rotary LOGGED BY EG CHECKED BY AC HOLE COMPLETION backfilled with cuttings and bentonite chips NOTES SAMPLE TYPE NUMBER BLOW COUNTS (N VALUE) GRAPHIC LOG DEPTH (ft) U.S.C.S. TESTS MATERIAL DESCRIPTION 0 Light Brownish Gray to Grayish Brown, moist, fine-grained Quartz Silty SAND with SS 5-4-6-3 SM trace roots. (Munsell 10YR6/2 to Munsell 10YR5/2) (Fill) 1 (10) 2.0 62.0 MC = 85% Very Dark Brown, moist Silty SAND with little organics. (Munsell 10YR2/2) 3-3-3-5 SS LL = NP 2 (6) PL = NP SM PI = NP 5 SS 3-4-9-8 OC = 25% 5.0 59.0 (13) Very Dark Brown, moist, fine-grained Silty SAND. (Musell 10YR2/2) 3 SM 6.0 58.0 Dark Brown, moist, fine-grained SAND. (Munsell 10YR3/3) SS 6-9-9-6 MC = 19% (18) #200 = 4% 4 SP SS 5-5-5-8 5 (10) 10 10.0 54.0 SP Light Gray, moist, fine-grained Quartz SAND. (Munsell 10YR 7/1) SS 4-5-6 6 (11)15 15.0 49.0 SM Light Gray, fine-grained Silty SAND. (Munsell 10YR7/1) SS 8-8-7 MC = 25% #200 = 21% 7 (15) 20 44.0

Bottom of borehole at 20.0 feet.

#### LEGEND:

MC=Moisture Content

LL= Liquid Limit

PL= Plastic Limit

PI= Plasticity Index

OC= Organic Content

NP= Not Plastic

#200= Percent passing #200 sieve

#### BORING NUMBER 2018-SPT-2 PAGE 1 OF 1 CLIENT St. Johns River Water Management District (SJRWMD) PROJECT NAME Prel. Design - Duda Pumps, Structures, and Levee Imp PROJECT LOCATION Lake County and Orange County, FL PROJECT NUMBER 600550X3 DATE STARTED \_9/24/18 **COMPLETED** 9/24/18 GROUND ELEVATION 64 ft HOLE SIZE 2.75 inches DRILLING CONTRACTOR AmDrill, Inc. LOCATION N1586255.17, E441985.03 DRILLING METHOD Standard Penetration / Mud Rotary LOGGED BY EG CHECKED BY AC HOLE COMPLETION backfilled with cuttings and bentonite chips NOTES Culvert 1: NW Cell to SW Duda Property Canal SAMPLE TYPE NUMBER BLOW COUNTS (N VALUE) GRAPHIC LOG DEPTH (ft) U.S.C.S. TESTS MATERIAL DESCRIPTION 0 63.9 0.1 Topsoil SS 8-5-3-3 Light Gray, fine-grained Quartz SAND with cemented sand particles. (Munsell SP 1 (8) 10YR7/2) (Fill) 2.5 61.5 SS 6-4-3-4 Very Dark Brown fine-grained Silty SAND (SM) with trace roots (<5%). (Munsell SM 2 (7) 10ÝR2/2) Proposed Culvert Invert Elevation: 60 feet 4.0 Very Dark Brown, moist, fine-grained Silty SAND. (Munsell 10YR2/2) 5 SS 4-4-3-4 SM (7) 3 6.0 58.0 Very Dark Gray, moist, fine-grained Quartz SAND with SILT. (Munsell 10YR3/1) SP-SS 3-5-4-6 SM 4 (9) 8.0 56.0 Light Gray to Dark Gray, fine-grained Quartz SAND with SILT. (Munsell 10YR7/2 to SS 3-4-5-11 SP-Munsell 10YR4/1) 5 (9) SM 10 10.0 🗸 54.0 SC Light Gray, wet, fine-grained Clayey SAND. (Munsell 10YR7/1) SS 14-12-13 MC = 14% 6 (25)#200 = 19% 15 15.0 49.0 SP Light Gray, moist, fine-grained Quartz SAND. (Munsell 10YR7/2) SS 7-6-4 7 (10)20 20.0 44.0 SM LL = NPLight Gray, moist fine-grained Silty SAND. (Munsell 10YR7/2) SS 9-5-8 PL = NP 8 (13) 25 25.0 39.0 PI = NP Bottom of borehole at 25.0 feet.

#### LEGEND:

MC=Moisture Content LL= Liquid Limit PL= Plastic Limit PI= Plasticity Index OC= Organic Content NP= Not Plastic #200= Percent passing #200 sieve

 $\bigtriangledown$  = Apparent Water Table

W	Ό	00	<b>J</b> .			BORING NUMBER 2018-SPT-3 PAGE 1 OF 1
			Nater Management	Distri	ct (SJ	JRWMD) PROJECT NAME Prel. Design - Duda Pumps, Structures, and Levee Imp
PROJEC		<b>IBER</b> 600	550X3			PROJECT LOCATION Lake County and Orange County, FL
DATE ST	ARTE	D 9/24/18	COMF	LETE	<b>D</b> _9/	/24/18 GROUND ELEVATION _64 ft HOLE SIZE _2.75 inches
DRILLIN	G CON	TRACTOR	AmDrill, Inc.		-	LOCATION N1586082.56 , E442291.86
DRILLING	G MET	HOD _Stan	dard Penetration / M	lud Ro	tary	GROUND WATER LEVEL AT TIME OF DRILLING 4.00 ft / Elev 60.00 ft
LOGGED	BY E	G	CHEC	KED E	<b>BY</b> _A	AC HOLE COMPLETION backfilled with cuttings and bentonite chips
NOTES	Culver	<u>t 2: SW Cel</u>	I to SE Duda Proper	ty Can	al, Cu	ulvert 3: SW Duda Cell to Duda Property Canal, Culvert 4: SE Duda Cell to Duda Proprty Canal
o DEPTH (ft)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION
	SS 1	7-5-6-8 (11)		SM		Grayish Brown to Very Dark Grayish Brown, fine-grained Silty SAND with trace gravel (<3/8"). (Munsell 10YR5/2 to Munsell 10YR3/2) (Fill)
$\overline{1}$	ss	8-6-9-9		SP- SM		Light Brownish Gray, fine-grained Quartz SAND with Silt. (Munsell 10YR6/2) (Fill) 61.
f 1/\	2	(15)				Dark Brown wet woody spongy mostly organic (< 30% fibers) Silty SAND
5	SS 3	6-6-5-5 (11)	MC = 538% LL = NP PL = NP	SМ		Proposed Culvert Invert Elevation: 60 fee
E IV	ss	6-4-8-8	PI = NP OC = 91%			7.0 57
ĺμ	4	(12)		SM		B.0 Dark Gray, wet, fine-grained Silty SAND. (Munsell 10YR4/1) 56.
$ \left[ - \right] $	SS 5	3-4-8-7 (12)		SP		Light Brown, wet, fine-grained Quartz SAND with trace Silt. (Munsell 10YR4/3)
		(12)				10.0 54
  <u>15</u>	SS 6	8-12-14 (26)	MC = 20% #200 = 2%	SP		Light Gray, wet, fine-grained Quartz SAND. (Munsell 10YR7/2)
  <u>20</u>	SS 7	12-16-19 (35)				20.0 44. Bottom of borehole at 20.0 feet.
LEGEND	D:					

MC=Moisture Content LL= Liquid Limit PL= Plastic Limit PI= Plasticity Index OC= Organic Content NP= Not Plastic #200- Bercent passing

#200= Percent passing #200 sieve  $\nabla$  = Apparent Water Table

#### **BORING NUMBER 2018-SPT-4** PAGE 1 OF 1 CLIENT St. Johns River Water Management District (SJRWMD) **PROJECT NAME** Prel. Design - Duda Pumps, Structures, and Levee Imp PROJECT NUMBER 600550X3 PROJECT LOCATION Lake County and Orange County, FL DATE STARTED \_9/24/18 **COMPLETED** 9/24/18 GROUND ELEVATION \_68 ft HOLE SIZE 2.75 inches DRILLING CONTRACTOR Amdrill, Inc. LOCATION N1586292.7, E442427.69 $\bigtriangledown$ GROUND WATER LEVEL AT TIME OF DRILLING 4.00 ft / Elev 64.00 ft DRILLING METHOD Standard Penetration / Mud Rotary LOGGED BY EG CHECKED BY AC HOLE COMPLETION backfilled with cuttings and bentonite chips NOTES SAMPLE TYPE NUMBER BLOW COUNTS (N VALUE) GRAPHIC LOG DEPTH (ft) U.S.C.S. TESTS MATERIAL DESCRIPTION 0 Light Brownish Gray, fine-grained Quartz SAND with Silt. (Munsell 10YR6/2) (Fill) 30-40-34-SS SP-23 SM 1 (74) 2.0 66.0 Dark Gray fine-grained Quartz SAND with Silt. (Munsell 10YR4/1) (Fill) 15-14-10-SS SP-13 SM 2 (24) 4.0 🗸 64.0 MC = 606% Very Dark Gravish Brown, wet, spongy, woody, mostly organic (~30% fibers) Silty 5 SS 2-2-3-5 LL = NP SAND. (Munsell 10YR3/2) (5) 3 PL = NP PI = NP SM SS 2-2-1-2 OC = 90% 4 (3) SS 5-8-4-6 59.0 9.0 5 (12) Brown, wet, CLAY with fine-grained SAND. (Munsell 10YR4/3) CL 10 10.0 58.0 CH LL = 74 Light Gray CLAY with fine grained Sand. (Munsell 10YR7/2) SS 3-3-4 PL = 20 6 (7) 15 15.0 53.0 PI = 54

Light Gray, fine-grained Quartz SAND with Clay. (Munsell 10YR7/2)

Bottom of borehole at 20.0 feet.

48.0

#### LEGEND:

20

MC=Moisture Content

SS

7

12-19-33

(52)

LL= Liquid Limit

PL= Plastic Limit

PI= Plasticity Index

OC= Organic Content

NP= Not Plastic

#200= Percent passing #200 sieve

SC

MC = 14% #200 = 19%

 $\bigtriangledown$  = Apparent Water Table

No.         SS         3-2-2-3         OH         CC2.5         Light Gray, Very Dark Brown, woody ORANC SILT with buried debris. (Munsell 10YR6/4)         61.0           5         -2        4        4         SM         Light Gray, Very Dark Brown, wet, fine-grained Silty SAND. (Munsell 10YR6/2)         Dark Gray to Dark Brown, wet, fine-grained Silty SAND. (Munsell 10YR3/3)         6.0         57.5           5         SS         3-2-2-3         (A)         PL = NP PL = NP PL = NP PL = NP PL = NP PL = NP         SM         Dark Gray to Dark Brown fine-grained SAND with Silt. (Munsell 10YR3/3)         57.5           6.0         SS         3-44-6         SN         SN         Dark Gray to Dark Brown, moist, fine-grained SAND with Silt. (Munsell 10YR5/3)         64.5           10         SS         3-44-6         SN         SN         9.0         Light Brown, moist, fine-grained Silty SAND. (Munsell 10YR5/3)         64.5           10         SS         3-84-10         SN         SN         15.0         48.5           15.0         SS         3-8-10         LL = NP PL = NP Pl = NP         SN         15.0         48.5           20         SS         10-11-18         MC = 23% #200 = 5%         SP         Light Brownish Gray, moist, fine-grained Quartz SAND. (Munsell 10YR6/2)         58.5           20         SS					4				BORING NUMBER 2018-SPT- PAGE 1 OF		
DATE STARTED         9/24/18         COMPLETED         9/24/18         GROUND ELEVATION         63.5 ft         HOLE SIZE         2.75 inches           DRILLING CONTRACTOR         Andrill, Inc.         UCCATION N1589170.83, E442763.65         UCCATION N1589170.83, E442763.65         UCCATION N1589170.83, E442763.65         UCCATION N1589170.83, E442763.65           DRILLING METHOD         Standard Penetration / Mud Rotary         CROUND WATER LEVEL AT TIME OF DRILLING 2.50 ft / Elev 61.00 ft         HOLE SOURDETTON backfilled with outtings and bentonite drips           NOTES         Duda Pump Station/ Guivert 5: SE Duda Property Cell to NE Duda Property Cenal         MATERIAL DESCRIPTION         61           V         SS         3-2-33         TESTS         0         0         0         0         0         0         61           V         SS         3-2-33         TESTS         0						Distri	ct (SJF	RWMD) PR	OJECT NAME Prel. Design - Duda Pumps, Structures, and Levee Imp		
DRILLING CONTRACTOR         Amdrill, Inc.         LOCATION N1580170.83, E442783.65           DRILLING METHOD         Standard Penetration / Mud Rotary         COCOUND WATER LEVEL AT TIME OF DRILLING 2.50 ft / Elev 61.00 ft           LOGGED BY         EG         CHECKED BY AC         MOLE COMPLETION backfilled with cuttings and bentonite chips           NOTES         Duda Pump Station / Cutvert 5: SE Duda Property Call to NE Duda Property Canal         MOLE COMPLETION backfilled with cuttings and bentonite chips           VETS         Duda Pump Station / Cutvert 5: SE Duda Property Call to NE Duda Property Canal         MATERIAL DESCRIPTION           0         SS         3-2-3-3         G         G           0         SS         3-2-2-3         OH         Grayleh Brown to Dark Brown, wet, ORGANIC SILT with comented sand particles. (Munsel 10YR3/2)         G11.00           0         SS         3-2-2-3         OH         Z2         Light Brown, woody ORGANIC SILT with puried debris. (Munsel 10YR2/2)         G13.00           10         SS         3-2-2-3         MC = 669%         SM         Dark Brown, wet, woody. spongy, mostly organic SIN SAND. (Munsell 10YR2/2)         G13.00           10         SS         3-4-44         O         SM         Dark Gray to Dark Brown, wet, woody. spongy, mostly organic SIN SAND. (Munsell 10YR4/1 to Munsel 10YR3/3)         S5.5           10         SS	PRO.	JECI		MBER 600	550X3			PR	DJECT LOCATION _ Lake County and Orange County, FL		
DRILLING METHOD         Standard Penetration / Mud Rotary	DATE	ST/	ARTE	<b>D</b> <u>9/24/18</u>	COMP	LETE	D _9/2	4/18 GR	OUND ELEVATION _63.5 ft HOLE SIZE _2.75 inches		
LOGGED BY       EG       CHECKED BY       AC       HOLE COMPLETION backfilled with cuttings and bentonite chips         NOTES       Duda Pump Station/ Cutvert 5: SE Duda Property Cell to NE Duda Property Cell to NE Duda Property Canal       MATERIAL DESCRIPTION $H_{ab}^{ab}$ <	DRILI	ling	CON	TRACTOR	Amdrill, Inc.			LO	CATION <u>N1586170.83</u> , E442763.65		
NOTES         Duda Pump Station/ Culvert 5: SE Duda Property Cell to NE Duda Property Cented           T         T         Station/ Culvert 5: SE Duda Property Cell to NE Duda Property Canal           T         Station/ Culvert 5: SE Duda Property Cell to NE Duda Property Canal         MATERIAL DESCRIPTION           0         Station/ Culvert 5: SE Duda Property Cell to NE Duda Property Canal         MATERIAL DESCRIPTION           0         Station/ Culvert 5: SE Duda Property Cell to NE Duda Property Canal         MATERIAL DESCRIPTION           0         Station/ Culvert 5: SE Duda Property Canal         MATERIAL DESCRIPTION           0         Station/ Culvert 5: SE Duda Property Canal         Station Culvert 5: SE Duda Property Canal           0         Station Culvert 5: SE Duda Property Canal         Material 107R3/2           0         Station Culvert 5: SE Duda Property Canal         Grayish Brown to Dark Brown, wet, ORGANIC SILT with cemented sand particles.           0         Station Culvert 5: Se Duda Property Canal         Station Culvert 5: Set Station Colleging           5         Station Culvert 5: Set Station Colleging         Station Colleging         Station Colleging           5         Station Culvert 5: Set Station Colleging         Station Colleging         Station Colleging           6         Station Colleging         Station Colleging         Station Colleging         Station Colleging	DRILI	ING	MET	HOD Stan	dard Penetration / M	ud Ro	tary	<u> </u>	GROUND WATER LEVEL AT TIME OF DRILLING 2.50 ft / Elev 61.00 ft		
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	LOGO	GED	BY _	EG	CHEC	KED I	<b>BY</b> <u>A</u>	но	LE COMPLETION backfilled with cuttings and bentonite chips		
0	NOTES Duda Pump Station/ Culvert 5: SE Duda Property Cell to NE Duda Property Canal										
A         SS         3-2-3-3 (5)         MC = 669% (L = NP PI = NP         MC = 669% CC = 92% SM         MC = 669% 6.0         MC = 669% CC = 92% SM         MC = 669% CC = 92% SM         MC = 669% 6.0         MC = 669% CC = 92% SM         MC = 669% CC		SAMPI F TYPF	NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG				
SS         3-2-2-3         Clight Gray, Very Dark Brown, wet, fine-grained Silty SAND. (Munsell 10YR2/2)           5         SS         3-2-2-3         MC = 669%           6         SS         3-2-2-3         MC = 669%           7         4         8         MC = 669%           8         3-2-2-3         MC = 669%         Light Gray, Very Dark Brown, wet, fine-grained Silty SAND. (Munsell 10YR2/2)           7         8         3-2-2-3         MC = 669%         5           6.0         9.0         Dark Brown, wet, woody, spongy, mostly organic Silty SAND. (Munsell 10YR3/3)           6.0         9.0         Dark Gray to Dark Brown fine-grained SAND with Silt. (Munsell 10YR4/1 to Munsell 10YR5/3)           8.0         SM         8.0         9.0         Light Brown, moist, fine-grained Silty SAND. (Munsell 10YR5/3)           10         SS         3-4-4-6         SM         9.0         Light Brown, moist, fine-grained Silty SAND. (Munsell 10YR5/3)           115         SS         3-8-19         LL = NP         SM         15.0         48.5           115         SS         10-11-18         MC = 23%         SP         Light Brownish Gray, moist, fine-grained Quartz SAND. (Munsell 10YR6/2)           20         X         SS         11-12-14         SP         25.0 <t< td=""><td></td><td><math>\mathbb{N}</math></td><td></td><td></td><td></td><td>он</td><td></td><td>(Munsell 10Y 2.0</td><td>(R5/2 to Munsell 10YR3/3)</td><td>61.5</td></t<>		$\mathbb{N}$				он		(Munsell 10Y 2.0	(R5/2 to Munsell 10YR3/3)	61.5	
A       B       Dark Gray to Dark Brown, wet, woody, spongy, mostly organic Silty SAND. (Munsell 10YR3/3)       A       A       B       B       Dark Gray to Dark Brown, moist, fine-grained SAND with Sit. (Munsell 10YR4/1 to Munsell 10YR4/1 to Munsell 10YR3/3)       B       B       B       D       B       D       Dark Gray to Dark Brown, moist, fine-grained Silty SAND. (Munsell 10YR5/3)       S		М	SS	3-2-2-3			444			61.0	
5       XS       3.2-2-3 3       (4)       LL = NP PL = NP       SM       Image: delta of the object of	[	$\mathbb{A}$	.2	(4)		<u>_SM</u> .				59.5	
PI = NP 4       P1 = NP 0C = 92%       SP- SM       Dark Gray to Dark Brown fine-grained SAND with Silt. (Munsell 10YR 4/1 to Munsell 10YR3/3)         SS       3-4-4-6 (8)       SM       SM       9.0       Light Brown, moist, fine-grained Silty SAND. (Munsell 10YR7/2)         SM       SM       9.0       Light Gray tine-grained Silty SAND. (Munsell 10YR7/2)       54.5         SM       SM       SM       15.0       Light Gray fine-grained Silty SAND. (Munsell 10YR7/2)         SS       3-8-19 6       1.L = NP PL = NP Pl = NP       SM       15.0         SS       10-11-18 7       MC = 23% (29)       SP       Light Brownish Gray, moist, fine-grained Quartz SAND. (Munsell 10YR6/2)         SP       SS       11-12-14 25       SS       11-12-14 25.0       SS       25.0	5	$\mathbb{N}$			LL = NP	SM				57 5	
SS       3-4-4-6       SM       SM       9.0       Light Brown,moist, fine-grained Silty SAND. (Munsell 10YR5/3)       54.5         10       SS       3-8-19       LL = NP       Light Gray fine-grained Silty SAND. (Munsell 10YR7/2)       54.5         15       SS       3-8-19       LL = NP       PL = NP       15.0       48.5         20       SS       10-11-18       MC = 23%       15.0       Light Brownish Gray, moist, fine-grained Quartz SAND. (Munsell 10YR6/2)         20       SS       10-11-18       MC = 23%       SP       Light Brownish Gray, moist, fine-grained Quartz SAND. (Munsell 10YR6/2)         20       SS       11-12-14       SP       SP       25.0       38.5								Dark Gray to Munsell 10Y	Dark Brown fine-grained SAND with Silt. (Munsell 10YR 4/1 to R3/3)		
10       5       (8)       10-11-18       LL = NP       LL = NP       Light Gray fine-grained Silty SAND. (Munsell 10YR7/2)         15       SS       3-8-19       LL = NP       15.0       48.5         15       SS       10-11-18       MC = 23%       15.0       48.5         20       SS       10-11-18       MC = 23%       15.0       Light Brownish Gray, moist, fine-grained Quartz SAND. (Munsell 10YR6/2)         20       SS       10-11-18       MC = 23%       SP       Light Brownish Gray, moist, fine-grained Quartz SAND. (Munsell 10YR6/2)         20       SS       11-12-14       SP       25.0       38.5		$\mathbb{N}$	66	2446		SM		Light Brown	moist_fine-grained Silty SAND_(Munsell 10YR5/3)		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	 									<u>54.5</u>	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		$\mathbb{N}$									
	  - 20  		SS 7 SS	10-11-18 (29) 11-12-14	PI = NP MC = 23%	SP		Light Brownis	sh Gray, moist, fine-grained Quartz SAND. (Munsell 10YR6/2)	48.5	
	25	VN	Ö	(20)				25.0	Bottom of borehole at 25.0 feet.	38.5	

LEGEND:

MC=Moisture Content MC=Moisture Content LL= Liquid Limit PL= Plastic Limit PI= Plasticity Index OC= Organic Content NP= Not Plastic #200= Percent passing #200 sieve

 $\bigtriangledown$  = Apparent Water Table

# **BORING NUMBER 2018-SPT-6**

PAGE 1 OF 1

 $\mathbf{O}\mathbf{O}$ CLIENT St. Johns River Water Management District (SJRWMD) P \_ P PROJECT NUMBER 600550X3 DATE STARTED \_9/24/18 \_\_\_\_\_ COMPLETED \_9/24/18 \_\_\_\_\_ LOCATION <u>N1586219.4</u>, E447803.99 DRILLING CONTRACTOR Amdrill, Inc. DRILLING METHOD Standard Penetration / Mud Rotary 🛛 🖓 GROUND WATER LEVEL AT TIME OF DRILLING 2.00 ft / Elev 61.50 ft

ROJECT NAME	Prel. Design - Duda Pumps, Structures, and Levee Imp
ROJECT LOCAT	ION _Lake County and Orange County, FL

GROUND ELEVATION \_63.5 ft HOLE SIZE \_2.75 inches

LOGGED BY EG CHECKED BY AC HOLE COMPLETION backfilled with cuttings and bentonite chips

NOTES

o DEPTH (ft)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	
	SS 1	5-4-3-3 (7)		SM		Dark Grayish Brown, moist, fine-grained Silty SAND with trace roots. (Munsell 10YR4/2) (Fill) 2.0 ▽	61.5
	SS 2	2-2-2-2 (4)	MC = 594% LL = NP PL = NP			Very Dark Brown, wet, woody, spongy, mostly organic Silty SAND with buried debris. (Munsell 10YR2/2)	
5	SS 3	2-2-2-2 (4)	PI = NP OC = 93%	SM			
	SS 4	2-6-5-3 (11)		SP		6.5 Dark Gray fine-grained Quartz SAND with trace Silt. (Munsell 10YR4/1)	57.0
		(11)				8.0	55.5
	SS 5	3-2-2-5 (4)	MC = 22% #200 = 15%	SM		Gray, moist, fine-grained Silty SAND. (Munsell 10YR5/1)	53.5
      	SS 6	8-6-9 (15)		SP		Light Gray, wet, fine-grained Quartz SAND. (Munsell 10YR6/1)	
	SS 7	6-7-8 (15)				20.0	43.5

LEGEND:

MC=Moisture Content

LL= Liquid Limit

PL= Plastic Limit

PI= Plasticity Index

OC= Organic Content NP= Not Plastic

#200= Percent passing #200 sieve

 $\bigtriangledown$  = Apparent Water Table

Bottom of borehole at 20.0 feet.

#### BORING NUMBER 2018-SPT-7 PAGE 1 OF 1 CLIENT St. Johns River Water Management District (SJRWMD) **PROJECT NAME** Prel. Design - Duda Pumps, Structures, and Levee Imp PROJECT NUMBER 600550X3 PROJECT LOCATION Lake County and Orange County, FL DATE STARTED 9/24/18 **COMPLETED** 9/24/18 GROUND ELEVATION 67.7 ft HOLE SIZE 2.75 inches DRILLING CONTRACTOR Amdrill, Inc. LOCATION N1587097.39, E452900.65 DRILLING METHOD Standard Penetration / Mud Rotary LOGGED BY EG CHECKED BY AC HOLE COMPLETION backfilled with cuttings and bentonite chips NOTES Culvert 7: Canal Rd. to Phase 7 SAMPLE TYPE NUMBER BLOW COUNTS (N VALUE) GRAPHIC LOG DEPTH (ft) U.S.C.S. TESTS MATERIAL DESCRIPTION 0 Yellowish Brown, moist, fine-grained Clayey SAND. (Munsell 10YR5/4) (Fill) SS 4-4-5-5 SC 1 (9) 2.0 65.7 Yellowish Brown to Gray fine-grained SAND with Clay. (Munsell 10YR5/4 to SS 3-7-6-9 SP-Munsell 10YR5/1) (Fill) SC 2 (13) 4.0 63.7 Yellowish Brown fine-grained Sandy CLAY. (Munsell 10YR5/4) (Fill) SS 5-5-7-6 MC = 29% 5 CL #200 = 55% (12) 3 6.0 61.7 Dark Brown, moist, fine-grained SAND with Silt. (Munsell 10YR3/3) (Fill) 12-3-4-3 SP-SS Proposed Culvert Invert Elevation: 60 feet 59:7 4 (7) SM 11118.0-MC = 459% Very Dark Brown, wet, woody (<30% fibers), spongy, mostly organic Silty SAND. SS 4-4-5-5 LL = NP (Munsell 10YR2/2) 5 (9) PL = NP 10 PI = NP OC = 91% SM

Light Brownish Gray, moist, fine-grained Silty SAND. (Munsell 10YR6/2)

Bottom of borehole at 20.0 feet.

52.7

47.7

15.0

SM

MC = 36% #200 = 14%

LEGEND:

15

20

MC=Moisture Content

SS

7

SS

6

2-6-6

(12)

3-6-8

(14)

LL= Liquid Limit

PL= Plastic Limit

PI= Plasticity Index

OC= Organic Content

NP= Not Plastic

#200= Percent passing #200 sieve

 $\bigtriangledown$  = Apparent Water Table

V		0	00	9				В	ORING NU		8-SPT-8 PAGE 1 OF 1
				Water Managemen	t Distri	ct (S I		PROJECT NAME Prel	Docian Dudo Pum	as Structures and	ovoo Imp
	_		<b>IBER</b> 600		C DIStri			PROJECT LOCATION			
			D_9/24/18			-/ a/	24/18	GROUND ELEVATION		HOLE SIZE 2.7	75 inches
				· · ·							
				dard Penetration / M			с				
LOGG							<u> </u>		ackinied with cuttings		<u> </u>
NOTES _Culvert 6: Duda Property Cell to Canal Rd.											
o DEPTH (ft)	SAMDI E TVDE	NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG		MATE	RIAL DESCRIPTION	I	
	М	SS	2-3-4-5				Brown, r	moist fine-grained Sandy	CLAY. (Munsell 10YF	R5/3) (Fill)	
	Д	1	(7)		CL						
	M	SS	5-4-5-5				3.0				64.0
	Д	2	(9)				Light Ye	llowish Brown fine-graine	d Clayey SAND. (Mu	nsell 10YR6/4) (Fill)	
5	M	SS	4-4-4-4	MC = 45%	SC						
	$\langle \rangle$	3	(8)	#200 = 29%			6.0				61.0
	Ŋ.	SS	5-2-3-3				Very Da	rk Brown, woody (<30% f I 10YR2/2)			
	$\langle \rangle$	4	(5)	NO 1019/	4				Propos	sed Culvert Invert E	levation: 60 feet
	X	SS 5	4-2-2-3 (4)	MC = 494% LL = NP PL = NP PI = NP OC = 75%	SM						
  _ 15 _	Х	SS 6	3-2-2 (4)				15.0				52.0
		SS	3-5-14	LL = NP	SM		Light Gr	ay, chalky, moist, fine-gra	ined Silty SAND. (Mu	insell 10YR7/1)	
20	Ŵ	7	(19)	PL = NP PI = NP			20.0				47.0
					/			Bottom	of borehole at 20.0 fe	eet.	
LEG MC=			Content								

MC=Moisture Content LL= Liquid Limit PL= Plastic Limit PI= Plasticity Index OC= Organic Content NP= Not Plastic #200= Percent passing #200 sieve

V	/0	000	<b>J</b> .				BORING NUMBER 2020-SP PAGE 1 OF	
			Vater Managemen	ıt Distri	ct		PROJECT NAME _ Duda Water Storage Improvements	
		MBER 600	-				PROJECT LOCATION Apopka, FL	
			COM	IPLETE	ED 2/2	27/20		
			ndard Penetration					
			CHE					
	S							
o DEPTH (ft)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION	
Ŭ	AU 1			SP		Dark	prown, poorly graded fine grained quartz SAND, with organics, trace silt,	63.0
	AU		MC = 17%		11/		rock fragments, moist (Munsell 10YR 2/2) greenish gray, CLAYEY SAND, fine grained quartz, with rock fragments,	0
	2 AU		#200 = 20%	- sc		moist	(Munsell 10YR 5/2)	
	AU		#200 - 20%		<u> </u>	3.0 Dark	prown to brown, very loose, SANDY ORGANIC SILT (PEAT), fine grained	61.0
L -	4				E		z, spongy, moist (Munsell 10YR 2/1)	
5	AU 5				[	Drillin	g fluid used below 5 feet Average Bottom Elevation of Proposed Culvert (EL	58.8
† ·	V ss	0-1-1-1			╞═╼╛	+	t of hammer for 6-inches, 1,1,1 (WOH/6", 1,1,1)	
	6	(2)		OL	E	-		
					[	1	us, less than 30% fibers, from 5 to 9 feet	
		0-0-1-1 (1)				weigh	t of hammer for 12-inches, 1,1 (WOH/12",1,1)	
 _ 10	ss 8	1-1-2-2 (3)		CL		9.0 Greer	nish gray, soft, SANDY CLAY, fine grained quartz (Munsell 10YR 5/2)	55.0
	$\square$	(0)				11.0		53.0
L .	V  ss	4-7-12-14		SP		Light 10YR	gray, medium dense, poorly graded fine grained quartz SAND (Munsell 4/2)	
	9	(19)				13.0	, ,	51.0
  15	SS 10	2-3-3-6 (6)	LL = 83 PL = 20 PI = 63	СН			nish gray, firm, SANDY CLAY, fine grained quartz (Munsell 10YR 5/2)	
						16.8		47.3
	-					Light	brown, medium dense, poorly graded fine grained quartz SAND with SILT sell 10YR 5/1)	
	V ss	6-10-7						
_ 20	11	(17)						
						- - -		
[				SP-				
	-			SM				
	-					4 		
		9-13-14				dense	e from 21.75 to 26.75 feet	
_ 25	12	(27)						
L -	1							
L						26.8		37.3
-				SP		Light 10YR	brown, dense, poorly graded fine grained quartz SAND, trace silt (Munsell 5/1 to 10YR 4/1)	
30	SS 13	7-13-14 (27)	#200 = 4%					

# BORING NUMBER 2020-SPT-1 PAGE 2 OF 2

CLIENT St Johns River Water Management District

wood.

PROJECT NUMBER 600550x4

PROJECT NAME \_ Duda Water Storage Improvements PROJECT LOCATION Apopka, FL

			000001			
ы DEPTH (ft)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION
						Light brown, dense, poorly graded fine grained quartz SAND, trace silt (Munsell 10YR 5/1 to 10YR 4/1) <i>(continued)</i>
  <u>35</u>  	SS 14	7-14-10 (24) 6-4-5		SP		medium dense from 31.75 to 36.75 feet
40	15	(9)	MC = 25%		40	loose from 36.75 to 40 feet 24.0
						Bottom of borehole at 40.0 feet.
LEGE	ND·					

LEGEND:

MC=Moisture Content

LL= Liquid Limit

PL= Plastic Limit

PI= Plasticity Index

OC= Organic Content NP= Not Plastic

#200= Percent passing #200 sieve

V	/0	00	J.				BORING NUMBER 2020-SPT-2 PAGE 1 OF 2			
CLIEN PROJ DATE DRILL DRILL LOGG	IT <u>St Jo</u> ECT NUN STARTE ING CON	hns River V IBER _600 D _2/27/20 ITRACTOR ITRACTOR IHOD _Star BA	Vater Management 550x4 COM _Amdrill, Inc. idard Penetration /	PLETE	ED _2/	27/20	GROUND ELEVATION         68 ft         HOLE SIZE         4 inches           LOCATION         N1585074.1 , E437990.364			
o DEPTH (ft)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION			
	AU 1		MC = 12%	SP		Brown	es of topsoil and vegetation , poorly graded fine grained quartz SAND, trace silt, trace organics, trace			
	AU 2 AU		OC = 7%			rock fra 2.0 Dark b	agments, moist (Munsell 10YR 2/2) 66.0 rown, SILTY SAND, fine grained quartz, with organics, spongy (Munsell			
  _ 5	3 AU 4 AU 5 SS	0-0-1-1	00 - 778	SM		10YR : Drilling verv lo				
	6	(1)				fiberou 7.0	Is, less than 30% fibers, from 5 to 7 feet 61.0 sh gray, loose, CLAYEY SAND, fine grained quartz (Munsell 10YR 5/2)			
	SS 7	1-2-2-2 (4)				Green	Bottom Elevation of Proposed Culvert (EL. 59.3)			
	SS 8	3-4-5-6 (9)	#200 = 31%	SC		trace r	ock fragments from 7 to 11 feet 57.0			
	ss 9	2-3-4-5 (7)	LL = 218 PL = 69 PI = 149				sh gray, firm, SANDY CLAY, fine grained quartz (Munsell 10YR 5/2)			
 	SS 10	1-2-2-2 (4)		СН						
						16.8 Light b (Munse	rown, medium dense, CLAYEY SAND, fine grained quartz, trace silt ell 10YR 5/1)			
 _ <u>20</u>	ss 11	3-5-7 (12)		SC						
						21.8 Light g SAND	46.3 ray to light brown, medium dense, poorly graded fine grained quartz with SILT (Munsell 10YR 5/1)			
 _ 25	SS 12	6-10-7 (17)	MC = 20%							
				SP- SM						
 30	SS 13	7-6-5 (11)				· · · · · · · · · · · · · · · · · · ·				

# BORING NUMBER 2020-SPT-2 PAGE 2 OF 2

CLIENT St Johns River Water Management District

WOO

PROJECT NAME \_ Duda Water Storage Improvements

PROJ		IBER _600	550x4			PROJECT LOCATION _ Apopka, FL
6 DEPTH 6 (ft)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION
						Light gray to light brown, medium dense, poorly graded fine grained quartz SAND with SILT (Munsell 10YR 5/1) <i>(continued)</i>
	SS 14	6-11-12 (23)		SP-		
				SM		
						dense from 36.75 to 40 feet
40	SS 15	12-13-11 (24)				40.0 28.0
						Bottom of borehole at 40.0 feet.

LEGEND:

MC=Moisture Content

LL= Liquid Limit

PL= Plastic Limit

PI= Plasticity Index

OC= Organic Content NP= Not Plastic

#200= Percent passing #200 sieve

V	/0	00	9				BORING NUMBER 2020-SPT-3 PAGE 1 OF 2
CLIEN PROJ DATE DRILL DRILL LOGG	NT <u>St Jo</u> ECT NUN STARTE LING COM	hns River V IBER 600 ED 2/25/20 NTRACTOR THOD Star BA	Vater Managemer 550x4 CON Amdrill, Inc.	IPLETE	ED _2/2 Rotary	25/20	PROJECT LOCATION _Apopka, FL         GROUND ELEVATION _63.5 ft       HOLE SIZE _4 inches         LOCATION _N1586275.453 , E442248.9374
o DEPTH (ft)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION
	AU 1 AU 2 AU 3 AU		#200 = 42%	SC SM		1.0 3.0	Light greenish gray, CLAYEY SAND, fine grained quartz, with rock fragments, trace silt, trace organics, moist (Munsell 10YR 5/2) 62. Brown, SILTY SAND, fine grained quartz, with rock fragments, with organics, moist (Munsell 10YR 2/1) 60. Dark brown, SANDY ORGANIC SILT (PEAT), fine grained quartz, spongy,
 5 	4 AU 5 SS 6	1-0-1-1	OC = 61%	OL			moist (Munsell 10YR 2/1) Fiberous, less than 30% fibers, from 4 to 9 feet 1 blow for 12-inches, 1,1 (1/12", 1,1) Bottom Elevation of Proposed Culvert (EL. 57.0
  _ <u>10</u>	SS 7 SS 8	2-0-1-1 (1) 1-2-3-3 (5)				9.0	very loose from 5 to 9 feet 2 blows for 12-inches, 1,1 (2/12", 1,1) Light greenish gray to white, firm, SANDY CLAY, fine grained quartz (Munsell 10YR 5/2) trace shell fragments from 9 to 11 feet
	SS 9	2-3-3-2 (6) 14-33-32-	#200 = 79%	- CH		13.0	50.: Light brown to light gray, very dense, poorly graded fine grained quartz SAND
 _ <u>15</u> 	SS 10	34 (65)		SP		16.8	(Munsell 10YR 5/1) 46.
  <u>20</u>	SS 11	7-9-7 (16)	MC = 17%	_			Light gray to light brown to brown, medium dense, poorly graded fine grained quartz SAND with SILT (Munsell 10YR 4/1)
   25	SS 12	5-4-4 (8)		SP- SM			loose from 21.75 to 40 feet
	- - - - - - - - - - - - - - - - - - -	2-2-2 (4)					

## **BORING NUMBER 2020-SPT-3**

PAGE 2 OF 2

CLIENT St Johns River Water Management District

VOO

PROJECT NAME Duda Water Storage Improvements

PROJ		IBER _600	550x4			PROJECT LOCATION Apopka, FL
6 DEPTH 6(ft)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION
  - 35     - 40	SS 14 SS 15	3-3-2 (5) 2-2-2 (4)	MC = 25%	SP- SM		Light gray to light brown to brown, medium dense, poorly graded fine grained quartz SAND with SILT (Munsell 10YR 4/1) <i>(continued)</i> 40.0 23.5
						Bottom of borehole at 40.0 feet.

LEGEND:

MC=Moisture Content

LL= Liquid Limit

PL= Plastic Limit

PI= Plasticity Index

OC= Organic Content NP= Not Plastic

#200= Percent passing #200 sieve

V	VO	00	<b>d</b> .				BORING NUMBER 2020-SPT-4 PAGE 1 OF 2
CLIEN PROJ DATE	NT <u>St Jo</u> Ject Nun Starte	hns River V IBER _600 D _2/26/20	Vater Managemen 550x4 COM	PLETE	ED _2/	26/20	PROJECT LOCATION _Apopka, FL         GROUND ELEVATION _63.5 ft         HOLE SIZE _4 inches
			Amdrill, Inc.				
LOGO							HOLE COMPLETION backfilled with cuttings and bentonite chips
o DEPTH (ft)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION
	AU 1 AU 2		MC = 28%	SP- SC SP- SM		1.0 Light g	es of topsoil and vegetation reenish gray, poorly graded fine grained quartz SAND with CLAY, with agments, trace silt, moist (Munsell 10YR 5/2) , poorly graded fine grained quartz SAND with SILT, with organics, trace
  _ 5	AU 3 AU 4 AU 5			- OL		Dark b moist (	, poorly graded line grained quartz SAND with SILT, with organics, trace agments, moist (Munsell 10YR 2/2) rown, SANDY ORGANIC SILT (PEAT), fine grained quartz, spongy, (Munsell 10YR 2/1) is, less than 30% fibers, from 3 to 7 feet i fluid used below 5 feet
	ss 6	1-1-1-1 (2)	OC = 91%			very lo	ose from 5 to 8 feet Bottom Elevation of Proposed Culvert (EL. 57.0)
	ss s	0-2-3-2				8.0	of hammer for 6-inches, 2,3,2 (WOH/6", 2, 3, 2)
	7	(5)		SP		9.0 5/1)	, loose, poorly graded fine grained quartz SAND, trace silt (Munsell 10YR
<u>    10    </u> -     -	SS 8	1-1-2-2 (3)	MC = 33%	- сн		Light g roots, f	reenish gray to white, firm, SANDY CLAY, fine grained quartz, trace trace rock fragments (Munsell 10YR 5/2)
	SS 9	1-2-3-2 (5)					
  _ <u>15</u>	ss 10	10-28-28- 35 (56)	#200 = 6%	SP- SM			50.5 prown, very dense, poorly graded fine grained quartz SAND with SILT ell 10YR 5/1)
	-			SIVI			
	-					Light g	46.٤ ray to brown, medium dense, poorly graded fine grained quartz SAND LT, trace clay (Munsell 10YR 4/1)
	SS 11	5-10-13 (23)	-				
	-						rom 21.75 to 40 feet
	- M ss	4-4-4	_	SP- SM			
_ 25	12	(8)					
	-						
	SS 13	2-2-2 (4)					

## **BORING NUMBER 2020-SPT-4**

CLIENT St Johns River Water Management District

VOO

PROJECT NAME Duda Water Storage Improvements

Bottom of borehole at 40.0 feet.

PROJ		IBER _600	550x4			PROJECT LOCATION _ Apopka, FL	
6 DEPTH 6(ft)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	
  - 35    - 40	SS 14 SS 15	3-2-2 (4) 4-3-3 (6)		SP- SM		Light gray to brown, medium dense, poorly graded fine grained quartz SAND with SILT, trace clay (Munsell 10YR 4/1) <i>(continued)</i> 40.0	23.5

LEGEND:

MC=Moisture Content

LL= Liquid Limit

PL= Plastic Limit

PI= Plasticity Index

OC= Organic Content NP= Not Plastic

#200= Percent passing #200 sieve

WC	00	<b>d</b> .				BORING NUMBER 2020-SPT PAGE 1 OF			
CLIENT St Ja PROJECT NU DATE STARTI DRILLING CO DRILLING ME	Dhns River V MBER 600 ED 2/25/20 NTRACTOR THOD Star BA	Vater Managemen 550x4 COM Amdrill, Inc. ndard Penetration	IPLETE	ED _2/2 Rotary	25/20	PROJECT LOCATION _Apopka, FL         GROUND ELEVATION _67 ft       HOLE SIZE _4 inches         LOCATION _N1586247.921 , E452625.998			
DEPTH (ft) SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION			
0 AU AU 2 AU 3 AU 5 5 5 5 5 5 5 6 7 10 8 8 7	1-1-1-1 (2) 0-1-1-1 (2) 2-2-1-1 (3) 1-2-1-1 (3)	#200 = 72% OC = 85% MC = 51%	SP- SC CL OL		1.0 Light to loamy 2.0 Light to 5/1) Dark to spong fiberou Drilling very to weight	of topsoil and vegetation prown, poorly graded fine grained quartz SAND with CLAY, trace silt, moist (Munsell 10YR 2/2) prown, SANDY CLAY, fine grained quartz, trace silt, moist (Munsell 10YR rown to brown, SANDY ORGANIC SILT (PEAT), fine grained quartz, y, moist (Munsell 10YR 2/1) is, less than 30% fibers, from 3 to 9 feet g fluid used below 5 feet nose from 5 to 11 feet to f hammer for 6-inches, 1, 1, 1 (WOH/6", 1, 1, 1) Bottom Elevation of Proposed Culvert (EL. ock fragments from 9 to 11 feet prown to light greenish gray, very loose, poorly graded fine grained quartz with CLAY, loamy, with shell fragments (Munsell 10YR 5/1)	<u>66.(</u> <u>65.(</u> <u>57.0)</u> <u>56.(</u>		
	(3) 2-2-5-9 (7)	MC = 20%	SP- SC		16.8	from 13 to 15 feet	50.3		
ss 20 11	7-12-14 (26)		sc		(Muns 21.8 Light c	gray, loose, poorly graded fine grained quartz SAND with SILT (Munsell	45.3		
	3-3-2 (5) 2-2-4 (6)	MC = 32%	SP- SM		10YR	5/1)			

## **BORING NUMBER 2020-SPT-5**

CLIENT St Johns River Water Management District

wood.

PROJECT NAME \_ Duda Water Storage Improvements

PROJ	ECT NUN	IBER _600	550x4			PROJECT LOCATION Apopka, FL						
6 DEPTH 6 (ft)	SAMPLE TYPE NUMBER	BLOW COUNTS (N VALUE)	TESTS	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION						
	_			SP- SM	77777	Light gray, loose, poorly graded fine grained quartz SAND with SILT (Munsell 10YR 5/1) (continued) 31.8	35.3					
  <u>35</u>	SS 14	4-4-3 (7)				Light gray, loose, CLAYEY SAND, fine grained quartz (Munsell 10YR 5/1)						
 - 40 	SS 15	4-4-4 (8)		sc								
 _ 45 	SS 16	4-6-7 (13)	#200 = 16%	-		shell fragments from 43.5 to 45 feet medium dense from 41.75 to 50 feet						
	SS 17	5-6-7 (13)	-			50.0	47.0					
LL= L PL= F PI= P OC= ( NP= 1	END: Moisture C iquid Limi Plastic Lim lasticity Ir Organic C Not Plastic	Content it nit idex Content	200 sieve			50.0 Bottom of borehole at 50.0 feet.	17.0					

#### **BORING NUMBER 2020-PT-1** PAGE 1 OF 1 PROJECT NAME Duda Water Storage Improvements CLIENT St Johns River Water Management District PROJECT NUMBER 600550x4 PROJECT LOCATION Apopka, FL DATE STARTED 2/27/20 COMPLETED 2/27/20 WATER ELEVATION 62 ft \_ HOLE SIZE \_2 inches DRILLING CONTRACTOR Wood LOCATION N1586297.88, E452763.4683 DRILLING METHOD Piston Tube Sampling GROUND WATER LEVEL AT TIME OF DRILLING ----CHECKED BY CS HOLE COMPLETION LOGGED BY BA NOTES SAMPLE TYPE NUMBER GRAPHIC LOG U.S.C.S. DEPTH (ft) TESTS MATERIAL DESCRIPTION 0 6 feet of water Bottom Elevation of Proposed Culvert (EL. 57.0) 5 6.0 6.5 56.0 55.5 NO RECOVERY UD OC = 17% Dark brown to light brown, CLAYEY SAND, fine grained quartz, with organics, wet SC 1 (Munsell 10YR Ž/2) UD 54.0 Bottom of borehole at 8.0 feet. 2 UD 3

#### LEGEND:

MC=Moisture Content LL= Liquid Limit PL= Plastic Limit PI= Plasticity Index OC= Organic Content NP= Not Plastic #200= Percent passing #200 sieve

#### **BORING NUMBER 2020-PT-2** PAGE 1 OF 1 PROJECT NAME Duda Water Storage Improvements CLIENT St Johns River Water Management District PROJECT NUMBER 600550x4 PROJECT LOCATION Apopka, FL DATE STARTED \_2/27/20 COMPLETED \_2/27/20 WATER ELEVATION 62 ft HOLE SIZE 2 inches DRILLING CONTRACTOR Wood LOCATION N1586171.658, E452766.5586 DRILLING METHOD Piston Tube Sampling GROUND WATER LEVEL AT TIME OF DRILLING ----CHECKED BY CS HOLE COMPLETION LOGGED BY BA NOTES SAMPLE TYPE NUMBER GRAPHIC LOG U.S.C.S. DEPTH (ft) TESTS MATERIAL DESCRIPTION 0 6 feet of water Bottom Elevation of Proposed Culvert (EL. 57.0) 5 6.0 56.0 OC = 2% Light brown, CLAYEY SAND, fine grained quartz, wet (Munsell 10YR 2/2) UD SC 6.8 55.3 1 Bottom of borehole at 6.8 feet. UD 2

LEGEND:

MC=Moisture Content LL= Liquid Limit PL= Plastic Limit PI= Plasticity Index OC= Organic Content NP= Not Plastic #200= Percent passing #200 sieve

# **APPENDIX C**



# Laboratory Test Result Summary

SPT / PT	Depth	Moisture	% Finer #200	Atte	rberg Li	mits	Organic
No.	Range (ft)	Content (%)	Sieve (%)	LL	PL	PI	Content (%)
2018-SPT-1	2 - 4	84.7	-	-	-	NP	25
2018-SPT-1	6 - 8	18.8	3.7	-	-	-	-
2018-SPT-1	18.5 - 20	25.1	20.5	-	-	-	-
2018-SPT-2	13.5 -15	14.1	18.8	-	-	-	-
2018-SPT-2	23.5 - 25	-	-	-	-	NP	-
2018-SPT-3	4 - 6	537.9	-	-	-	NP	91.4
2018-SPT-3	13.5 - 15	19.7	1.8	-	-	-	-
2018-SPT-4	4 - 6	605.7	-	-	-	NP	89.8
2018-SPT-4	13.5 - 15	-	-	74	20	54	-
2018-SPT-4	18.5 - 20	14	18.6	-	-	-	-
2018-SPT-5	4 - 6	669.1	-	-	-	NP	92.3
2018-SPT-5	13.5 - 15	_	-	_	-	NP	-
2018-SPT-5	18.5 - 20	23	4.6	_	-	-	-
2018-SPT-6	2 - 4	593.9	-	_	-	NP	92.6
2018-SPT-6	8 - 10	21.6	15.3	_	-	-	-
2018-SPT-7	4 - 6	29.3	54.5	_	-	-	-
2018-SPT-7	8 - 10	458.9	-	_	-	NP	91.3
2018-SPT-7	18.5 - 20	36.1	14.3	_	-	-	-
2018-SPT-8	4 - 6	45	29	_	_	_	-
2018-SPT-8	8 - 10	494.2	-	_	-	NP	74.9
2018-SPT-8	18.5 - 20	-	-	_	_	NP	-
2020-SPT-1	1 - 2	17	-	_	_	-	-
2020-SPT-1	2 - 3	-	20	_	-	-	-
2020-SPT-1	13 - 15	_	-	83	20	63	-
2020-SPT-1	28.5 - 30	-	4	-	-	-	-
2020-SPT-1	38.5 - 40	25	-	-	-	-	-
2020-SPT-2	0 - 1	12	-	-	-	-	-
2020-SPT-2	2 - 3	-	-	-	-	-	7
2020-SPT-2	9 - 11	-	31	-	-	-	-
2020-SPT-2	11 - 13	-	-	218	69	149	-
2020-SPT-2	23.5 - 25	20	-	-	-	-	-
2020-SPT-3	1 - 2	ļ	42	-	-	-	-
2020-SPT-3	4 - 5	-	-	-	-	-	61
2020-SPT-3	11 - 13	-	79	-	-	-	-
2020-SPT-3	18.5 - 20	17	-	-	-	-	-



SPT / PT	Depth	Moisture	% Finer #200	Atte	rberg Lir	Organic	
No.	Range (ft)	Content (%)	Sieve (%)	LL	PL	PI	Content (%)
2020-SPT-3	33.5 - 35	25	-	-	-	-	-
2020-SPT-4	1 - 2	28	-	-	-	-	-
2020-SPT-4	5 - 7	-	-	-	-	-	91
2020-SPT-4	9 - 11	33	-	-	-	-	-
2020-SPT-4	13 - 15	-	6	-	-	-	-
2020-SPT-5	1 - 2	-	72	-	-	-	-
2020-SPT-5	3 - 4	-	-	-	-	-	85
2020-SPT-5	11 - 13	51	-	-	-	-	-
2020-SPT-5	13 -15	20	-	-	-	-	-
2020-SPT-5	28.5 - 30	32	-	-	-	-	-
2020-SPT-5	43.5 - 45	-	16	-	-	-	-
2020-PT-1	6.5 - 7	-	-	-	-	-	17
2020-PT2	6 - 6.8	-	-	-	-	-	2

# Laboratory Test Result Summary



#### TOTAL ORGANIC CONTENT ANALYSIS (ASTM D 2974)

CLIENT: St. John River Water Management District (SJRWMD)

**PROJECT:** Prel. Design - Duda Pumps, Structures, and Levee Improvements **LOCATION:** Lake County and Orange County, FL

Test Date: October 4, 2018 Project #: 600550x3.\*\*\*\*.04 Requested By: L.Garcia Tested By: M. Hall Checked By: A. Chordia

Sample No. and Depth	Weight of Container + Wet Soil	Weight of Container + Dry Soil	Weight of Container	Weight of Container + Furnace Ash	Organic Loss	Moisture Content	Organic Content
	(grams)	(grams)	(grams)	(grams)	(grams)	(%)	(%)
2018-SPT-1 2-4	20.59	15.77	10.08	14.35	1.42	84.7	25.0
2018-SPT-3 4-6	20.37	12.84	11.44	11.56	1.28	537.9	91.4
2018-SPT-4 4-6	20.82	11.31	9.74	9.90	1.41	605.7	89.8
2018-SPT-5 4-6	26.62	13.64	11.70	11.85	1.79	669.1	92.3
2018-SPT-6 2-4	20.17	11.38	9.90	10.01	1.37	593.9	92.6
2018-SPT-7 8-10	23.42	12.82	10.51	10.71	2.11	458.9	91.3
2018-SPT-8 8-10	23.89	12.87	10.64	11.20	1.67	494.2	74.9



#### MOISTURE CONTENT and WET SIEVE ANALYSIS

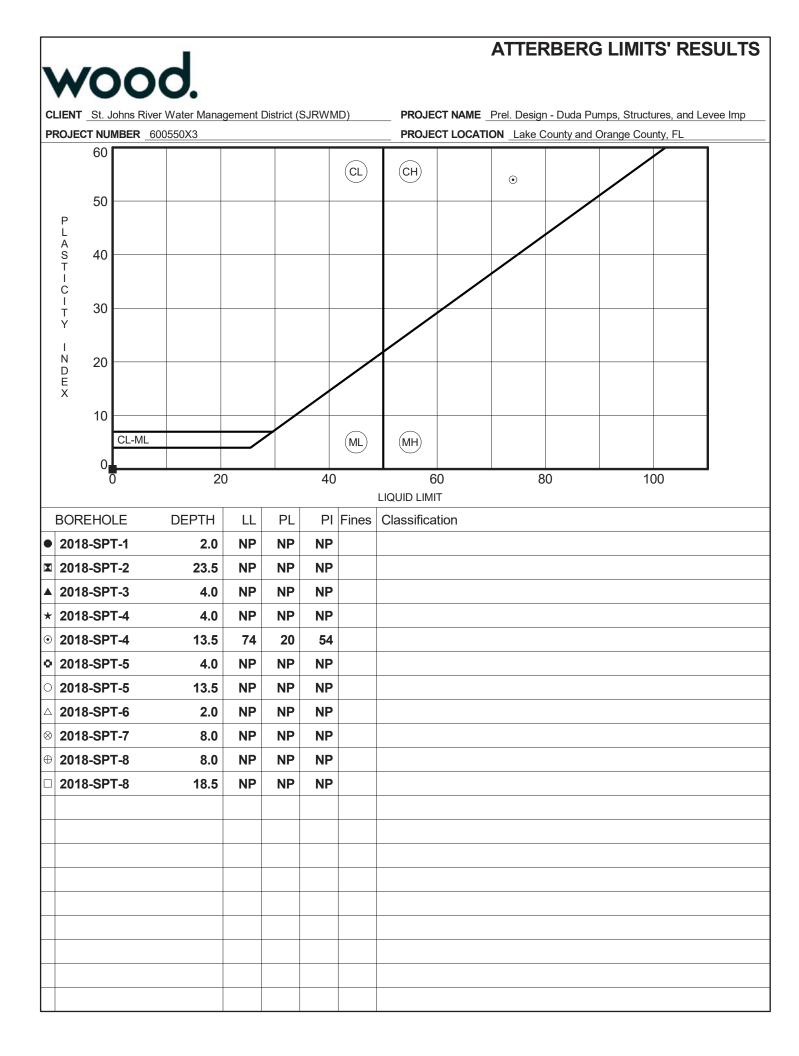
CLIENT: St. John River Water Management District (SJRWMD)

PROJECT: Prel. Design - Duda Pumps, Structures, and Levee Improvements

LOCATION: Lake County and Orange County, FL

ober 4, 2018
)550x3.****.04
arcia
Hall
Chordia

		% Sol	ids, Moisture Con	itent				Wet Sieve Test	
Sample No. and Depth	Tare ID	Weight of Container (g)	Weight of Container + Wet Soil (g)	Weight of Container + Dry Soil (g)	Solids Content (%)	Moisture Content (%)	Weight of Container + Dry Soil (g)	Weight of Container + Dry washed Soil (g)	% Finer than #200 Sieve (%)
2018-SPT-1 6-8	1010	85.25	333.57	294.26	84.17	18.8	294.26	286.45	3.7
2018-SPT-1 18.5-20	1012	84.18	382.62	322.76	79.94	25.1	322.76	273.91	20.5
2018-SPT-2 13.5-15	89A	84.21	377.99	341.60	87.61	14.1	341.6	293.15	18.8
2018-SPT-3 13.5-15	В	87.45	391.08	341.18	83.57	19.7	341.18	336.60	1.8
2018-SPT-4 18.5-20	Q	87.06	418.05	377.34	87.70	14.0	377.34	323.33	18.6
2018-SPT-5 18.5-20	4	85.29	401.41	342.24	81.28	23.0	342.24	330.53	4.6
2018-SPT-6 8-10	1961	86.13	380.92	328.46	82.20	21.6	328.46	291.47	15.3
2018-SPT-7 4-6	89C	84.16	256.65	217.60	77.36	29.3	217.6	144.90	54.5
2018-SPT-7 18.5-20	Р	85.65	345.73	276.75	73.48	36.1	276.75	249.47	14.3
2018-SPT-8 4-6	0	89.48	243.55	195.75	68.98	45.0	195.75	164.94	29.0



# wood.

## SOIL TESTING REPORT

Project: Duda Water Storage Improvements

Client: SJRWMD

Project Number: Date Tested: Date Reported: 600550x4.\*\*\*\*.02 March 4, 2020 March 18, 2020

Wood Environment & Infrastructure Solutions, Inc. performed soil testing on the soil samples delivered to our Jacksonville laboratory on March 4, 2020. The samples were tested in general accordance with ASTM standards. The results are outlined below.

Boring No	Sample No.	Depth (ft)	Percent Moisture (ASTM D2216)	Percent Organic (ASTM D2974)	Percent Passing #200 (ASTM D1140)
2020-SPT-1	2	1.0-2.0	17.1%	i=)	3-1
2020- SPT-1	3	2.0-3.0	-	1	20.4%
2020-SPT-1	13	28.5-30.0	-	2 <b>2</b> 5	4.3%
2020-SPT-1	15	38.5-40.0	24.6%	<b>1</b>	-
2020-SPT-2	1	0.0-1.0	12.3%		(H)
2020-SPT-2	3	2.0-3.0	-	31.0%	
2020-SPT-2	8	9.0-11.0	-	-	31.0%
2020-SPT-2	12	23.5-25.0	19.9%	-	-
2020-SPT-3	1	1.0-2.0	-	( <b>-</b> 1)	42.4%
2020-SPT-3	5	4.0-5.0	-	78.0%	-
2020-SPT-3	9	11.0-13.0	-	<b>a</b> t	78.6%
2020-SPT-3	11	18.5-20.0	16.5%	-	-
2020-SPT-3	14	33.5-35.0	24.6%	2	-
2020-SPT-4	2	1.0-2.0	27.5%	-	-
2020-SPT-4	6	5.0-7.0		38.0%	-
2020-SPT-4	8	9.0-11.0	33.4%	-	-
2020-SPT-4	10	13.0-15.0	-	-	6.0%
2020-SPT-5	2	1.0-2.0	-	-	71.8%
2020-SPT-5	4	3.0-4.0	5 <b>-</b> 0	18.0%	-
2020-SPT-5	9	11.0-13.0	51.3%	-	-
2020-SPT-5	10	13.0-15.0	20.3%	-	-
2020-SPT-5	13	28.5-30.0	31.5%	-	-
2020-SPT-5	16	43.5-45.0	•	19	16.4%
2020-PT-1	1	0.5-1.0	1	64.0%	15
2020-PT-2	2	0.3-0.8	171	48.0%	-

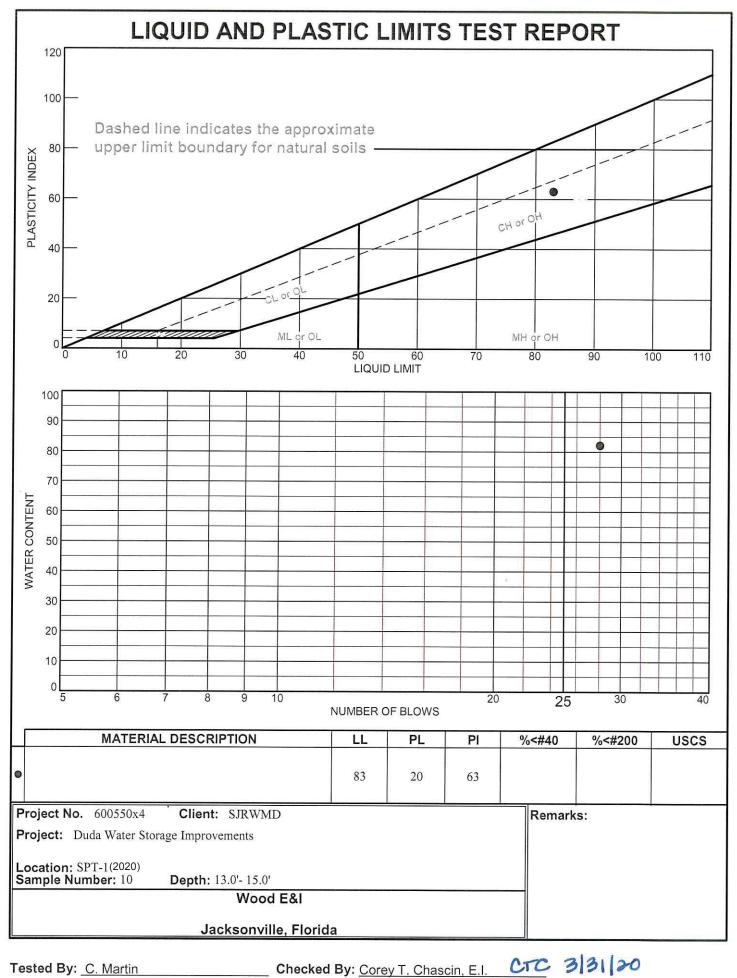
"-" Test not performed.

Performed By:

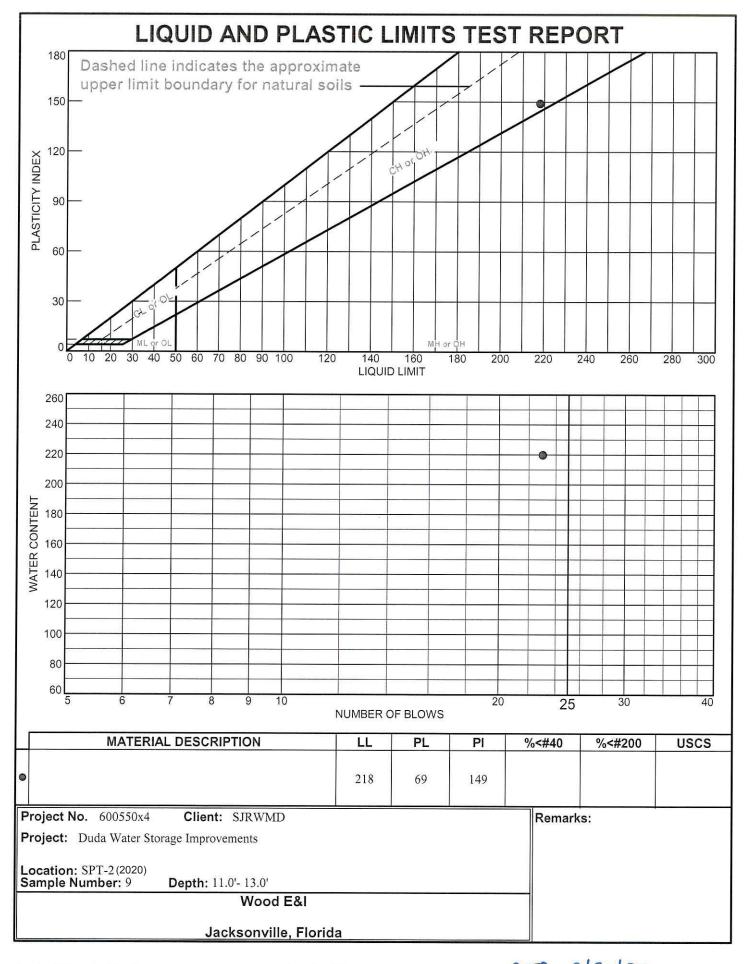
Reviewed By:

Ras 3/31/20 101 Corey T. Chascin, E.I.

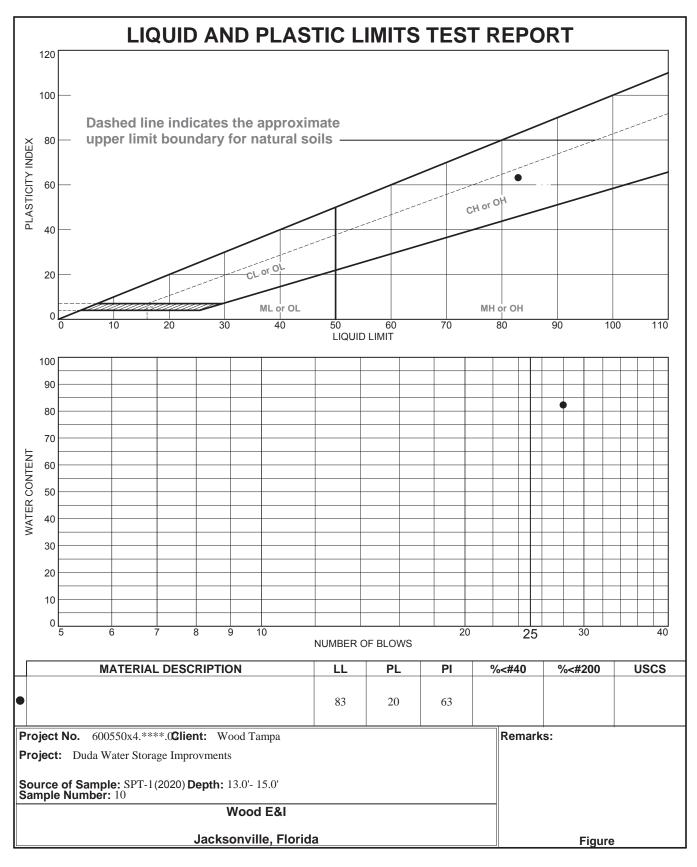
C. Martin



Checked By: Corey T. Chascin, E.I.

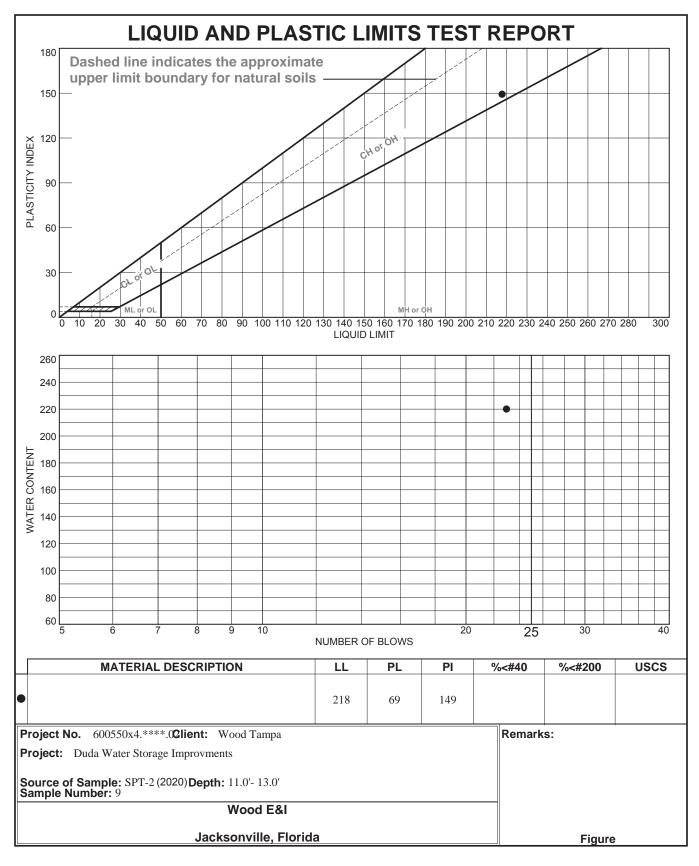


Checked By: Corey T. Chascin, E.I. CTC 331/20



Tested By: C. Martin

Checked By: Corey T. Chascin, E.I.



Tested By: C. Martin

Checked By: Corey T. Chascin, E.I.

# **APPENDIX D**



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St. Johns River Water Management District Duda Water Storage Improvements (WSI) Appendix D: Lateral Capacity Analysis Project No. 600550X04 June 2020 Page 1

# wood.

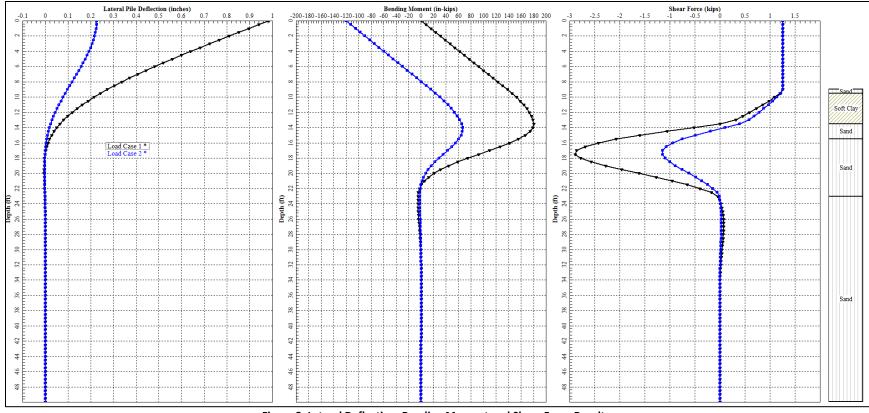


Figure 2. Lateral Deflection, Bending Moment and Shear Force Results

Project No. 600550X04 June 2020 Page 1

# **APPENDIX E**

Project: Project No: Prepared by:	Duda Water Storage Im 600550X4 Luis Garcia	provements (WSI) FINAL Geotechnical Report
Boring Reference:	2020-SPT-4	
Water depth:	0.3 ft	from top of pile
Design Water Elevation:	64.0 ft	NAVD88
Pile Top Elevation:	64.3 ft	NAVD88
Pile Ground Elevation: Depth from Water to	55.0 ft	NAVD88
Existing Ground =	9.0 ft	
Design Pile Tip Elevation =	24.3 ft	NAVD88
Design Embedment Depth =	30.7 ft	
D/b Ratio =	45	
Proposed Steel Pile:	HP8X36	
Cross Sectional Area =	10.6 in2	
	0.1 ft2	
Flange Width, b <sub>f</sub> =	8.2 in	
Flange Thickness, t <sub>f</sub> =	0.45 in	
Depth, d =	8.0 in	
Web Thickness, t <sub>w</sub> =	0.45 in	
Perimeter =	47.8 in	
Perimeter =	4.0 ft	
"Box Perimeter" =	32.3 in	
Box Perimeter =	2.7 ft	
"Box Area" =	65.4 in2	
Box Area -	0.5 ft2	
Critical Depth (D <sub>c</sub> ) =	13.6 ft	(20 B)
Factor of Safety (FS) =	2.0	

ω = 0.0 deg

Desc         Desc        Desc        Desc        De																							Side Friction Resistance							
	Soil Stratum No.	Description	SPT-N	N	from Ground Surface	from Ground Surface	THICKNESS	Top Ground Elevation (ft, NAVD88)	Elevation	Surface to Top	from Water Surface	rom Ground urface to mid	γ (pcf)	γ' (pcf)	Shear Strength, S <sub>u</sub>	Embedded	faster -	Adhesion, C <sub>α</sub> , (ksf)	displaced, V	, μπ,φ	δ/φ	Pile Interface Friction Angle, δ	Lateral Earth Pressure at	Correction Factor, C <sub>F</sub>		PWP @ Mid depth (psf)	depth	Unit Skin Friction Resistance, f <sub>s</sub> , (ksf)	Ult. Skin Friction Resistance, Q <sub>a</sub> , (kips) Resistance, Q	Skin Friction Resistance,
	3	SP / SC / SP-SC	5	5	0.0	0.5	0.5	55.0	54.5	9.0	9.3	0.3	115	53	-	0.0	-	-	0.91	28	1.00	28	1.00	1.00	590	577	13	0	0 0.0	0.0
	4	CH	3	3	0.5	1.0	0.5	54.5	54.0	9.5	9.8	0.8	120	58	200	0.5	0.55	0.11	0.91	-	-	-	-	-	649	608	41	0.1	0.1 0.1	0.1
	4	CH	3	3	1.5	2.0	0.5	53.5	53.0	10.0	10.3	1.8	120	58	200	1.5	0.55	0.11	0.91	-	-		-		769	671	98	0.1	0.1 0.3	0.1
····································	4	CH	3	3	2.0	2.5	0.5	53.0	52.5	11.0	11.3	2.3	120	58	200	2.0	0.55	0.11	0.91	-	-	-	-	-	829	702	127	0.1	0.1 0.6	0.3
····································	4	CH	5	5	2.5	3.0	0.5	52.5	52.0	11.5	11.8	2.8	120	58	200	2.5	0.55	0.11	0.91	-	-	-	-	-	889	733	156	0.1	0.1 0.7	0.4
	4	CH	5	5	3.5	4.0	0.5	51.5	51.0	12.0	12.3	3.8	120	58	200	3.5	0.55	0.11	0.91	-	-	-	-	-	1009	796	214	0.1	0.1 0.9	0.4
	4	CH	5	5	4.0	4.5	0.5	51.0	50.5	13.0	13.3	4.3	120	58	200	4.0	0.55	0.11	0.91	-	-	-	-	-	1069	827	242	0.1	0.1 1.2	0.6
	5	SP-SM	56	56	3 4.5	5.0	0.5	50.5	50.0	13.5	13.8	4.8	115	53	-	4.5	-	-	0.91	35	1.00	35	1.75	1.00	1128	858	270	0.27	0.4 1.6	0.8
	5		56	56	5.0	5.5	0.5	50.0	49.5	14.0	14.3	5.3	115	53	-	5.5	-		0.91	35	1.00	35	1.75	1.00		920	290	0.30	0.4 2.0	1.0
	5	SP-SM	56	56	6.0	6.5	0.5		48.5	15.0	15.3	6.3	115	53	-		-	-	0.91	35	1.00	35	1.75	1.00	1300	952	349	0.35	0.5 2.9	1.4
	5	SP-SM	23	23	6.5	7.0	0.5	48.5		15.5	15.8	6.8		53	-	6.5	-	-	0.91	30	1.00	30	1.15	1.00	1358	983	375	0.22	0.3 3.1	1.6
	5	SP-SM SP-SM	23	23	3 7.5	7.5	0.5	48.0		16.0	16.8	7.3	115	53	-	7.0	-		0.91	30	1.00	30		1.00	1415	1014	401	0.23	0.3 3.5	1.7
	5	SP-SM	23	23	3 8.0	8.5	0.5	47.0	46.5	17.0	17.3	8.3	115	53	-	8.0	-	-		30	1.00	30		1.00	1530	1076	454	0.26		2.1
	5	SP-SM	23	23	8.5	9.0	0.5		46.0	17.5	17.8	8.8	115	53	-	8.5	-	-	0.91	30	1.00	30	1.15	1.00	1588	1108	480	0.28	0.4 4.5	2.3
	5	SP-SM SP-SM	23	23	3 9.0	9.5	0.5	46.0		18.0	18.3	9.3	115	53	-	9.0	-		0.91	30	1.00	30	1.15	1.00	1645	1139	507	0.29	0.4 4.9	2.5
	5	SP-SM	23	23	3 10.0	10.5	0.5	45.0	44.5	19.0	19.3	10.3	115	53	-	10.0	-	-	0.91	30	1.00	30		1.00	1760	1201	559	0.32	0.4 5.8	2.9
	5	SP-SM	23	23	3 10.5	11.0	0.5		44.0	19.5	19.8	10.8	115	53	-	10.5	-	-	0.91	30	1.00	30		1.00	1818	1232	585	0.34	0.5 6.2	3.1
	5	SP-SM	23	23	3 11.0	11.5	0.5	44.0		20.0	20.3	11.3	115	53	-	11.0	-	-	0.91	30	1.00	30	1.15	1.00	1875	1264	612	0.35	0.5 6.7	3.3
	5	SP-SM	23	23	3 12.0	12.5	0.5	43.0		21.0	21.3	12.3	115	53	-	12.0	-	-	0.91	30	1.00	30	1.15	1.00	1990	1326	664	0.38	0.5 7.7	3.8
Image         Image <th< td=""><td>5</td><td>SP-SM</td><td>23</td><td>23</td><td>3 12.5</td><td>13.0</td><td>0.5</td><td>42.5</td><td>42.0</td><td>21.5</td><td>21.8</td><td>12.8</td><td>115</td><td>53</td><td>-</td><td>12.5</td><td>-</td><td>-</td><td>0.91</td><td>30</td><td>1.00</td><td>30</td><td>1.15</td><td>1.00</td><td>2048</td><td>1357</td><td>691</td><td>0.40</td><td>0.5 8.2</td><td>4.1</td></th<>	5	SP-SM	23	23	3 12.5	13.0	0.5	42.5	42.0	21.5	21.8	12.8	115	53	-	12.5	-	-	0.91	30	1.00	30	1.15	1.00	2048	1357	691	0.40	0.5 8.2	4.1
Image         Image <th< td=""><td>5</td><td>SP-SM</td><td>23</td><td>23</td><td>3 13.0</td><td>13.5</td><td>0.5</td><td>42.0</td><td>41.5</td><td>22.0</td><td>22.3</td><td>13.3</td><td>115</td><td>53</td><td>-</td><td>13.0</td><td>-</td><td>-</td><td>0.91</td><td>30</td><td>1.00</td><td>30</td><td></td><td>1.00</td><td>2105</td><td>1388</td><td>717</td><td></td><td>0.6 8.8</td><td>4.4</td></th<>	5	SP-SM	23	23	3 13.0	13.5	0.5	42.0	41.5	22.0	22.3	13.3	115	53	-	13.0	-	-	0.91	30	1.00	30		1.00	2105	1388	717		0.6 8.8	4.4
Image         Image <th< td=""><td>5</td><td>SP-SM SP-SM</td><td>23</td><td>23</td><td>3 14.0</td><td>14.0</td><td>0.5</td><td></td><td>40.5</td><td>22.5</td><td>23.3</td><td>14.3</td><td>115</td><td>53</td><td>-</td><td>13.5</td><td>-</td><td>-</td><td>0.91</td><td>30</td><td>1.00</td><td>30</td><td>1.15</td><td>1.00</td><td>2163</td><td>1451</td><td>743</td><td>0.44</td><td>0.6 9.4</td><td>4.7</td></th<>	5	SP-SM SP-SM	23	23	3 14.0	14.0	0.5		40.5	22.5	23.3	14.3	115	53	-	13.5	-	-	0.91	30	1.00	30	1.15	1.00	2163	1451	743	0.44	0.6 9.4	4.7
Image         Image <th< td=""><td>5</td><td>SP-SM</td><td>6</td><td>6</td><td></td><td>15.0</td><td>0.5</td><td></td><td></td><td>23.5</td><td>23.8</td><td>14.8</td><td>115</td><td>53</td><td>-</td><td>14.5</td><td>-</td><td>-</td><td>0.91</td><td>28</td><td>1.00</td><td>28</td><td></td><td>1.00</td><td>2278</td><td>1482</td><td>796</td><td></td><td>0.5 10.5</td><td>5.2</td></th<>	5	SP-SM	6	6		15.0	0.5			23.5	23.8	14.8	115	53	-	14.5	-	-	0.91	28	1.00	28		1.00	2278	1482	796		0.5 10.5	5.2
1         1	5	SP-SM	6	6		15.5	0.5			24.0	24.3	15.3		53	-		-	-		28	1.00	28		1.00	2335	1513				5.5
1         1	5	SP-SM	6	6	15.5	16.5	0.5	39.0	38.5	24.5	24.0	16.3	115	53	-	16.0	-	-	0.91	28	1.00	20	1.00	1.00	2393	1576	875	0.40	0.6 12.1	5.0
1         1	5	SP-SM	6	6	16.5	17.0	0.5	38.5	38.0	25.5	25.8	16.8	115	53	-	16.5	-	-	0.91	28	1.00	28	1.00	1.00	2508	1607	901	0.42	0.6 12.6	6.3
	5	SP-SM	6	6	17.0	17.5	0.5	38.0	37.5	26.0	26.3	17.3	115	53	-	17.0	-	-		28	1.00	28	1.00	1.00	2565	1638	927		0.6 13.2	6.6
	5	SP-SM SP SM	6	6	17.5	18.0	0.5	37.5	37.0	26.5	26.8	17.8	115	53	-	17.5	-	-	0.91	28	1.00	28	1.00	1.00	2623	1669	954	0.45	0.6 13.8	6.9
1         1	5	SP-SM	6	6	18.5	19.0	0.5	36.5	36.0	27.5	27.8	18.8	115	53	-	18.5	-	-	0.91	28	1.00	28	1.00	1.00	2738	1732		0.40	0.6 15.1	7.5
1         1	5	SP-SM	6	6	19.0	19.5	0.5	36.0	35.5	28.0	28.3	19.3	115	53	-	19.0	-	-	0.91	28	1.00	28	1.00	1.00	2795	1763	1033	0.48	0.7 15.7	7.9
1         1	5	SP-SM SP-SM	6	6	19.5	20.0	0.5	35.5	35.0	28.5	28.8	19.8	115	53	-	19.5	-	-		28	1.00	28	1.00	1.00	2853	1/94	1059	0.50	0.7 17.1	8.2
····································	5	SP-SM	6	6	20.5	21.0	0.5	34.5	34.0	29.5	29.8	20.8	115	53	-	20.5	-	-	0.91	28	1.00	28	1.00	1.00	2968	1856	1111	0.52	0.7 17.8	8.9
····································	5	SP-SM	6	6	21.0	21.5	0.5	34.0	33.5	30.0	30.3	21.3	115	53	-	21.0	-	-	0.91	28	1.00	28	1.00	1.00	3025	1888	1138	0.53	0.7 18.5	9.3
1         0	5		6	6	21.5	22.0	0.5	33.5	33.0	30.5	30.8	21.8	115	53	-	21.5	-	-	0.91	28	1.00	28		1.00	3083	1919	1164	0.55	0.7 19.3	9.6
b         b	5	SP-SM	6	6	22.5	23.0	0.5	32.5	32.0	31.5	31.8	22.8	115	53	-	22.5	-	-		28	1.00	28	1.00	1.00	3198	1981	1217	0.57	0.8 20.8	10.4
b         b	5	SP-SM	6	6	23.0	23.5	0.5	32.0	31.5	32.0	32.3	23.3	115	53	-	23.0	-	-	0.91	28	1.00	28	1.00	1.00	3255	2012	1243	0.58	0.8 21.6	10.8
b         b	5	SP-SM	6	6	23.5	24.0	0.5	31.5	31.0	32.5	32.8	23.8	115	53	-	23.5	-	-	0.91	28	1.00	28	1.00	1.00	3313	2044	1269	0.60	0.8 22.4	11.2
b         b	5	SP-SM	6	6	24.5	25.0	0.5	30.5	30.0	33.5	33.8	24.8	115	53	-	24.5	-	-	0.91	28	1.00	28		1.00		2106	1322	0.62	0.8 24.0	12.0
6         954         6         0         250        250     <	5	SP-SM	6	6	25.0	25.5	0.5	30.0	29.5	34.0	34.3	25.3	115	53	-	25.0	-	-	0.91	28	1.00	28	1.00	1.00	3485	2137	1348	0.63	0.9 24.9	12.4
6         954         6         0         250        250     <	5	SP-SM	6	6	25.5	26.0	0.5	29.5	29.0	34.5	34.8	25.8	115	53	-	25.5	-	-	0.91	28	1.00	28	1.00	1.00	3543	2168	1374	0.65	0.9 25.7	12.9
6         954         6         0         250        250     <	5	SP-SM	6	6	26.5	27.0	0.5	28.5	28.0	35.5	35.8	26.8	115	53	-	26.5	-	-		28	1.00	28	1.00	1.00	3658	2231	1427	0.67	0.9 27.5	13.8
5         98-M         6         6         25         25         25         25         27         28         16         5         26         16         5         26         16 <td>5</td> <td>SP-SM</td> <td>6</td> <td>6</td> <td>27.0</td> <td>27.5</td> <td>0.5</td> <td>28.0</td> <td>27.5</td> <td>36.0</td> <td>36.3</td> <td>27.3</td> <td>115</td> <td>53</td> <td>-</td> <td>27.0</td> <td>-</td> <td>-</td> <td></td> <td>28</td> <td>1.00</td> <td>28</td> <td>1.00</td> <td>1.00</td> <td>3715</td> <td>2262</td> <td></td> <td>0.68</td> <td>0.9 28.5</td> <td>14.2</td>	5	SP-SM	6	6	27.0	27.5	0.5	28.0	27.5	36.0	36.3	27.3	115	53	-	27.0	-	-		28	1.00	28	1.00	1.00	3715	2262		0.68	0.9 28.5	14.2
5         98-M         6         6         25         25         25         25         27         28         16         5         26         16         5         26         16 <td>5</td> <td>SP-SM SP-SM</td> <td>6</td> <td>6</td> <td>27.5</td> <td>28.0</td> <td>0.5</td> <td>27.5</td> <td>27.0</td> <td>36.5</td> <td>36.8</td> <td>27.8</td> <td>115</td> <td>53</td> <td></td> <td>27.5</td> <td></td> <td></td> <td>0.91</td> <td>28</td> <td>1.00</td> <td>28</td> <td>1.00</td> <td>1.00</td> <td>3773</td> <td>2293</td> <td>1480</td> <td>0.69</td> <td>0.9 29.4</td> <td>14.7</td>	5	SP-SM SP-SM	6	6	27.5	28.0	0.5	27.5	27.0	36.5	36.8	27.8	115	53		27.5			0.91	28	1.00	28	1.00	1.00	3773	2293	1480	0.69	0.9 29.4	14.7
5         5%         6         6         6         2.0         3.0        3.0        3.0 </td <td>5</td> <td>SP-SM</td> <td>6</td> <td>6</td> <td>28.5</td> <td>29.0</td> <td>0.5</td> <td>26.5</td> <td>26.0</td> <td>37.5</td> <td>37.8</td> <td>28.8</td> <td>115</td> <td>53</td> <td>-</td> <td>28.5</td> <td>-</td> <td>-</td> <td>0.91</td> <td>28</td> <td>1.00</td> <td>28</td> <td>1.00</td> <td>1.00</td> <td>3888</td> <td>2356</td> <td>1532</td> <td>0.72</td> <td>1.0 31.3</td> <td>15.7</td>	5	SP-SM	6	6	28.5	29.0	0.5	26.5	26.0	37.5	37.8	28.8	115	53	-	28.5	-	-	0.91	28	1.00	28	1.00	1.00	3888	2356	1532	0.72	1.0 31.3	15.7
5         SP-5M         6         6         31.6         32.0         0.5         23.0         0.6         0.6         31.6         32.0         0.6         0.6         31.6         32.0         0.6         32.5         10.0         10.0         42.3         27.6         10.0         0.7         11.0         37.5         16.7           5         SP-5M         6         0.6         33.0         32.0         0.5         23.0         23.0         11.0         33.0         1	5	SP-SM	6	6	29.0	29.5	0.5	26.0	25.5	38.0	38.3	29.3	115	53	-	29.0	-	-	0.91	28	1.00	28	1.00	1.00		2387	1559	0.73	1.0 32.3	16.1
5         SP-5M         6         6         31.6         32.0         0.5         23.0         0.6         0.6         31.6         32.0         0.6         0.6         31.6         32.0         0.6         32.5         10.0         10.0         42.3         27.6         10.0         0.7         11.0         37.5         16.7           5         SP-5M         6         0.6         33.0         32.0         0.5         23.0         23.0         11.0         33.0         1	5	SP-SM	6	6	29.5	30.0	0.5	25.5	25.0	38.5	38.8	29.8	115	53		29.5	-	-	0.91	28	1.00	28	1.00	1.00	4003	2418	1585	0.74	1.0 33.3	16.6
5         SP-5M         6         6         31.6         32.0         0.5         23.0         0.6         0.6         31.6         32.0         0.6         0.6         31.6         32.0         0.6         32.5         10.0         10.0         42.3         27.6         10.0         0.7         11.0         37.5         16.7           5         SP-5M         6         0.6         33.0         32.0         0.5         23.0         23.0         11.0         33.0         1	5	SP-SM	6	6	30.5	31.0	0.5	23.0	24.0	39.5	39.8	30.8	115	53	-	30.5	-	-	0.91	28	1.00	20	1.00	1.00	4118	2449	1637	0.70	1.0 34.3	17.7
5         SP-M         6         6         33.0         33.5         0.5         21.0         21.5         42.0         42.0         33.0         1.5         5.0         0.5         1.0         0.0         2.0         1.0         0.0         2.00         1.00         4405         26.00         1.1         49.0         20.0           5         SP-M         6         3.0         3.0         1.0         3.0         1.0         4.00         2.00         4.00         2.00         4.00         2.00         4.00         2.00         4.00         4.00         2.00         4.00         2.00         4.00 <td>5</td> <td>SP-SM</td> <td>6</td> <td>6</td> <td>31.0</td> <td>31.5</td> <td>0.5</td> <td>24.0</td> <td>23.5</td> <td></td> <td>40.3</td> <td>31.3</td> <td>115</td> <td>53</td> <td>-</td> <td>31.0</td> <td>-</td> <td>-</td> <td>0.91</td> <td>28</td> <td>1.00</td> <td>28</td> <td>1.00</td> <td>1.00</td> <td></td> <td>2512</td> <td></td> <td>0.78</td> <td>1.1 36.4</td> <td>18.2</td>	5	SP-SM	6	6	31.0	31.5	0.5	24.0	23.5		40.3	31.3	115	53	-	31.0	-	-	0.91	28	1.00	28	1.00	1.00		2512		0.78	1.1 36.4	18.2
5         SP-M         6         6         33.0         33.5         0.5         21.0         21.5         42.0         42.0         33.0         1.5         5.0         0.5         1.0         0.0         2.0         1.0         0.0         2.00         1.00         4405         26.00         1.1         49.0         20.0           5         SP-M         6         3.0         3.0         1.0         3.0         1.0         4.00         2.00         4.00         2.00         4.00         2.00         4.00         2.00         4.00         4.00         2.00         4.00         2.00         4.00 <td>5</td> <td>SP-SM</td> <td>6</td> <td>6</td> <td>31.5</td> <td>32.0</td> <td>0.5</td> <td>23.5</td> <td>23.0</td> <td></td> <td>40.8</td> <td>31.8</td> <td>115</td> <td>53</td> <td></td> <td>31.5</td> <td>-</td> <td>-</td> <td>0.91</td> <td>28</td> <td>1.00</td> <td>28</td> <td>1.00</td> <td>1.00</td> <td></td> <td>2543</td> <td>1690</td> <td>0.79</td> <td>1.1 37.5</td> <td>18.7</td>	5	SP-SM	6	6	31.5	32.0	0.5	23.5	23.0		40.8	31.8	115	53		31.5	-	-	0.91	28	1.00	28	1.00	1.00		2543	1690	0.79	1.1 37.5	18.7
5         SP-M         6         6         33.0         33.5         0.5         21.0         21.5         42.0         42.0         33.0         1.5         5.0         0.5         1.0         0.0         2.0         1.0         0.0         2.00         1.00         4405         26.00         1.1         49.0         20.0           5         SP-M         6         3.0         3.0         1.0         3.0         1.0         4.00         2.00         4.00         2.00         4.00         2.00         4.00         2.00         4.00         4.00         2.00         4.00         2.00         4.00 <td>5</td> <td>SP-SM</td> <td>6</td> <td>6</td> <td>32.5</td> <td>33.0</td> <td>0.5</td> <td>22.5</td> <td>22.0</td> <td>41.5</td> <td>41.8</td> <td>32.8</td> <td>115</td> <td>53</td> <td>-</td> <td>32.5</td> <td>-</td> <td>-</td> <td>0.91</td> <td>28</td> <td>1.00</td> <td>28</td> <td>1.00</td> <td>1.00</td> <td>4348</td> <td>2605</td> <td>1743</td> <td>0.82</td> <td>1.1 39.7</td> <td>19.8</td>	5	SP-SM	6	6	32.5	33.0	0.5	22.5	22.0	41.5	41.8	32.8	115	53	-	32.5	-	-	0.91	28	1.00	28	1.00	1.00	4348	2605	1743	0.82	1.1 39.7	19.8
5       SP-SM       6       6       34.0       35.0       0.5       20.0       43.5       43.8       34.8       115       63       -       0.91       28       1.00       28       1.00       46.0       27.0       184       0.87       1.2       44.4       22.1         5       SP-SM       6       6       35.0       0.5       20.0       19.5       44.0       35.3       15       53       -       36.0       10.0       28       10.0       28       10.0       28       10.0       46.0       46.7       12.7       44.4       22.7         5       SP-SM       6       6       36.0       0.5       19.0       44.5       44.8       35.8       115       53       -       36.7       -       0.91       28       10.0       28       10.0       40	5	SP-SM	6	6	33.0	33.5	0.5	22.0	21.5		42.3	33.3	115	53	-	33.0	-	-	0.91	28	1.00	28	1.00	1.00		2636	1769	0.83	1.1 40.8	20.4
5       SP-SM       6       6       34.0       35.0       0.5       20.0       43.5       43.8       34.8       115       63       -       0.91       28       1.00       28       1.00       46.0       27.0       184       0.87       1.2       44.4       22.1         5       SP-SM       6       6       35.0       0.5       20.0       19.5       44.0       35.3       15       53       -       36.0       10.0       28       10.0       28       10.0       28       10.0       46.0       46.7       12.7       44.4       22.7         5       SP-SM       6       6       36.0       0.5       19.0       44.5       44.8       35.8       115       53       -       36.7       -       0.91       28       10.0       28       10.0       40	5	SP-SM	6	6	33.5	34.0	0.5	21.5	21.0	42.5	42.8	33.8	115	53		33.5	-	-		28	1.00	28	1.00	1.00	4463	2668		0.84	1.1 41.9	21.0
5       SP-SM       6       6       37.0       37.5       0.5       18.0       17.5       46.0       43.3       37.3       115       53       -       70       28       1.00       28       1.00       28       1.00       1.00       4865       2886       1979       0.33       1.3       50.3       25.2         5       SP-SM       6       6       37.0       17.5       17.0       46.0       37.8       115       53       -       0.91       28       1.00       28       1.00       1.00       4863       286       1.03       1.0       483.2       216       37.3       61.6       25.4         5       SP-SM       6       6       38.0       0.5       17.5       17.0       46.5       47.0       47.3       38.3       115       53       -       0.91       28       1.00       28       1.00       480.3       284       20.2       29.6       0.35       1.3       54.2       27.1         5       SP-SM       6       6       38.0       39.5       15       53       -       38.0       -       -       0.91       28       1.00       28       1.00       480.3 </td <td>5</td> <td>SP-SM</td> <td>6</td> <td>6</td> <td>34.5</td> <td>34.5</td> <td>0.5</td> <td>21.0</td> <td>20.5</td> <td>43.5</td> <td>43.8</td> <td>34.8</td> <td>115</td> <td>53</td> <td>-</td> <td>34.5</td> <td>-</td> <td>1</td> <td>0.91</td> <td>20</td> <td>1.00</td> <td>20</td> <td>1.00</td> <td>1.00</td> <td>4578</td> <td>2099</td> <td>1848</td> <td>0.87</td> <td>1.2 43.1</td> <td>21.5</td>	5	SP-SM	6	6	34.5	34.5	0.5	21.0	20.5	43.5	43.8	34.8	115	53	-	34.5	-	1	0.91	20	1.00	20	1.00	1.00	4578	2099	1848	0.87	1.2 43.1	21.5
5       SP-SM       6       6       37.0       37.5       0.5       18.0       17.5       46.0       43.3       37.3       115       53       -       70       28       1.00       28       1.00       28       1.00       1.00       4865       2886       1979       0.33       1.3       50.3       25.2         5       SP-SM       6       6       37.0       17.5       17.0       46.0       37.8       115       53       -       0.91       28       1.00       28       1.00       1.00       4863       286       1.03       1.0       483.2       216       37.3       61.6       25.4         5       SP-SM       6       6       38.0       0.5       17.5       17.0       46.5       47.0       47.3       38.3       115       53       -       0.91       28       1.00       28       1.00       480.3       284       20.2       29.6       0.35       1.3       54.2       27.1         5       SP-SM       6       6       38.0       39.5       15       53       -       38.0       -       -       0.91       28       1.00       28       1.00       480.3 </td <td>5</td> <td>SP-SM</td> <td>6</td> <td>6</td> <td>35.0</td> <td>35.5</td> <td>0.5</td> <td>20.0</td> <td>19.5</td> <td>44.0</td> <td>44.3</td> <td>35.3</td> <td>115</td> <td>53</td> <td>-</td> <td>35.0</td> <td>-</td> <td>-</td> <td></td> <td>28</td> <td>1.00</td> <td>28</td> <td>1.00</td> <td>1.00</td> <td>4635</td> <td>2761</td> <td></td> <td>0.88</td> <td>1.2 45.4</td> <td>22.7</td>	5	SP-SM	6	6	35.0	35.5	0.5	20.0	19.5	44.0	44.3	35.3	115	53	-	35.0	-	-		28	1.00	28	1.00	1.00	4635	2761		0.88	1.2 45.4	22.7
5       SP-SM       6       6       37.0       37.5       0.5       18.0       17.5       46.0       43.3       37.3       115       53       -       70       28       1.00       28       1.00       28       1.00       1.00       4865       2886       1979       0.33       1.3       50.3       25.2         5       SP-SM       6       6       37.0       17.5       17.0       46.0       37.8       115       53       -       0.91       28       1.00       28       1.00       1.00       4863       286       1.03       1.0       483.2       216       37.3       61.6       25.4         5       SP-SM       6       6       38.0       0.5       17.5       17.0       46.5       47.0       47.3       38.3       115       53       -       0.91       28       1.00       28       1.00       480.3       284       20.2       29.6       0.35       1.3       54.2       27.1         5       SP-SM       6       6       38.0       39.5       15       53       -       38.0       -       -       0.91       28       1.00       28       1.00       480.3 </td <td>5</td> <td>SP-SM</td> <td>6</td> <td>6</td> <td>35.5</td> <td>36.0</td> <td>0.5</td> <td>19.5</td> <td>19.0</td> <td>44.5</td> <td>44.8</td> <td>35.8</td> <td>115</td> <td>53</td> <td></td> <td>35.5</td> <td></td> <td>-</td> <td>0.91</td> <td>28</td> <td>1.00</td> <td>28</td> <td>1.00</td> <td>1.00</td> <td>4693</td> <td>2792</td> <td>1900</td> <td>0.89</td> <td>1.2 46.6</td> <td>23.3</td>	5	SP-SM	6	6	35.5	36.0	0.5	19.5	19.0	44.5	44.8	35.8	115	53		35.5		-	0.91	28	1.00	28	1.00	1.00	4693	2792	1900	0.89	1.2 46.6	23.3
5       SP-SM       6       6       37.0       37.5       0.5       18.0       17.5       46.0       43.3       37.3       115       53       -       70       28       1.00       28       1.00       28       1.00       1.00       4865       2886       1979       0.33       1.3       50.3       25.2         5       SP-SM       6       6       37.0       17.5       17.0       46.0       37.8       115       53       -       0.91       28       1.00       28       1.00       1.00       4863       286       1.03       1.0       483.2       216       37.3       61.6       25.4         5       SP-SM       6       6       38.0       0.5       17.5       17.0       46.5       47.0       47.3       38.3       115       53       -       0.91       28       1.00       28       1.00       480.3       284       20.2       29.6       0.35       1.3       54.2       27.1         5       SP-SM       6       6       38.0       39.5       15       53       -       38.0       -       -       0.91       28       1.00       28       1.00       480.3 </td <td>5</td> <td>SP-SM</td> <td>0 6</td> <td>6</td> <td>30.0</td> <td>30.5</td> <td>0.5</td> <td>19.0</td> <td>18.5</td> <td>45.0</td> <td>45.3</td> <td>30.3</td> <td></td> <td>53</td> <td>-</td> <td>30.0</td> <td>-</td> <td></td> <td>0.91</td> <td>28</td> <td>1.00</td> <td>28</td> <td>1.00</td> <td>1.00</td> <td></td> <td>2824</td> <td>1927</td> <td>0.90</td> <td>1.2 4/.8</td> <td>23.9</td>	5	SP-SM	0 6	6	30.0	30.5	0.5	19.0	18.5	45.0	45.3	30.3		53	-	30.0	-		0.91	28	1.00	28	1.00	1.00		2824	1927	0.90	1.2 4/.8	23.9
5       SP-SM       6       6       38.0       38.5       0.5       17.0       16.5       47.0       47.3       38.3       115       63       -       -       0.91       28       1.00       1.00       4880       2948       2052       0.95       1.3       54.9       22.4         5       SP-SM       6       6       38.0       0.5       16.5       16.0       47.0       47.3       38.3       115       63       -       0.91       28       1.00       1.00       1.00       4880       2948       2052       0.95       1.3       54.9       27.1         5       SP-SM       6       6       38.0       39.5       0.5       16.0       47.5       47.8       38.8       115       53       -       0.91       28       1.00       28       1.00       1.00       4800       2948       2052       0.95       1.3       54.2       27.1         5       SP-SM       6       6       38.0       39.5       1.5       53       -       38.0       -       -       0.91       28       1.00       28       1.00       1.00       505       3011       20.5       1.3       55.	5	SP-SM	6	6	37.0	37.5	0.5	18.0	17.5	46.0	46.3	37.3		53	-	37.0	-	-	0.91	28	1.00	28		1.00	4865	2886		0.93	1.3 50.3	25.2
5 SP-SM 6 6 39.5 40.0 0.5 15.5 15.0 48.5 48.8 39.8 115 53 - 39.5 0.91 28 1.00 28 1.00 1.00 5153 3042 211 0.99 1.3 56.8 28.4	5	SP-SM	6	6	37.5	38.0	0.5	17.5	17.0	46.5	46.8	37.8	115	53	-	37.5	-	-	0.91	28	1.00	28	1.00	1.00		2917		0.94	1.3 51.6	25.8
5 SP-SM 6 6 39.5 40.0 0.5 15.5 15.0 48.5 48.8 39.8 115 53 - 39.5 0.91 28 1.00 28 1.00 1.00 5153 3042 211 0.99 1.3 56.8 28.4	5	SP-SM	0 6	6	38.0	38.5	0.5	17.0	16.0	47.0	47.3	38.8	115	53	-	38.0	-		0.91	28	1.00	28	1.00	1.00	4980 5038	2948	2032	0.95	1.3 52.9	20.4
	5	SP-SM	6	6	39.0	39.5	0.5	16.0	15.5	48.0	48.3	39.3	115	53	-	39.0	-	-	0.91	28	1.00	28	1.00	1.00	5095	3011	2085	0.98	1.3 55.5	27.8
	5	SP-SM	6	6	39.5	40.0	0.5 40 ft	15.5	15.0	48.5	48.8	39.8	115	53		39.5		-	0.91	28	1.00	28	1.00	1.00	5153	3042	2111	0.99	1.3 56.8	28.4

#### Axial Capacity Analysis on Steel piles Ref: United States Department of Transportation of Federal Highway Administration (FHWA) - Design and Construction of Driven Pile Foundations - Volume 1



Project: Project No: Prepared by:	Duda Water Storage In 600550X4 Luis Garcia	provements (WSI) FINAL Geotechnical Report
Boring Reference:	2020-SPT-4	
Water depth:	0.3 ft	from top of pile
Design Water Elevation:	64.0 ft	NAVD88
Pile Top Elevation:	64.3 ft	NAVD88
Pile Ground Elevation:	55.0 ft	NAVD88
Depth from Water to Existing Ground =	9.0 ft	
Design Pile Tip Elevation =	24.3 ft	NAVD88
Design Embedment Depth =	30.7 ft	
D/b Ratio =	45	
Proposed Steel Pile:	HP8X36	
Cross Sectional Area =	10.6 in2	
Cross Sectional Area -	0.1 ft2	
Flange Width, b <sub>f</sub> =	8.2 in	
Flange Thickness, t <sub>f</sub> =	0.45 in	
Depth, d =	8.0 in	
Web Thickness, t <sub>w</sub> =	0.45 in	
Perimeter =	47.8 in	
Perimeter -	4.0 ft	
"Box Perimeter" =	32.3 in	
Box Ferineter =	2.7 ft	
"Box Area" =	65.4 in2	
Box Alda -	0.5 ft2	
Critical Depth ( $D_c$ ) =	13.6 ft	(20 B)
Factor of Safety (FS) =	2.0	
ω =	0.0 deg	

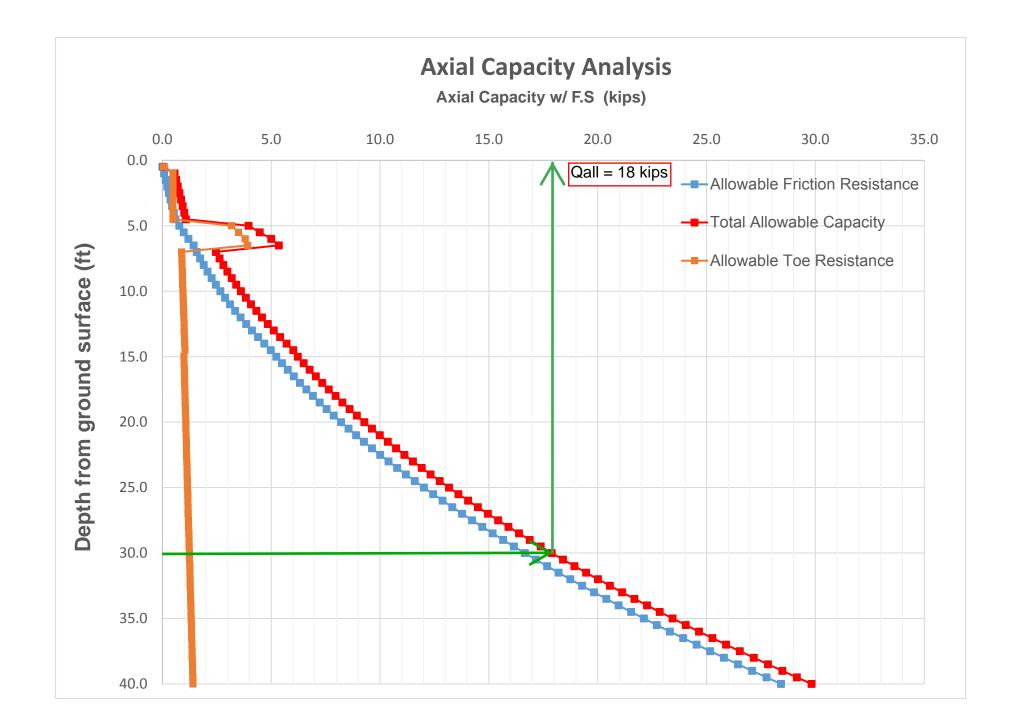
												h.h.s			-	nd Bearing R		1	21-3		-					
Soil Stratum No.	Description	SPT-N (field)	Top Embedment Depth from Ground Surface (Elev +55 ft, NAVD88)	Bottom Embedment Depth from Ground Surface (Elev +55 ft, NAVD88)	Thickness (ft)	Depth from Water Surface to Top	Depth from Water Surface to Mid Layer (ft)	Surface to fillu layer	γ (pcf)	γ' (pcf)	Undrained Shear Strength, S <sub>u</sub> (psf)	lpha method (c N <sub>c</sub>	Unit Toe Resistance, c	Nominal toe Resistance (R <sub>p</sub> ) (kips)	α <sub>t</sub> Coefficient	N'q	$\sigma_v$ at Pile toe at $\sigma$	thod (cohesionless s 'v at Pile toe at his depth (psf)	l toe Limiting Unit ce (R <sub>p</sub> ) Toe Resistance (q		Governing Nominal toe Resistance (R <sub>p</sub> )	Q <sub>ult</sub> ) (kips)	Allowable Toe Resistance (Q <sub>end</sub> ) (kips) (FS = 2)	Total Allowable Capacity (Q <sub>all</sub> ) (kips) (FS = 2)	Uplift Φ <sub>υρ</sub>	Accumulated Ruplift (kips)
			(2164 - 33 11, 1444 200)	(LIEV 133 IL, INAV 200)		Layer (ft)	wild Layer (it)	(ft)					(ksf)	(Rp) (Rips)				(kit	.,,	(kips)	(kips)		(Kips) (F3 = 2)	(Kips) (F3 = 2)		
3	SP / SC / SP-SC	5	0	0.5	0.5	9.0	9.25	0.25	115	52.6	-	-	-	-	0.6	30	590	13 0.	100	7.4	0.1	0.1	0.1	0.1	0.35	0.0
4	CH	3	0.5	1.0	0.5	9.5	9.75	0.75	120	57.6	200	9	1.8	0.82	-	-	649	41 -	-	-	0.8	1.0	0.5	0.6	0.25	0.0
4	CH	3	1.0	1.5	0.5	10.0	10.25	1.25	120	57.6	200	9	1.8	0.82	-	-	709		-	-	0.8	1.0	0.5	0.6	0.25	0.1
4	СН	3	2.0	2.0 2.5	0.5	10.5	10.75 11.25	1.75 2.25	120	57.6 57.6	200	9	1.8	0.82	-	-	829	127 -		-	0.8	1.0	0.5	0.7	0.25	0.1
4	CH	5	2.5	3.0	0.5	11.5	11.75	2.25	120	57.6	200	9	1.8	0.82	-	-	889	156		-	0.8	1.0	0.5	0.9	0.25	0.1
4	CH	5	3.0	3.5	0.5	12.0	12.25	3.25	120	57.6	200	9	1.8	0.82	-	-	949	185 -	-	-	0.8	1.0	0.5	0.9	0.25	0.2
4	CH	5	3.5	4.0	0.5	12.5	12.75	3.75	120	57.6	200	9	1.8	0.82	-	-	1009	214 -	-	-	0.8	1.0	0.5	1.0	0.25	0.3
4	CH	5	4.0	4.5	0.5	13.0	13.25	4.25	120	57.6	200	9	1.8	0.82	-	-	1069	242 -	-	-	0.8	1.0	0.5	1.1	0.25	0.3
5	SP-SM	56	4.5	5.0	0.5	13.5	13.75	4.75	115	52.6	-	-	-	-	0.7	70	1128	270 6.		7.4	6.0	6.4	3.2	4.0	0.35	0.5
5	SP-SM SP-SM	56	5.0	6.0	0.5	14.0	14.25 14.75	5.25 5.75	115	52.6 52.6	-	-	-	-	0.7	70	1185 1243	296 6. 322 7.		7.4	6.6 7.2	7.0	3.5 3.8	4.5	0.35	0.7
5	SP-SM	56	6.0	6.5	0.5	14.5	15.25	6.25	115	52.6	-		-	-	0.7	70	1300	349 7.		7.4	7.4	7.8	3.9	5.3	0.35	1.0
5	SP-SM	23	6.5	7.0	0.5	15.5	15.75	6.75	115	52.6	-	-	-	-	0.6	30	1358	375 3.	20	1.5	1.5	1.8	0.9	2.5	0.35	1.1
5	SP-SM	23	7.0	7.5	0.5	16.0	16.25	7.25	115	52.6	-	-	-	-	0.6	30	1415	401 3.		1.5	1.5	1.8	0.9	2.6	0.35	1.2
5	SP-SM	23	7.5	8.0	0.5	16.5	16.75	7.75	115	52.6	-	-	-	-	0.6	30	1473	428 3.	20	1.5	1.5	1.8	0.9	2.8	0.35	1.3
5	SP-SM	23	8.0	8.5	0.5	17.0	17.25	8.25	115	52.6 52.6	-	-	-	-	0.6	30	1530	454 3.		1.5	1.5	1.8	0.9	3.0	0.35	1.5
5	SP-SM SP-SM	23	9.0		0.5	17.5	17.75	8.75	115 115	52.6 52.6	-	-	-	-	0.6	30	1588 1645	480 3. 507 4.		1.5	1.5	1.8	0.9	3.2	0.35	1.6
5	SP-SM SP-SM	23	9.5	9.5	0.5	18.5	18.25	9.25 9.75	115	52.6	-	-	-	-	0.6	30	1703	533 4.		1.5	1.5	1.9		3.6	0.35	1.9
5	SP-SM	23	10.0	10.0 10.5	0.5	19.0	18.75 19.25	10.25	115	52.6		-	-	-	0.6	30	1760	559 4.		1.5	1.5	1.9	0.9	3.8	0.35	2.0
5	SP-SM	23	10.5	11.0	0.5	19.5	19.75	10.75	115	52.6	-	-	-	-	0.6	30	1818	585 4.		1.5	1.5	1.9	1.0	4.1	0.35	2.2
5	SP-SM	23	11.0	11.5	0.5	20.0	20.25	11.25	115	52.6	-	-	-	-	0.6	30	1875	612 5.		1.5	1.5	1.9	1.0	4.3	0.35	2.3
5	SP-SM	23	11.5	12.0	0.5	20.5	20.75	11.75	115	52.6		-	-	-	0.6	30	1933	638 5.		1.5	1.5	2.0	1.0	4.6	0.35	2.5
5	SP-SM	23	12.0	12.5	0.5	21.0	21.25	12.25	115	52.6		-	-	-	0.6	30 30	1990	664 5.		1.5	1.5	2.0	1.0	4.8 5.1	0.35	2.7
5	SP-SM SP-SM	23	12.5	13.0	0.5	21.5 22.0	21.75 22.25	12.75 13.25	115	52.6 52.6	-	-	-	-	0.6	30	2048 2105	691 5. 717 5.		1.5	1.5	2.0	1.0	5.1	0.35	2.9 3.1
5	SP-SM	23	13.5	14.0	0.5	22.5	22.25	13.75	115	52.6	-	-	-	-	0.6	30	2163	743 6.		1.5	1.5	2.0	1.0	5.7	0.35	3.3
5	SP-SM	23	14.0	14.5	0.5	23.0	23.25	14.25	115	52.6	-	-	-	-	0.6	30	2220	770 6.		1.5	1.5	2.1	1.0	6.0	0.35	3.5
5	SP-SM	6	14.5	15.0	0.5	23.5	23.75	14.75	115	52.6	-	-	-	-	0.6	30	2278	796 6.	20	1.5	1.5	2.0	1.0	6.2	0.35	3.7
5	SP-SM	6	15.0	15.5	0.5	24.0	24.25	15.25	115	52.6	-	-	-	-	0.6	30	2335	822 6.		1.5	1.5	2.0	1.0	6.5	0.35	3.8
5	SP-SM	6	15.5	16.0	0.5	24.5	24.75	15.75	115	52.6	-	-	-	-	0.6	30	2393	848 6.		1.5	1.5	2.0	1.0	6.8	0.35	4.0
5	SP-SM SP-SM	6	16.0	16.5 17.0	0.5	25.0	25.25	16.25 16.75	115 115	52.6 52.6	-	-	-	-	0.6	30	2450 2508	875 7. 901 7.		1.5	1.5	2.0	1.0	7.0	0.35	4.2
5	SP-SM	6	17.0	17.5	0.5	25.5	25.75 26.25	17.25	115	52.6	-		-	-	0.6	30	2565	901 7.		1.5	1.5	2.0	1.0	7.5	0.35	4.4
5	SP-SM	6	17.5	18.0	0.5	26.5	26.75	17.75	115	52.6	-	-	-	-	0.6	30	2623	954 7.		1.5	1.5	2.1	1.0	8.0	0.35	4.8
5	SP-SM	6	18.0	18.5	0.5	27.0	27.25	18.25	115	52.6	-	-	-	-	0.6	30	2680	980 8.		1.5	1.5	2.1	1.0	8.3	0.35	5.1
5	SP-SM	6	18.5	19.0	0.5	27.5	27.75	18.75	115	52.6	-	-	-	-	0.6	30	2738	1006 8.		1.5	1.5	2.1	1.1	8.6	0.35	5.3
5	SP-SM	6	19.0	19.5	0.5	28.0	28.25	19.25	115	52.6	-	-	-	-	0.6	30	2795	1033 8.		1.5	1.5	2.1	1.1	8.9	0.35	5.5
5	SP-SM	6	19.5	20.0	0.5	28.5	28.75	19.75	115	52.6	-	-	-	-	0.6	30	2853	1059 8.		1.5	1.5	2.1	1.1	9.3	0.35	5.7
5	SP-SM SP-SM	6	20.0 20.5	20.5 21.0	0.5	29.0	29.25 29.75	20.25 20.75	115	52.6 52.6	-		-	-	0.6	30	2910 2968	1085 8. 1111 9.		1.5	1.5	2.2	1.1	9.6 10.0	0.35	6.0
5	SP-SM	6	21.0	21.5	0.5	30.0	30.25	21.25	115	52.6	-	-	-	-	0.6	30	3025	1138 9.		1.5	1.5	2.2	1.1	10.4	0.35	6.5
5	SP-SM	6	21.5	22.0	0.5	30.5	30.75	21.75	115	52.6	-	-	-	-	0.6	30	3083	1164 9.	20	1.5	1.5	2.2	1.1	10.7	0.35	6.7
5	SP-SM	6	22.0	22.5	0.5	31.0	31.25	22.25	115	52.6	-	-	-	-	0.6	30	3140	1190 9.		1.5	1.5	2.2	1.1	11.1	0.35	7.0
5	SP-SM	6	22.5	23.0	0.5	31.5	31.75	22.75	115	52.6	-	-	-	-	0.6	30	3198	1217 9.		1.5	1.5	2.2	1.1	11.5	0.35	7.3
5	SP-SM SP-SM	6	23.0	23.5	0.5	32.0	32.25	23.25	115	52.6	-	-	-	-	0.6	30 30	3255	1243 10		1.5	1.5	2.3	1.1	11.9 12.3	0.35	7.5
5	SP-SM SP-SM	6	23.5 24.0	24.0 24.5	0.5	32.5 33.0	32.75 33.25	23.75 24.25	115	52.6 52.6	-		-		0.6	30	3313 3370	1269 10 1296 10		1.5	1.5	2.3	1.1	12.3	0.35	8.1
5	SP-SM	6	24.5	25.0	0.5	33.5	33.75	24.75	115	52.6	-	-	-	-	0.6	30	3428	1322 10		1.5	1.5	2.3	1.2	13.2	0.35	8.4
5	SP-SM	6	25.0	25.5	0.5	34.0	34.25	25.25	115	52.6	-	-	-	-	0.6	30	3485	1348 11		1.5	1.5	2.3	1.2	13.6	0.35	8.7
5	SP-SM	6	25.5	26.0	0.5	34.5	34.75	25.75	115	52.6		-	-	-	0.6	30	3543	1374 11	2 20	1.5	1.5	2.3	1.2	14.0	0.35	9.0
5	SP-SM	6	26.0	26.5	0.5	35.0	35.25	26.25	115	52.6		-	-	-	0.6	30	3600	1401 11		1.5	1.5	2.4	1.2	14.5	0.35	9.3
5	SP-SM SP-SM	6	26.5 27.0	27.0	0.5	35.5	35.75 36.25	26.75 27.25	115	52.6 52.6	+ :		-	-	0.6	30	3658	1427 11 1453 11		1.5	1.5	2.4	1.2	15.0	0.35	9.6 10.0
5	SP-SM	6	27.5	28.0	0.5	36.5	36.75	27.75	115	52.6	1	-	-	-	0.6	30	3773	1480 12		1.5	1.5	2.4	1.2	15.9	0.35	10.0
5	SP-SM	6	28.0	28.5	0.5	37.0	37.25	28.25	115	52.6	· ·	-	-	-	0.6	30	3830	1506 12	3 20	1.5	1.5	2.4	1.2	16.4	0.35	10.6
5	SP-SM	6	28.5	29.0	0.5	37.5	37.75	28.75	115	52.6	-	-	-	-	0.6	30	3888	1532 12	5 20	1.5	1.5	2.4	1.2	16.9	0.35	11.0
5	SP-SM	6	29.0	29.5	0.5	38.0	38.25	29.25	115	52.6		-	-	-	0.6	30	3945	1559 12		1.5	1.5	2.5	1.2	17.4	0.35	11.3
5	SP-SM SP-SM	6	29.5 30.0	30.0 30.5	0.5	38.5	38.75	29.75 30.25	115	52.6		-	-	-	0.6	30	4003	1585 12 1611 13	20	1.5	1.5	2.5	1.2	17.9 18.4	0.35	11.7
5	SP-SM SP-SM	9	30.0	30.5	0.5	39.0	39.25 39.75	30.25	115	52.6 52.6	1	-	1	-	0.6	30	4060 4118	1611 13 1637 13		1.5	1.5	2.5	1.2	18.4	0.35	12.0
5	SP-SM	6	31.0	31.5	0.5	40.0	40.25	31.25	115	52.6	-	-	-	-	0.6	30	4175	1664 13		1.5	1.5	2.5	1.3	19.5	0.35	12.7
5	SP-SM	6	31.5	32.0	0.5	40.5	40.75	31.75	115	52.6	-	-	-	-	0.6	30	4233	1690 13		1.5	1.5	2.5	1.3	20.0	0.35	13.1
5	SP-SM	6	32.0	32.5	0.5	41.0	41.25	32.25	115	52.6	-	-	-	-	0.6	30	4290	1716 14	20	1.5	1.5	2.6	1.3	20.6	0.35	13.5
5	SP-SM	6	32.5	33.0	0.5	41.5	41.75	32.75	115	52.6		-	-		0.6	30	4348	1743 14		1.5	1.5	2.6	1.3	21.1	0.35	13.9
d a	SP-SM SP-SM	6	33.0 33.5	33.5 34.0	0.5	42.0 42.5	42.25 42.75	33.25 33.75	115	52.6 52.6		-	-	-	0.6	30	4405 4463	1769 14 1795 14		1.5	1.5	2.6	1.3	21.7 22.3	0.35	14.3
5	SP-SM SP-SM	6	33.5	34.0	0.5	42.5	42.75	33.75	115	52.6	1	-	-	-	0.6	30	4463	1795 14 1822 14		1.5	1.5	2.6	1.3	22.3	0.35	14.7
5	SP-SM	6	34.5	35.0	0.5	43.5	43.75	34.75	115	52.6	· ·	-	-	-	0.6	30	4578	1848 15		1.5	1.5	2.6	1.3	23.4	0.35	15.5
5	SP-SM	6	35.0	35.5	0.5	44.0	44.25	35.25	115	52.6	-	-	-	-	0.6	30	4635	1874 15	3 20	1.5	1.5	2.7	1.3	24.0	0.35	15.9
5	SP-SM	6	35.5	36.0	0.5	44.5	44.75	35.75	115	52.6	-	-	-	-	0.6	30	4693	1900 15	5 20	1.5	1.5	2.7	1.3	24.7	0.35	16.3
5	SP-SM	6	36.0	36.5	0.5	45.0	45.25	36.25	115	52.6	-	-	-	-	0.6	30	4750	1927 15		1.5	1.5	2.7	1.3	25.3	0.35	16.7
5	SP-SM	6	36.5	37.0	0.5	45.5	45.75	36.75	115	52.6		-	-	-	0.6	30	4808	1953 16		1.5	1.5	2.7	1.4	25.9	0.35	17.2
5	SP-SM SP-SM	6	37.0 37.5	37.5 38.0	0.5	46.0	46.25 46.75	37.25 37.75	115	52.6 52.6	+ :		1	-	0.6	30 30	4865 4923	1979 16 2006 16		1.5	1.5	2.7	1.4	26.5 27.2	0.35	17.6
5	SP-SM	6	37.5	38.5	0.5	40.5	40.75	38.25	115	52.6		-	-	-	0.6	30	4923	2006 16		1.5	1.5	2.7	1.4	27.8	0.35	18.5
5	SP-SM	6	38.5	39.0	0.5	47.5	47.75	38.75	115	52.6	-	-	-	-	0.6	30	5038	2058 16	3 20	1.5	1.5	2.8	1.4	28.5	0.35	19.0
5	SP-SM	6	39.0	39.5	0.5	48.0	48.25	39.25	115	52.6	-	-	-	-	0.6	30	5095	2085 17	20	1.5	1.5	2.8	1.4	29.1	0.35	19.4
5	SP-SM	6	39.5	40.0	0.5	48.5	48.75	39.75	115	52.6	-	-	-	-	0.6	30	5153	2111 17	2 20	1.5	1.5	2.8	1.4	29.8	0.35	19.9
					40 ft																					

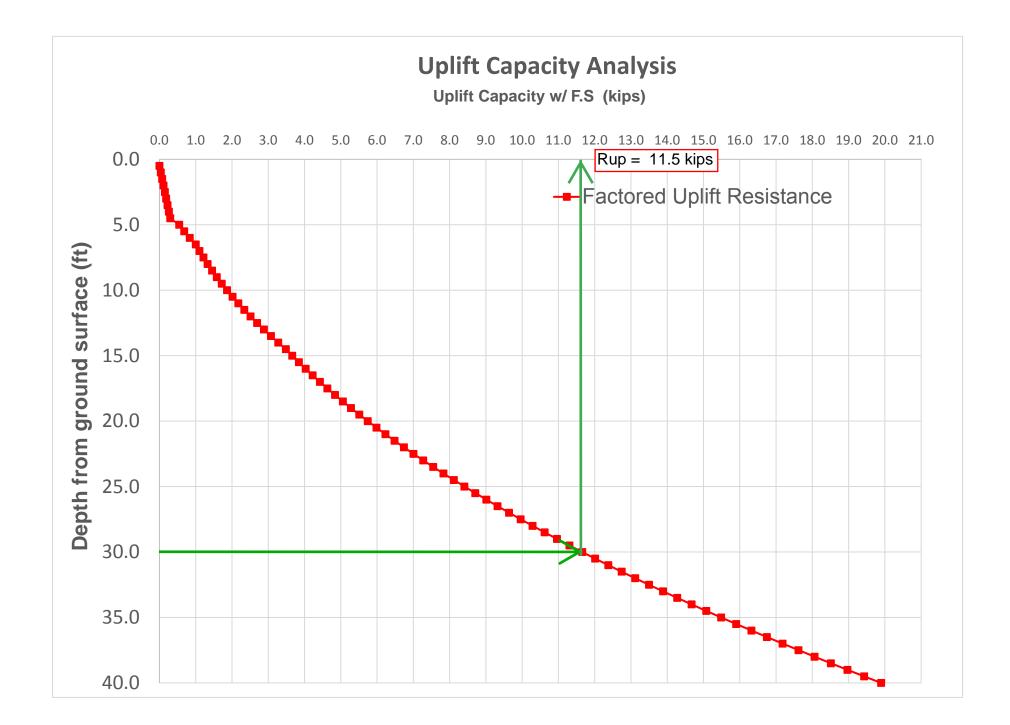
#### Axial Capacity Analysis on Steel piles Ref: United States Department of Transportation of Federal Highway Administration (FHWA) – Design and Construction of Driven Pile Foundations – Volume 1

End Bearing Resistance



			Uplift R	esistance
Q <sub>ult</sub> (kips)	Allowable Toe Resistance (Q <sub>end</sub> ) (kips) (FS = 2)	Total Allowable Capacity (Q <sub>all</sub> ) (kips) (FS = 2)	Φιφ	Accumulated R <sub>uplift</sub> (kips)
0.1	0.1	0.1	0.35	0.0
1.0	0.5	0.6	0.25	0.0
1.0	0.5	0.6	0.25	0.1
1.0	0.5	0.7	0.25	0.1
1.0	0.5	0.8	0.25	0.1
1.0	0.5	0.9	0.25	0.2
1.0	0.5	0.9	0.25	0.2
1.0	0.5	1.0	0.25	0.3
1.0	0.5	1.1	0.25	0.3
6.4	3.2	4.0	0.35	0.5
7.0	3.5	4.5	0.35	0.7
7.6	3.8	5.0	0.35	0.8
7.8	3.9	5.3	0.35	1.0
1.8	0.9	2.5	0.35	1.1
1.8	0.9	2.6	0.35	1.2
1.8	0.9	2.8	0.35	1.3
1.8	0.9	3.0	0.35	1.5
1.8	0.9	3.2	0.35	1.6
1.9	0.9	3.4	0.35	1.7
1.9	0.9	3.6	0.35	1.9
1.9	1.0	3.8	0.35	2.0
1.9	1.0	4.1	0.35	2.2
1.9	1.0	4.3	0.35	2.3
2.0	1.0	4.6	0.35	2.5
2.0	1.0	4.8	0.35	2.7
2.0	1.0	5.1	0.35	2.9
2.0	1.0	5.4	0.35	3.1
2.0	1.0	5.7	0.35	3.3
2.1	1.0	6.0	0.35	3.5
2.0	1.0	6.2	0.35	3.7
2.0	1.0	6.5	0.35	3.8
2.0	1.0	6.8	0.35	4.0
2.0	1.0	7.0	0.35	4.2
2.0	1.0	7.3	0.35	4.4
2.1	1.0	7.6	0.35	4.6
2.1	1.0	8.0	0.35	4.8
2.1	1.0	8.3	0.35	5.1
2.1	1.1	8.6	0.35	5.3
2.1	1.1	8.9	0.35	5.5
2.1	1.1	9.3	0.35	5.7
2.2	1.1	9.6	0.35	6.0
2.2	1.1	10.0	0.35	6.2
2.2	1.1	10.4	0.35	6.5
2.2	1.1	10.7	0.35	6.7
2.2	1.1	11.1	0.35	7.0
2.2	1.1	11.5	0.35	7.3
2.3	1.1	11.9	0.35	7.5
2.3	1.1	12.3	0.35	7.8
2.3	1.1	12.7	0.35	8.1
2.3	1.2	13.2	0.35	8.4
2.3	1.2	13.6	0.35	8.7
2.3	1.2	14.0	0.35	9.0
2.4	1.2	14.5	0.35	9.3
2.4	1.2	15.0	0.35	9.6
2.4	1.2	15.4	0.35	10.0
2.4	1.2	15.9	0.35	10.3
2.4	1.2	16.4	0.35	10.6
2.4	1.2	16.9	0.35	11.0
2.5	1.2	17.4	0.35	11.3
2.5	1.2	17.9	0.35	11.7
2.5	1.2	18.4	0.35	12.0
2.5	1.3	18.9	0.35	12.4
2.5	1.3	19.5	0.35	12.7
2.5	1.3	20.0	0.35	13.1
2.6	1.3	20.6	0.35	13.5
2.6	1.3	21.1	0.35	13.9
2.6	1.3	21.7	0.35	14.3
2.6	1.3	22.3	0.35	14.7
2.6	1.3	22.8	0.35	15.1
2.6	1.3	23.4	0.35	15.5
2.7	1.3	24.0	0.35	15.9
2.7	1.3	24.7	0.35	16.3
2.7	1.3	25.3	0.35	16.7
2.7	1.4	25.9	0.35	17.2
2.7	1.4	26.5	0.35	17.6
2.7	1.4	27.2	0.35	18.1
2.8	1.4	27.8	0.35	18.5
2.8	1.4	28.5	0.35	19.0
2.8	1.4	29.1	0.35	19.4
2.8	1.4	20.9	0.35	10.0





### Wood

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