REPORT

Geotechnical Exploration Water Storage Tank 3090 Gees Mill Road Rockdale County Conyers, Georgia

Project Number 2014.5138.01

November 28, 2014





November 28, 2014

Mr. Pavel Vayner **Rockdale County Water Recourses** Water Treatment – Gees Mill 3090 Gees Mill Road Conyers, GA 30012

Via E-mail: pavel.vayner@rockdalecounty.com

RE: Report of Geotechnical Exploration Water Storage Tank 3090 Gees Mill Road Conyers, Rockdale County, Georgia Project No. 2014.5138.01

Dear Mr. Vayner:

United Consulting is pleased to submit this report of geotechnical exploration for the above referenced project. We appreciate the opportunity to assist you with this project and look forward to working with you during design development and construction phase. Please contact us if you have any questions regarding this report or if we can be of further assistance.

UNITED CONSULTING Mehdi Moa Senior Geotechn

Chris L. Roberds, P.G. Senior Executive Vice President

NP/MM/CLR/nj

ucblade10/sites/Geotechenv/10015/2014.5138.01/Geotechnical Documents/2014.5138.01.geo.doc



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FIGURE

Figure 1 - Boring Location Plan Figure 2 – Subsurface Profile

APPENDIX

General Notes/Narrative of Drilling Operations Boring Logs (16) Exploration Procedure French Drain Detail





EXECUTIVE SUMMARY

United Consulting has completed a Geotechnical Exploration for the proposed 10 million gallon water storage tank to be located at 3090 Gees Mill Road in the city of Conyers, Rockdale County, Georgia. The results of this exploration are briefly summarized below. The text of the report should be reviewed for a discussion of these items.

- 1. A complete geotechnical engineering service is performed through the Observational Method as an indivisible two-phase process. The first phase provides advice about project specific risks and represents our firm's opinion of subsurface conditions with preliminary recommendations. Field observation during construction comprises the second phase of our service and provides us the opportunity to assess the reliability of the subsurface data and the appropriateness of our preliminary recommendations. Actual conditions may differ from those encountered in the exploration phase.
- 2. Up to thirteen (13) feet of fill was encountered in the borings drilled within the site. The fill contained a high concentration of boulder-sized rocks and concrete debris. Based on the provided topographic site plan and finished floor elevations, the fill will be removed from within the water tank footprint during construction.
- 3. Partially weathered rock (PWR) was encountered in the borings at depths ranging from 1 to 18 feet. Auger refusal occurred in the borings at depths ranging from 2 to 32 feet. Based on the existing site elevation and proposed FFE, difficult excavation associated with PWR and rock should be anticipated over most of the water tank footprint.
- 4. Provided the site is prepared as recommended, the proposed water tank may be supported on a shallow foundation system such as slab on grade and perimeter footings. We recommend a uniform modulus of vertical subgrade reaction of 30 pci for design of slabon-grade. The shallow foundation under perimeter footing could be designed for allowable soil bearing pressure of 4,000 psf.
- 5. Partially weathered rock (PWR) or rock was encountered at or above the proposed tank FFE. To mitigate the high cost of isolated excavations in PWR and rock and avoid possible damage to under floor piping laid over an irregular rock surface, we suggest in the areas of the storage tank where PWR or rock is present at or above the foundation bearing level, the storage tank area be excavated to a level of 2 to 3 feet below the bottom of footings and under-floor utilities and brought back to grade with soils compacted to 98% of the material standard Proctor maximum dry density.
- 6. Groundwater was not encountered in the borings at the time of drilling.





PROJECT INFORMATION

The project site is located at 3090 Gees Mill Road in Conyers, Rockdale County, Georgia. At the time of drilling operations, the project site consisted of a wooded tract of land located to the south of an existing storage tank. The project site was bounded to the west and south by a wooded area, to the east by a lake, and to the north by the existing water tank. Based on the provided topographic site plan, there is a steep slope from northeast to southwest near the center of the proposed tank. At the time of our visit, a large quantity of boulder rocks and concrete debris was observed in the high elevation portion of the site (north and northeast of the proposed tank).

The proposed development consists of the construction of a 10 million gallons water tank. We understand that the water tank will be 25 feet high with a diameter of 270 feet. As such, the contact pressure below the tank slab will be about 1,560 psf. Based on the provided information, the proposed finished floor elevation of the tank will be at $724\pm$ feet above mean sea level (msl). The existing site elevation in the proposed water tank area ranged from 724 to 786 feet above msl. Therefore, cuts on the order of 0 to 64 feet are anticipated to achieve the proposed tank finished grade elevation.

A topographic map of the site was provided by the client to use as a guide to locate the boundaries of the project site. The general locations of the borings are shown on the attached boring location plan (Figure 1).

PURPOSE

The purpose of the Geotechnical Exploration was to explore the soils in the area of the proposed water tan and to provide soil and foundation recommendation for the design of the structure.

SCOPE

The scope of our services included the following items:

- 1. A visual reconnaissance of the site from a geotechnical standpoint;
- 2. Drilling five (5) standard penetration test (SPT) and eleven (11) offset borings to determine the nature and condition of the subsurface soils;
- 3. A visual evaluation of the soil samples obtained during our field testing program;
- 4. Analyzing the existing soil conditions with respect to the proposed tank structure.





5. Preparing this report to document the results of the field test program, engineering analysis, and to provide recommendations for foundation design, earthwork, and quality control.

SITE GEOLOGY

This Project Site is located in the Piedmont Physiographic Province. The virgin, "residual" soils (or "residuum") native to this region have been formed by the in-place weathering of the parent crystalline rock. A typical residual soil profile consists of a clayey silt zone from the ground surface, underlain by sandy silts and silty sands. These silts and sands often exhibit the banded appearance of the parent rock. Seams of partially weathered rock (PWR) are often encountered with depth until the sound, relatively unaltered parent rock is encountered. Partially weathered rock (PWR) is a term for the residuum that can be penetrated by soil drilling techniques and has standard penetration test resistance N-values in excess of 100 blows per foot (bpf). Auger refusal indicates the depth at which the boring cannot be drilled further using soil drillings tools and techniques. Auger refusal levels may represent the top of massive bedrock, a boulder or other obstructions.

SUBSURFACE CONDITIONS

Initially, the borings encountered a thin layer of topsoil. Below the topsoil layer, borings B-5 and B-5C encountered fill to auger refusal depths of 6 to 7 feet. Borings B-1, B-5A, and B-5D encountered auger refusal (apparently in the fill) at depths of 2, 9, and 5 feet, respectively. Boring B-5B encountered fill to a depth of 13 feet and boring B-1A encountered fill to a depth of 3 feet. The fill encountered generally consisted of very loose to very dense sand with varying amounts of rock fragments, some silt, and trace amounts of clay. The Standard Penetration Test Resistances (N-values) in the fill soils encountered ranged from 4 to over 100 blows per foot (bpf). The high N-values recorded in the fill was generally due to presence of rock and boulders within the fill.

Below the fill in borings B-1A and B-5B and below the topsoil in borings B-1B, B-2, B-2B, B-3, B-3A, B-3B, and B-4, typical residual soils of the Piedmont Physiographic province were encountered. The residual soils encountered consisted of firm to dense sand with some silt and trace amounts of clay. The N-values in the residual soils encountered ranged from 14 to 34 bpf.

Partially weathered rock (PWR) was encountered in borings B-1A, B-2, B-2B, B-3, B-3A, B-4, and B-5B at depths ranging from 1 to 18 feet. The PWR encountered consisted of very dense sand with some silt and rock fragments, and trace amounts of clay. Auger refusal occurred in the borings at depths ranging from 2 to 32 feet.

Groundwater was not encountered in the borings at the time of drilling. However, groundwater levels should be anticipated to fluctuate with the change of seasons, during periods of very low or high precipitation, or due to changes in the flood plain or watershed upstream from the area.





For a more detailed description of the subsurface conditions encountered, please see the attached boring logs included in the Appendix.

DISCUSSION AND RECOMMENDATIONS

The following recommendations are based on our understanding of the proposed construction, the data obtained in our soil test borings, a site reconnaissance, and our experience with soils and subsurface conditions similar to those encountered at the project site.

United Consulting requests the opportunity for a general review of final design and specifications in order to verify that earthwork and foundation recommendations have been properly interpreted and implemented in the design and specifications. We recommend that United Consulting, as the Geotechnical Engineer of Record, be consulted during construction to conduct Geotechnical Controls as the Owner's Representative. The purpose is to verify the similarity of the subsurface conditions on site versus conditions anticipated by the designers.

Existing Fill

Up to thirteen (13) feet of fill was encountered in the borings drilled in the high elevation portion of the site. Due to the presence of boulders, most of the borings, except boring B-5B, drilled in this area encountered refusal within the fill at depths of 6 to 9 feet. Boring B-5B encountered possible residual at a depth of 13 feet. The near surface fill generally consisted of sand with varying amounts of rock fragments. Based on the existing site elevation and the proposed finished floor elevation, the existing fill will be completely removed from the area of the proposed water storage tank during construction.

Difficult Excavation

Partially weathered rock (PWR) was encountered in the borings at depths ranging from 1 to 18 feet. Auger refusal occurred in the borings at depths ranging from 2 to 32 feet. Auger refusal in the high elevation areas of the site was due to boulder within the fill. The presence of the high concentration of boulders within the fill could result in lower excavation rates in the fill.

Auger refusal due to bedrock occurred in most of the borings. In the areas of borings B-1 to B-1B, B-2 to B-2B, and B-5B, the auger refusal depths were about 7 to 26 feet above the proposed tank bottom elevation. In the areas of boring B-4, PWR was encountered a few feet above the tank bottom elevations. As such difficult excavation associated with PWR and rock should be anticipated over most of the proposed tank area.

Please note that due to the geology of the area, depth to bedrock can vary significantly (as indicated by the borings) over short horizontal distances. Therefore, it is not unusual to encounter pinnacles of rock and PWR at depths shallower than those anticipated by the borings. PWR typically requires loosening by ripping with large dozers pulling single tooth rippers in mass excavation or blasting in confined (trench) excavation.





Conventional scrapers and loaders can generally excavate soils. Lower consistency PWR (50/6", 50/5" and 50/4") typically requires loosening by ripping with large dozers pulling single tooth rippers in mass and trench excavation. Denser PWR (50/3" or denser) may be removed by ripping using large dozer pulling single tooth ripper in mass excavation but generally requires blasting in confined (trench) excavation. Relatively sound, massive, rock typically requires blasting for removal in mass or trench excavation.

Excavation techniques will vary based on the weathering of the materials, fracturing and jointing in the rock, and the overall stratigraphy of the feature. Actual field conditions usually display a gradual weathering progression with poorly defined and uneven boundaries between layers of different materials. We recommend that the following definitions for rock in earthwork excavation be included in bid documents:

- <u>In Mass Excavation:</u> Any material occupying an original volume of more than 1 cubic yard which cannot be excavated with a single-toothed ripper drawn by a crawler tractor having a minimum draw bar pull rating of not less than 80,000 pounds usable pull (Caterpillar D-8 or larger).
- In Trench Excavation: Any material occupying an original volume of more than 1/2 cubic yard which cannot be excavated with a backhoe having a bucket curling rate of not less than 40,000 pounds, using a rock bucket and rock teeth (a John Deere 790 or larger).

Removal of rock by blasting can be very expensive. The costs of excavation vary with the type of material encountered and the quantities to be excavated. Hence, control of quantities is important. You may consider exposing the rock surface prior to blasting so the rock quantities can be more accurately estimated using surveying methods. Leaving soil overburden in place during blasting may result in difficulties in determination of blast rock quantities resulting in greater rock excavation costs. Also, residual soil overburden may increase the confining pressure of the rock and reduce the effectiveness of blast charges. Loose fill or blasting mats can be placed over the blast area to control fly-rock.

We recommend that the surrounding structures be surveyed prior to and upon completion of blasting to document the current conditions of these structures, in order to reduce potential lawsuits.

Ripped PWR and/or blasted rock fragments may be reused and mixed into engineered fill provided that they are pulverized to less than 6 inches in any dimension and fully choked with soil to fill voids between the rock pieces. PWR or rock greater than 12 inches in any dimension may be used in deep fill areas outside the buildings footprint and in non-structural areas and should be well choked with a geotextile fabric or a minimum 6-inch layer of crusher-run or GAB. A minimum of 4 feet of clean fill is recommended over the soil/rock fill.





Site Preparation

As an initial step in site preparation, existing topsoil, trees and their associated root mats should be stripped and disposed offsite. Boulder rocks and concrete debris should be properly disposed. Removal of trees should include removal of their root balls that may extend to several feet below grade.

After lowering the site to achieve the proposed subgrade (anticipated cuts on the order of 0 to 64 feet), the areas underlain by soils, generally the area of borings B-3, should be proofrolled. Proofrolling should be performed under the observation of the Geotechnical Engineer or his representative so that areas, which exhibit "pumping" during proofrolling, may be treated by a method recommended by the Geotechnical Engineer.

Earthwork

The on-site low-plasticity residual soils, if properly moisture conditioned should generally be suitable for reuse as engineered fill. The onsite fill if free of organic should also be suitable for reuse as engineered fill. We recommend that the contractor be equipped for both drying and wetting soils. Also, we recommend that rocks and boulders greater than 6 inches in diameter be separated and properly disposed. Typical restrictions on suitable fill are no organics, plasticity index less than 25, and maximum particle size of four inches, with not more than 30 percent greater than 3/4-inch. These restrictions should also be applied to the imported borrow soils if needed. Positive drainage should be maintained at all times to prevent saturation of exposed soils in case of sudden rains. Rolling the surface of disturbed soils will also improve runoff and reduce the fill soil moisture and construction delays.

Fill Placement

Moisture-density determinations should be performed for each soil type used, to provide data necessary for quality assurance testing. The natural moisture content at the time of compaction should be within moisture content limits, which will allow the required compaction to be obtained. The contractor should be prepared to increase or decrease soil water content.

The fill should be placed in thin lifts (not to exceed 8 inches) and then compacted. We recommend that fill under the proposed storage tank be compacted to at least 98% of Standard Proctor (ASTM D 698) maximum dry density.

A Geotechnical Engineer, or his representative, on a full-time basis should observe all grading operations. In-place density tests taken by that individual will assess the degree of compaction being obtained. The Geotechnical Engineer should determine the frequency of the testing.

Groundwater Conditions

Groundwater was not encountered in the borings at the time of drilling. Therefore, groundwater is not anticipated to impact construction activities at the project site. Due to the presence of <u>PWR</u> and rock above the proposed FFE/FGE, the site is susceptible to formation of perched





water during periods of wet weather. We recommend that upon the excavation of the slope along the eastern-northeastern boundary of the water tank, a toe drain (See Appendix for a detail) be installed. The toe drain should be installed at a depth of at least 3 feet below the water tank proposed FFE/FGE and be "daylighted" further away from the water tank or discharged into a manhole. Over blasting of the rock in the area of the toe drain will be required.

Foundation Design Recommendations

As previously mentioned, the maximum contact pressure exerted by the tank under overflow conditions would be about 1,560 psf below the slab and not more than 4,000 psf for the perimeter ring foundation. Based on the boring data and our settlement analyses, the existing soils are suitable for support of the proposed tank on a conventional shallow foundation system.

Due to dense material (PWR and rock) present below the proposed water storage tank finished floor elevation, undisturbed samples could not be obtained. Based on our analysis using the soil information obtained from the borings, we anticipate settlement across the tank will be from negligible amount to on the order of 1.5 inches or so. The tank footing should bear at 12 inches below outside finished grades for frost protection.

Borings B-1, B-2, B-5, and their associated offsets encountered refusal material above the proposed tank FFE of 724. We suggest the areas of the water storage tank where PWR or rock is present at or above the foundation bearing level be excavated to a level below the bottom of footing and under-floor utilities, between 2 to 3 feet but not to exceed 3 feet, and brought back to grade with soil compacted to 98% of the material standard Proctor maximum dry density. This will mitigate the high cost of isolated excavations in PWR and rock, avoid possible damage to piping laid over an irregular rock surface, and decrease the potential for abrupt differential settlement where footings transition from PWR or rock to soil.

Surface water control should be maintained to prevent accumulation of water in footing excavations. Standing water in footing excavations should be removed promptly. Soil softened by the water should be removed, and the Geotechnical Engineer or his representative should reexamine the area. Our representative must evaluate the storage tank footing excavations prior to concrete placement. The conditions observed should be compared to test boring data and design requirements.

Caving Considerations

Due to the presence of existing fill, some caving of excavations should be expected. Flattening of the excavation sidewalls and/or the use of bracing may be needed to maintain stability. All excavations must be performed in accordance with OSHA excavation safety standards.





LIMITATIONS

This report is for the exclusive use of **Rockdale County Water Resources**, and the designers of the project described herein, and may only be applied to this specific project. Our conclusions and recommendations have been prepared using generally accepted standards of Geotechnical Engineering practice in the State of Georgia. No other warranty is expressed or implied. Our firm is not responsible for conclusions, opinions or recommendations of others.

The right to rely upon this report and the data within may not be assigned without UNITED CONSULTING'S written permission.

The scope of this evaluation was limited to an evaluation of the load-carrying capabilities and stability of the subsoils. Oil, hazardous waste, radioactivity, irritants, pollutants, molds, or other dangerous substance and conditions were not the subject of this study. Their presence and/or absence are not implied or suggested by this report, and should not be inferred.

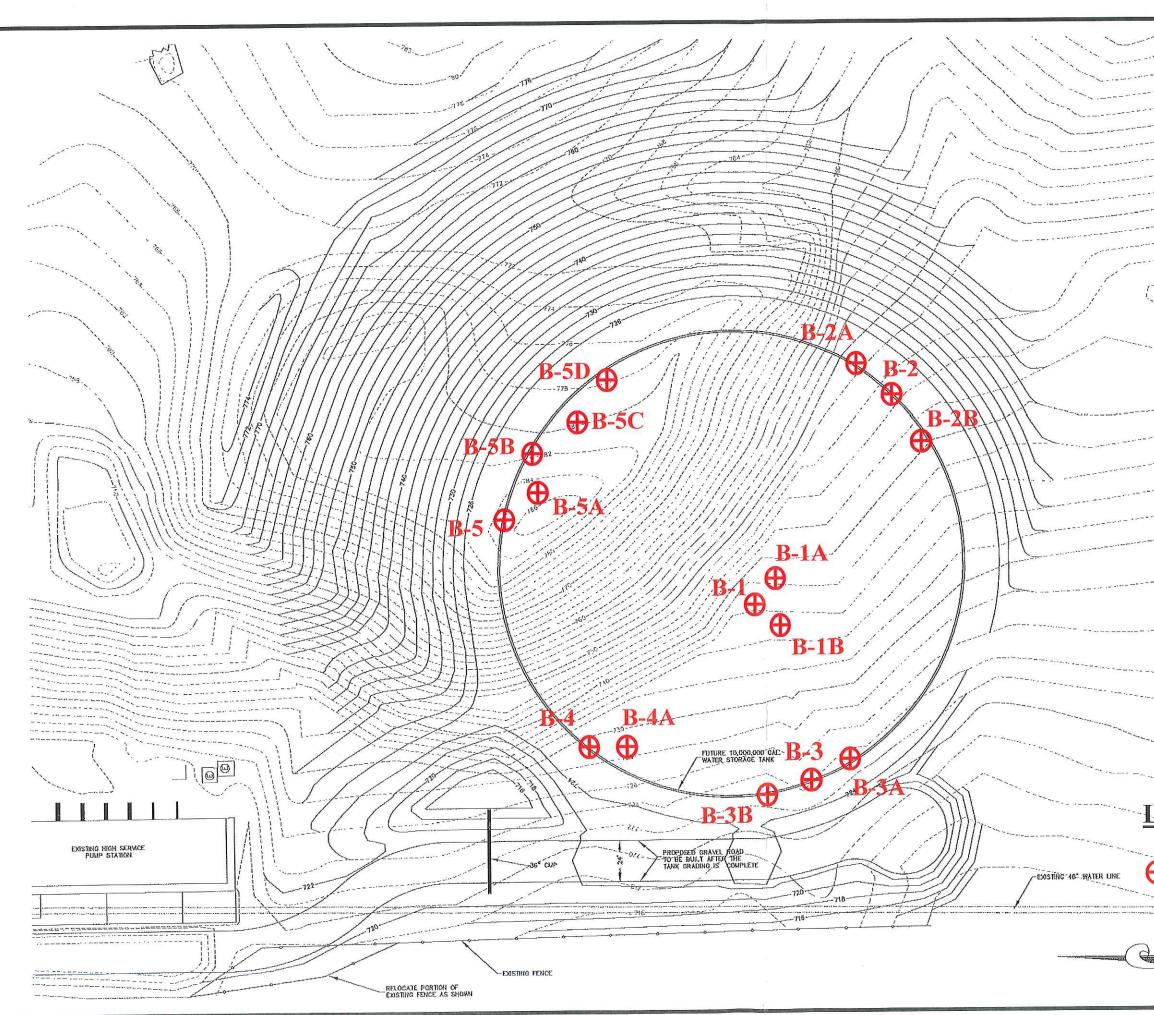
Our conclusions and recommendations are based upon design information furnished us, data obtained from the previously described exploration and testing program and our past experience. They do not reflect variations in subsurface conditions that may exist intermediate of our borings and in unexplored areas of the site. Should such variations become apparent during construction, it will be necessary to re-evaluate our conclusions and recommendations based upon "on-site" observations of the conditions.

If the design or location of the project is changed, the recommendations contained herein, must be considered invalid unless our firm reviews the changes and our recommendations are either verified or modified in writing. When design is complete, we should be given the opportunity to review the foundation plan, grading plan, and applicable portions of the specifications to see if they are consistent with the intent of our recommendations.

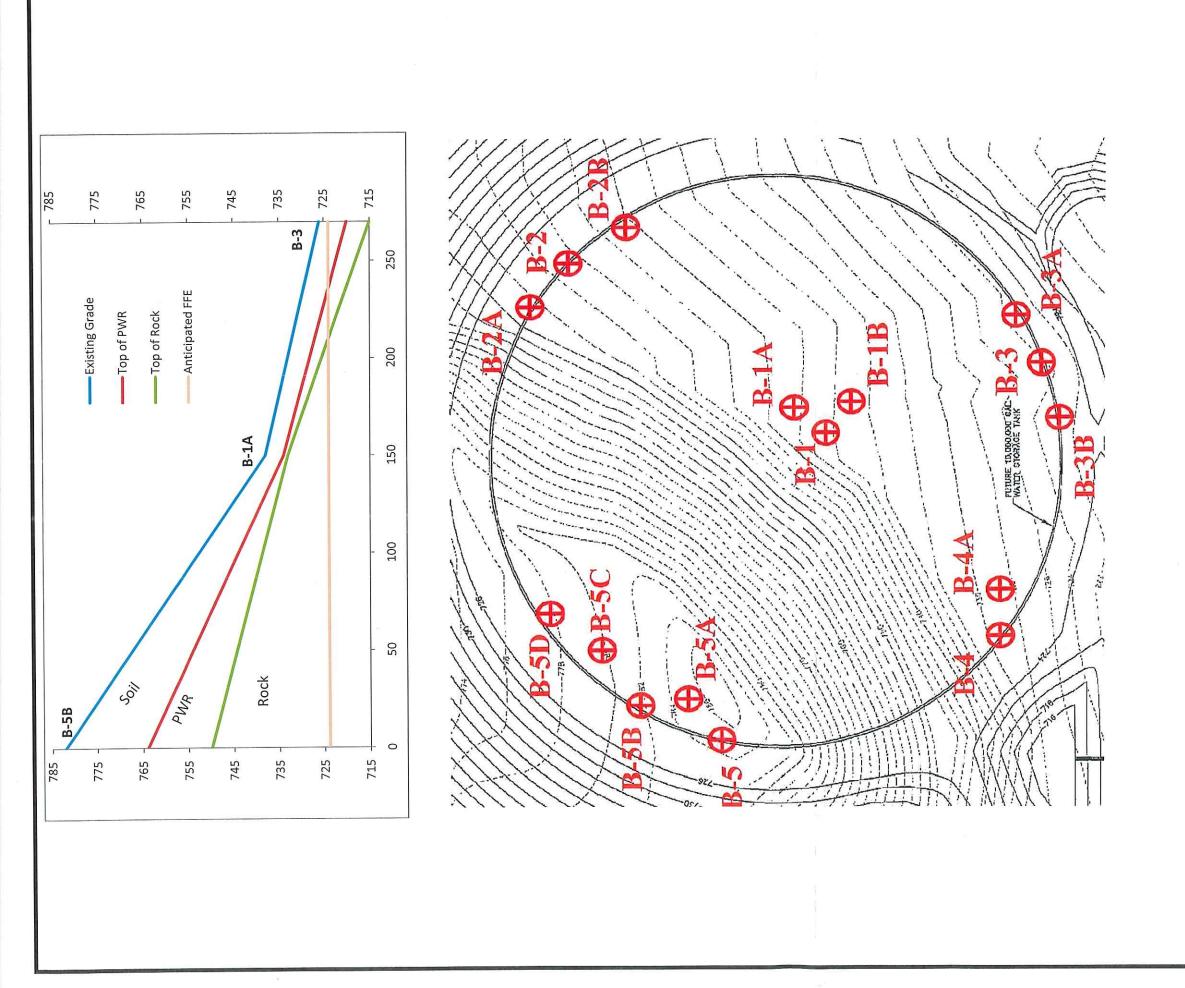
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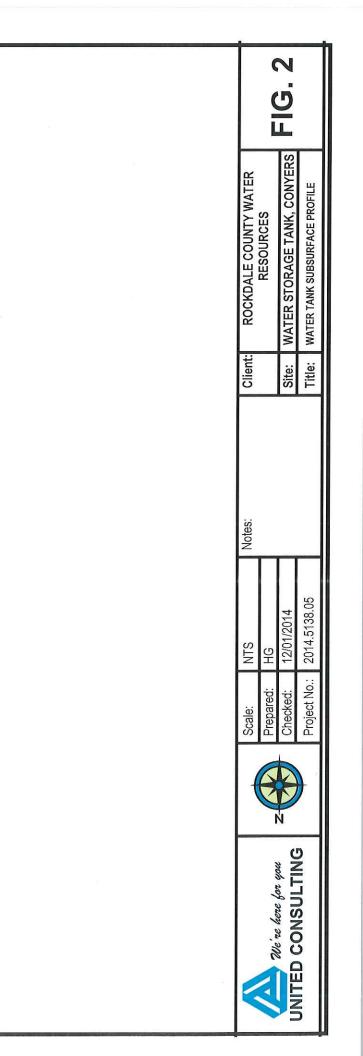






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APPENDIX

General Notes/Narrative of Drilling Operations Logs of Boring (16) Exploration Procedure French Drain Detail

GENERAL NOTES

The soil classifications noted on the Boring Logs are visual classifications unless otherwise noted. Minor constituents of a soil sample are termed as follows:

Тгасе	0 - 10%
Some	11 - 35 %
Suffix "y" or "ey"	36 - 49%

LEGEND



Split Spoon Sample obtained during Standard Penetration Testing



Relatively Undisturbed Shelby Tube Sample



Groundwater Level at Time of Boring Completion



Groundwater Level at 24 hours (or as noted) after Termination of Boring

- w Natural Moisture Content
- LL Liquid Limit
- PL Plastic Limit Atterberg Limits
- PI Plasticity Index
- PF Percent Fines (Percent Passing #200 Sieve)
- 8 d Dry Unit Weight (Pounds per Cubic Foot or PCF
- 8 m Moist or In-Situ Unit Weight (PCF)
- **X** sat Saturated Unit Weight (PCF)

BORING LOG DATA AND NARRATIVE OF DRILLING OPERATIONS

The test borings were made by mechanically advancing helical hollow stem augers into the ground. Samples were covered at regular intervals in each of the borings following established procedures for performing the Standard Penetration Test in accordance with ASTM Specification D-1586. Soil samples were obtained with a standard 1.4" I.D. x 2.0" O.D. split barrel sampler. The sampler is first seated 6" to penetrate any loose cuttings and then driven an additional foot with the blows of a 140 pound hammer freely falling a distance of 30". The number of blows required to drive the sampler each six inches is recorded on the Boring Logs. The total number of blows required to drive the sampler the final foot is designated the "standard penetration resistance." This driving resistance, known as the "N" value, is a measure of the relative density of granular soils and is an indication of the consistency of cohesive deposits.

The Following table describes soil consistencies and relative densities based on standard-penetration resistance values (N) determined by the Standard Penetration Test.

	"N"	Consistency
Clay and Silt	0-2 3-4 5-8 9-15 16-30 Over 31	Very Soft Soft Firm Stiff Very Stiff Hard
	"N"	Relative Density
Sand	0-4 5-10 11-19 20-29 30-49 50+	Very Loose Loose Firm Medium Dense Dense Very Dense

BORING LOG

	CTED WITH: ROCI									
	NAME: WATER S									
DB NO.:	2014.5138.01	DRILLER:					LOGGED BY:	NP		
ELEV.	DESCRIF	PTION	DEPTH in FEET NO. TYPE			SAMPLES			TES	
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ELEV.	DESCRIPTION	DEPTH in		1	SAMPLE				TES
	3" Topsoil	FEET	NO.	TYPE	BLOWS/6"	RECOV.	W		1.1.1.1.
	Sand-some silt, trace clay; very loose; brown (Fill).	0	1		2-2-2	5"		Offset 20 feet so	outheast of B-1
- 735	Coultana ilt trans slavu dangar								
	Sand-some silt, trace clay; dense; brown (Residual)	5	2		19-50/1	4"			
	Partially weathered rock sampled as: sand-some silt and rock fragments, trace clay; very dense;							No groundwater encounter the time of drilling.	
- 730	tan. AUGER REFUSAL AT 5 FEET.	- 							
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	ELEV.	DESCRIPTION	DEPTH in FEET		TYPE	SAMPLE BLOWS/6"	S RECOV.	w	NO	TES
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	-	Sand-some silt, trace clay; dense; brown (Residual).		1		7-11-23	3"			
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	ELEV.	DESCRIPTION	DEPTH in FEET	NO.	TYPE	SAMPLE BLOWS/6"	ES RECOV.	w	N	DTES
	745	3" Topsoil	0							
		Sand-some silt, trace clay and mica; firm; brown (Residual).		1		4-5-12	6"			
	740 -	Partially weathered rock sampled as: sand-some silt and rock fragments, trace clay; very dense;	5	2		50/2	1"		No groundwate	er encountered at
	-	\tan. AUGER REFUSAL AT 5 FEET.							the time of dril	
	- 735		10							
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	- 705		40						FFE = Finish F	loor Elevation

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ELEV.	DESCRIPTION	DEPTH in FEET NO. TYP	SAMPL	ES	w NOT	
	3" Topsoil Straight auger to 4 feet.	0			Offset 30 feet nor	theast of B-2
- 745						
	AUGER REFUSAL AT 4 FEET.	5			No groundwater e the time of drillin	
- 740						
- 735						
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- 715		35				
- 710		40			FFE = Finish Floo	or Elevation

62	NITED CONSULTING 25 HOLCOMB BRIDGE ROAD			_					Sheet 1 of 1
	ORCROSS, GEORGIA 30071 70)209-0029, FAX (770)582-2800			<u>B(</u>	DRING L	OG			
	TED WITH: ROCKDALE COUNT	Y WAT	ΓER	RESC	OURCES		ļ	BORING NO.:	B-2B
	NAME: WATER STORAGE TAN							DATE:	
	2014.5138.01 DRILLER:)AVE		RIG:	CME57	I	LOGGED BY:	NP
ELEV.	DESCRIPTION	DEPTH in	NO.	TYPE	SAMPLES BLOWS/6"	G RECOV.	w		DTES
	3" Topsoil	FEET	NO.	IIME	BLUYYS/0	REGOV.	vv		
- 740	Sand-some silt, trace clay and mica; medium dense; brown (Residual).	0	1		10-17-50/1	6"		Offset 30 feet s	outhwest of B-2
-	Partially weathered rock sampled as: sand-some silt and rock								
- 735	fragments, trace clay; very dense; tan. AUGER REFUSAL AT 4 FEET.	5	2		50/1	0		No groundwate the time of drill	
-									
- - 730		10							
-									
- ~ 725		15							
-		·							
-									
- 720		20							
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- 710		30							
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- 705		35							
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- 700		40		:				FFE = Finish F	loor Elevation

			IYEF	RS, GA	4		[DATE: <u>11/20/14</u>
_			DAVE		RIG:	CME57	L	LOGGED BY: NP
ELEV.	DESCRIPTION	DEPTH in FEET	NO.	TYPE	SAMPLE BLOWS/6"	S RECOV.	w	NOTES
725	3" Topsoil	0						
	Sand-some silt, trace clay and mica; dense; brown (Residual).		1		9-11-22	12"		
720	Partially weathered rock sampled as: sand-some silt and rock fragments, trace clay; very dense;	5	2		50/2	1 [#]		No groundwater encountered a
	∖ <u>tan.</u> AUGER REFUSAL AT 5.5 FEET.							the time of drilling.
715		10						
- 710		15						
~ 705		20						
- 700								
		25						
- 695		30						
690		35						

	TED WITH: <u>ROCKDALE COUNT</u> NAME: WATER STORAGE TAN							BORING NO.: DATE: 11/	
			DAVE			CME57			
ELEV.	DESCRIPTION	DEPTH in FEET	NO.	TYPE	SAMPLE BLOWS/6"	ES RECOV.	W	NOTES	
725	3" Topsoil Straight auger to 8.5 feet.	0						Offset 20 feet south	of B-3
- 720		5							
- 715	Partially weathered rock sampled as: sand-some silt and rock fragments, trace clay; very dense;	10	1		50/5	2"		No groundwater enc	ountered a
- 710	\tan. AUGER REFUSAL AT 10 FEET.							the time of drilling.	
- 705		20		:					
- 700		25							
- 695		30							
- - 690 -		35		W MARY WAY I AMAR AND					



BORING LOG

	NAME: <u>WATER S</u> 2014.5138.01			 	RIG:			DATE: <u>11/20/14</u> _OGGED BY: <u>NP</u>
			DEPTH		SAMPLE			
ELEV.	DESCRIP	TION	in FEET	 TYPE	BLOWS/6"	RECOV.	W	NOTES
725	3" Topsoil		0					
+	Straight auger to 8	feet.						Offset 20 feet north of B-3
,	0 0		armana area					
-								
- 720			5					
- 715	AUGER REFUSAI	L AT 8 FEET.						No groundwater encountered at the time of drilling.
			10					
_			· · · · · · · · · · · · · · · · · · ·					
-								
- 710								
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ŀ								
- 685			1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.					FFE = Finish Floor Elevation

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FFE=724-

UNITED CONSULTING 625 HOLCOMB BRIDGE ROAD NORCROSS, GEORGIA 30071 (770)209-0029, FAX (770)582-2800

BORING LOG

		NAME: WATER STORAGE TAN					011557		DATE: <u>11/20/14</u>
л Р	NO :	2014.5138.01 DRILLER: _			-		CME57	L	OGGED BY: NP
	ELEV,	DESCRIPTION	DEPTH in FEET			SAMPLES		14/	NOTES
┞	730	211 T		NO,	TYPE	BLOWS/6"	RECOV.	W	
+		3" Topsoil	0						
-		Sand-some silt, trace clay; firm; brown (Residual).		1		4-6-8	10"		
-	- 725	Partially weathered rock sampled as: sand- some silt and rock		2		50/5	2"		
		fragments, trace clay; very dense; tan.	5						
	- 720		1995.						
-	- 720	AUGER REFUSAL AT 10 FEET.	10	3		21-50/5	6"		No groundwater encountered at the time of drilling.
-									the time of diming,
	- 715		15						
-									
-	- 710		20						
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	- 705		25						
	- 700								
			30	-					
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-	- 695		35						
	- 690		40						FFE = Finish Floor Elevation

UNITED CONSULTING 625 HOLCOMB BRIDGE ROAD NORCROSS, GEORGIA 30071

(770)209-0029, FAX (770)582-2800

BORING LOG

DB NO.:	NAME: WATER STORAGE TAN 2014.5138.01 DRILLER:		DAVE			CME57		DATE: <u>11/20/14</u> _OGGED BY: <u>NP</u>
		DEPTH	<u> </u>		SAMPLE	S		1
ELEV.	DESCRIPTION	in FEET	NO.	TYPE	BLOWS/6"	RECOV.	w	NOTES
730	3" Topsoil	0						
	Straight auger to 10 feet.							Offset 20 feet South of B-4
- 725		5						
-								
··· 720	AUGER REFUSAL AT 10 FEET.	10						No groundwater encountered at
- 								the time of drilling.
		15						
- 710								
- - - 705 -		25						
- - - 700		30						
~ 695 - -		35						
690								FFE = Finish Floor Elevation

NO	5 HOLCOMB BRIDGE ROAD DRCROSS, GEORGIA 30071			BC	RING LO	CO			
	70)209-0029, FAX (770)582-2800								
	TED WITH: ROCKDALE COUNT							BORING NO.:	
	NAME: WATER STORAGE TAN. 2014.5138.01 DRILLER:					CME57		DATE: LOGGED BY: _	
<u> </u>		DEPTH							
ELEV.	DESCRIPTION	in	NO.	TYPE	SAMPLES BLOWS/6"	RECOV.	w	- N(DTES
- 785	3" Topsoil	0							
-	Sand-significant rock fragments, some silt, trace clay; very dense; brown and tan (Fill).		1		50/5	3"		High N-value o	lue to boulders
- 780	-some rock fragments; very dense	5	2		24-27-32	6"			
-	AUGER REFUSAL AT 7 FEET.		-					No groundwate the time of dril	er encountered
- 775		10	-						U
-									
- 770		15							
			~						
- 765									
- 760		25	-						
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- 755		30	-						
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- 750 -		35							
-			-					,	
- 745		40	4						

	U	NITED CONSULTING						:	Sheet 2 of 2
	N N	25 HOLCOMB BRIDGE ROAD ORCROSS, GEORGIA 30071 '70)209-0029, FAX (770)582-2800		BC	DRING	LOG			
		TED WITH: <u>ROCKDALE COUN</u> NAME: <u>WATER STORAGE TAN</u>						BORING NO.: _ DATE:	
		2014.5138.01 DRILLER:						LOGGED BY:	
	ELEV.	DESCRIPTION	DEPTH in FEET	 TYPE	SAMPLI BLOWS/6"		w	- NO	TES
	-		P						
	- 740 -		45	-					
	-								
	- 735		50						
	-								
	- 730		55						
	- 725								
FFE=724 -									
	- 720		65						
	- 715		70						
			75						
	- 710								
	- 705		80					FFE = Finish Flo	oor Elevation

BORING LOG

ROJECT NAME: WATER STORAGE TANK-CONYERS, GA DATE:	11/20/14
ELEV. DESCRIPTION DEPTH in FEET SAMPLES NO -785 3" Topsoil 0 0 Straight auger to 8.5 feet. 0 -780 5 5 0 0 0 -780 5 5 0 0 No groundwatet	
ELEV. DESCRIPTION in FEET NO. TYPE BLOWS/6" RECOV. W NO -785 3" Topsoil 0 No groundwated -780 -780 - <td>NP</td>	NP
785 3" Topsoil 0 11/2 BLOWS# RECOV. W -785 3" Topsoil 0 0 0 0 0 Straight auger to 8.5 feet. 0 5 0 0 0 -780 5 0 0 0 0	TES
785 Straight auger to 8.5 feet. Offset 20 feet so 780 5 No groundwater	
-780 ALIGER REFUSAL AT 9 EEET 1 50/0 0 No groundwater	outheast of B-5
AUGER REFUSAL AT 9 FEET 1 50/0 0 No groundwater	
AUGER REFUSAL AT 9 FEET 1 50/0 0 No groundwater	
ALIGER REFUSAL AT 9 FEET 1 50/0 0 No groundwater	
AUGER REFUSAL AT 9 FEET 1 50/0 0 No groundwater	
AUGER REFUSAL AT 9 FEET. 10 1 50/0 0 No groundwater the time of drilli	
AUGER REFUSAL AT 9 FEET. 10 1 50/0 0 No groundwater the time of drilli	
AUGER REFUSAL AT 9 FEET. 10 1 50/0 0 No groundwater the time of drilli	
AUGER REFUSAL AT 9 FEET. 10 1 50/0 0 No groundwater the time of drilli	
	encountered a
	uig.
-770	
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- 765	
- 760	
- 755	
750 35	
-745	

BORING LOG

Sheet 2 of 2

CONTRACTED WITH: ROCKDALE COUNTY WATER RESOURCES BORING NO .: B-5A DATE: <u>11/20/14</u> PROJECT NAME: WATER STORAGE TANK-CONYERS, GA JOB NO.: 2014.5138.01 DRILLER: RIG: CME57 LOGGED BY: NP DAVE DEPTH SAMPLES NOTES ELEV. DESCRIPTION in FEET BLOWS/6" RECOV. W NO. TYPE 45 - 740 50 - 735 55 -730 60 725 FFE=724-65 720 70 - 715 75 710 80 - 705 FFE = Finish Floor Elevation

OJECT NAME: WATER STORAGE TANK-CONYERS, GA DATE: B NO.: 2014.5138.01 DRILLER: DAVE RIG: CME57 LOGGED BY: ELEV. DESCRIPTION Image: total stress stress stress some silt, trace clay; very dense; tan (Fill). 0 TYPE BLOWSOF* RECOV. W NC 776 Sand-significant rock fragments, some silt, trace clay; very dense; tan (Fill). 10 1 21-34-50/4 6" High N-value d 776 Sand-some rock fragments and silt, trace clay; very dense; tan (Possible Residual) 15 2 9-10-9 6" 776 Partial weather rock sampled as: sand-some silt and rock fragments, trace clay; very dense; tan. 3 50/1 0 760 Partial weather rock sampled as: sand-some silt and rock fragments, trace clay; very dense; tan. 3 50/1 0 760 Partial weather rock sampled as: sand-some silt and rock fragments, trace clay; very dense; tan. 3 50/1 0 760 Sample classific and rock fragments, trace clay; very dense; tan. 3 50/1 0	
ELEV. DESCRIPTION DEPTH FEE SAMPLES NC 3" Topsoil 0 1 TYPE BLOWS®" RECOV. W NC 780 Straight auger to 8.5 feet. - - - - - Offset 20 feet e 776 - - - - - - - - 776 - - - - - - - - 776 - - - - - - - - 777 Sand-significant rock fragments, some silt, trace clay; very dense; tan (Fill). 1 21-34-50/4 6" - 770 Sand-some rock fragments and silt, trace clay; firm; brown and tan (Possible Residual) 15 2 9-10-9 6" 776 - - - - - - - 770 Sand-some rock fragments, trace clay; very dense; tan. 20 3 50/1 0 776 - - - - - - - 770 Sand-some silt and rock fragments, trace clay; very dense; tan. - - - - 776 - - - - - - -	11/20/14
ELEV. DESCRIPTION Implement NO. TYPE BLOWSIG ¹ RECOV. W NO. 3" Topsoil 0 0 1 Straight auger to 8.5 feet. 0 0 0 0 0 -780 5 - - - 0 0 0 0 -775 - - - - - 0 0 -776 - - - - - 0 -776 - - - - 0 -770 - - - - - -770 - - - - - -770 - - - - - -770 - - - - - -770 - - - - - -770 - - - - - -770 - - - - - -770 - - - - - -770 - - - - - -780 - - - - - -780 - -	NP
Straight auger to 8.5 feet. Offset 20 feet e 780 5 775 5 777 5 778 1 21-34-50/4 6" 10 1 21-34-50/4 6" 10 1 21-34-50/4 6" 10 1 21-34-50/4 6" 10 1 21-34-50/4 6" 10 1 21-34-50/4 6" 11 21-34-50/4 12 9-10-9 13 2 9-10-9 6" (Possible Residual) 15 760 760 760 25 761 26 762 25 763 3 764 50/0 765 760 765 760 765 755 5 50/4 1"	DTES
780 5 775 5 775 5 Sand-significant rock fragments, some silt, trace clay; very dense; tan (Fill). 1 770 2 781 1 782 1 783 1 784 1 785 1 785 1 785 1 786 1 787 1 788 1 789 1 789 1 780 1 781 1 782 1 783 1 784 1 785 1 785 1 786 1 787 1 788 1 789 1 789 1 780 1 781 1 782 1 783 1 784 1 785 1 785 1 786 1 787 1 788 1 799 1 790 1 750 1	est of B-5A
775 5 5 5 5 5 5 5 5 5 5 5 770 1 785 1 785 1 785 20 785 3 785 5 785 1 785 1 785 1 785 1 785 1 780	ast of D-JA
-775 Sand-significant rock fragments, some silt, trace clay; very dense; tan (Fill). 1 21-34-50/4 6" -770 Sand-some rock fragments and silt, trace clay; firm; brown and tan (Possible Residual) 15 2 9-10-9 6" -785 Partial weather rock sampled as: sand-some silt and rock fragments, trace clay; very dense; tan. 3 50/1 0 -760 -760 - - - -	
-775 Sand-significant rock fragments, some silt, trace clay; very dense; tan (Fill). 1 21-34-50/4 6" -770 Sand-some rock fragments and silt, trace clay; firm; brown and tan (Possible Residual) 15 2 9-10-9 6" -785 Partial weather rock sampled as: sand-some silt and rock fragments, trace clay; very dense; tan. 3 50/1 0 -760 -760 - - - -	
Sand-significant rock fragments, some silt, trace clay; very dense; tan (Fill). 1 21-34-50/4 6" -770 Sand-some rock fragments and silt, trace clay; firm; brown and tan (Possible Residual) 15 9-10-9 6" -785 Partial weather rock sampled as: sand-some silt and rock fragments, trace clay; very dense; tan. 3 50/1 0 -760 25 4 50/0 0 5 50/4 1"	
Sand-significant rock fragments, some silt, trace clay; very dense; tan (Fill). 1 21-34-50/4 6" -770 Sand-some rock fragments and silt, trace clay; firm; brown and tan (Possible Residual) 15 9-10-9 6" -785 Partial weather rock sampled as: sand-some silt and rock fragments, trace clay; very dense; tan. 3 50/1 0 -760 25 4 50/0 0 5 50/4 1"	
some silt, trace clay; very dense; tan (Fill). 770 Sand-some rock fragments and silt, trace clay; firm; brown and tan (Possible Residual) 785 Partial weather rock sampled as: sand-some silt and rock fragments, trace clay; very dense; tan. 760 760 760 765 765 760 765 765 765 765 765 765 765 765	
some silt, trace clay; very dense; tan (Fill). 770 Sand-some rock fragments and silt, trace clay; firm; brown and tan (Possible Residual) 785 Partial weather rock sampled as: sand-some silt and rock fragments, trace clay; very dense; tan. 760 760 760 765 765 760 765 765 765 765 765 765 765 765	
tan (Fill). -770 Sand-some rock fragments and silt, trace clay; firm; brown and tan (Possible Residual) -785 Partial weather rock sampled as: sand-some silt and rock fragments, trace clay; very dense; tan. -760 -765 -760 -760 -760 -760 -760 -760 -761 -762 -763 -764 -765 -765 -760 -	lue to boulder
-770 Sand-some rock fragments and silt, trace clay; firm; brown and tan (Possible Residual) 15 2 9-10-9 6" -785 -785 - - - - Sample classific materials cut out the second	
Sand-some rock fragments and silt, trace clay; firm; brown and tan (Possible Residual) 15 9-10-9 6" -785 -785 - - - Sample classific materials cut out out out out out out out out out o	
trace clay; firm; brown and tan (Possible Residual) 15 9-10-9 6" -765 -765 -	
(Possible Residual) -765 Partial weather rock sampled as: sand-some silt and rock fragments, trace clay; very dense; tan. -760 -755 -755 -755 -755 -755 -755 -755 -755 -755 -755 -760 -760 -755 -757 -755 -755 -757 -755 -755 -757 -755 -757 -755 -757 -755 -757 -755 -757 -755 -757 -755 -757 -755 -757 -755 -757 -755 -757 -755 -757 -755 -757 -755 -757 -755 -757 -755 -757 -755 -757 -755 -757	
-765 Partial weather rock sampled as: sand-some silt and rock fragments, trace clay; very dense; tan. 3 50/1 0 -760 -760 -760 -755 -755 5 50/4 1"	
Partial weather rock sampled as: sand-some silt and rock fragments, trace clay; very dense; tan. 760 775 775 775 775 775 775 775 77	
- 760 - 755 - 755 - 755 - 755 - 755 - 755 - 755 - 755 - 760 - 755 - 757 - 755 - 757 - 757	
-760 -755 -755	
	it from auger
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5 50/4 1"	
5 50/4 1"	
<u> </u>	
AUGER REFUSAL AT 32 FEET.	
the time of drill	ling.
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- 745	

BORING LOG

Sheet 2 of 2

CONTRACTED WITH: ROCKDALE COUNTY WATER RESOURCES BORING NO.: B-5B DATE: _____11/20/14 PROJECT NAME: WATER STORAGE TANK-CONYERS, GA LOGGED BY: NP RIG: CME57 JOB NO.: 2014.5138.01 DRILLER: DAVE DEPTH SAMPLES NOTES DESCRIPTION ELEV. in FEET BLOWS/6" RECOV. W NO. TYPE - 740 45 - 735 50 - 730 55 - 725 FFE=724~ 60 - 720 65 - 715 70 - 710 75 - 705 80 FFE = Finish Floor Elevation 700

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BORING LOG

	TED WITH: ROCI									B-5C
	NAME: WATER S								DATE:1 .OGGED BY:	1/20/14
3 NO.: _	2014.5138.01					CME57	L	NP		
ELEV.	DESCRIPTION		DEPTH			SAMPLE	ES		NOT	EQ
ELEV.			in FEET	NO.	TYPE	BLOWS/6"	RECOV.	w		L0
	3" Topsoil		0							
- 780	Sand-significant r	ock fragments,		1		5-5-50/1	6"		High N-value due	to boulders
-	some silt, trace cla	iy; very dense;		<u> </u>				-		
	brown (Fill).									
				 				_		
	-trace rock fragme	ents; medium		2		10-12-13	10"			
~ 775	dense		5							
.									No groundwater e	encountered at
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	UNITED CONSULTING								Sheet 2 of 2
	625 HOLCOMB BRIDGE ROAD NORCROSS, GEORGIA 30071 (770)209-0029, FAX (770)582-2800			<u>BC</u>	RING	LOG			
CONTRA	CTED WITH: ROCKDALE COUN	TY WAT	ER F	RESO	URCES		E	BORING NO .:	B-5C
PROJEC	T NAME: WATER STORAGE TAN	IK-CON	YER	S, GA				DATE:	
JOB NO.:	: <u>2014.5138.01</u> DRILLER:	D	AVE		_ RIG:	CME57	L	OGGED BY:	NP
ELEV	/. DESCRIPTION	DEPTH in			SAMPLI	ES		- N	OTES
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BORING LOG

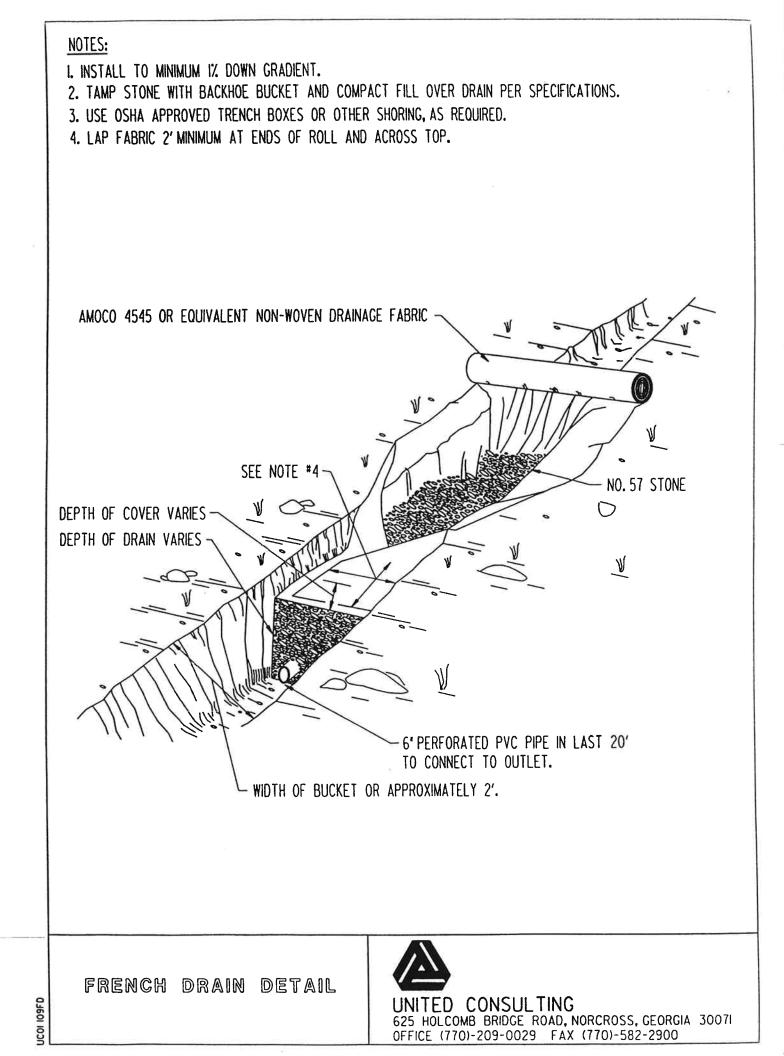
CONTRAC	TED WITH: ROCKDALE COUN	TY WA	FER	RESC				BORING NO.:	
ROJECT NAME: WATER STORAGE TANK-CONYERS, GA								DATE:11	/20/14
JOB NO.:	2014.5138.01 DRILLER:]	DAVE	=	RIG:	CME57	L	OGGED BY:	NP
ELEV.	DESCRIPTION	DEPTH in FEET	NO.	TYPE	SAMPLE BLOWS/6"	RECOV.	w	NOTE	S
-	3" Topsoil Straight auger to 5 feet.	0						Offset 20 feet east	of B-5C
- 775	AUGER REFUSAL AT 5 FEET.							No groundwater en	countered at
- 770		10						the time of drilling	,
- 765									
- - 760 -									
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- - 750 -		30							
- 745		35							
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OJECT I	TED WITH: <u>ROCKDALE COUI</u> NAME: <u>WATER STORAGE TA</u> 2014.5138.01 DRILLER:	ANK-CON	IYER	rs, ga	۱		[DATE:	11/20/14
ELEV.	DESCRIPTION	DEPTH		-	SAMPLE	ES			DTES
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EXPLORATION PROCEDURES

Five (5) SPT (designated as B-1 and B-5) and eleven (11) offset borings were drilled during this subsurface exploration. The approximate locations of the borings are indicated on the attached Boring Location Plan (Figure 1) provided in the Appendix. The SPT borings were performed in general accordance with ASTM D 1586. Soil samples obtained using the split spoon sampler were visually evaluated by the Project Engineer and visually evaluated according to the visual-manual procedure described in ASTM D 2488. A narrative of field operations is included in The Appendix.

Boring locations were determined in the field by the Project Engineer by measuring distances and estimating angles from existing site features and should be considered approximate. The elevations shown on the boring logs were obtained from the provided topographic site plan by interpolation and should be considered *very* approximate.



Important Information About Your Geotechnical Engineering Report

Subsurface problems are a principal cause of construction delays, cost overruns, claims, and disputes.

The following information is provided to help you manage your risks.

Geotechnical Services Are Performed for Specific Purposes, Persons, and Projects

Geotechnical engineers structure their services to meet the specific needs of their clients. A geotechnical engineering study conducted for a civil engineer may not fulfill the needs of a construction contractor or even another civil engineer. Because each geotechnical engineering study is unique, each geotechnical engineering report is unique, prepared *solely* for the client. No one except you should rely on your geotechnical engineering report without first conferring with the geotechnical engineer who prepared it. *And no one* — *not even you* — should apply the report for any purpose or project except the one originally contemplated.

Read the Full Report

Serious problems have occurred because those relying on a geotechnical engineering report did not read it all. Do not rely on an executive summary. Do not read selected elements only.

A Geotechnical Engineering Report is Based on A Unique Set of Project-Specific Factors

Geotechnical engineers consider a number of unique, project-specific factors when establishing the scope of a study. Typical factors include: the client's goals, objectives, and risk management preferences; the general nature of the structure involved, its size, and configuration; the location of the structure on the site; and other planned or existing site improvements, such as access roads, parking lots, and underground utilities. Unless the geotechnical engineer who conducted the study specifically indicates otherwise, do not rely on a geotechnical engineering report that was:

- not prepared for you,
- not prepared for your project,
- · not prepared for the specific site explored, or
- completed before important project changes were made.

Typical changes that can erode the reliability of an existing geotechnical engineering report include those that affect:

 the function of the proposed structure, as when it's changed from a parking garage to an office building, or from a light industrial plant to a refrigerated warehouse,

- elevation, configuration, location, orientation, or weight of the proposed structure,
- composition of the design team, or
- project ownership.

As a general rule, *always* inform your geotechnical engineer of project changes—even minor ones—and request an assessment of their impact. *Geotechnical engineers cannot accept responsibility or liability for problems that occur because their reports do not consider developments of which they were not informed.*

Subsurface Conditions Can Change

A geotechnical engineering report is based on conditions that existed at the time the study was performed. *Do not rely on a geotechnical engineering report* whose adequacy may have been affected by: the passage of time; by man-made events, such as construction on or adjacent to the site; or by natural events, such as floods, earthquakes, or groundwater fluctuations. *Always* contact the geotechnical engineer before applying the report to determine if it is still reliable. A minor amount of additional testing or analysis could prevent major problems.

Most Geotechnical Findings Are Professional Opinions

Site exploration identifies subsurface conditions only at those points where subsurface tests are conducted or samples are taken. Geotechnical engineers review field and laboratory data and then apply their professional judgment to render an opinion about subsurface conditions throughout the site. Actual subsurface conditions may differ—sometimes significantly—from those indicated in your report. Retaining the geotechnical engineer who developed your report to provide construction observation is the most effective method of managing the risks associated with unanticipated conditions.

A Report's Recommendations Are Not Final

Do not overrely on the construction recommendations included in your report. *Those recommendations are not final*, because geotechnical engineers develop them principally from judgment and opinion. Geotechnical engineers can finalize their recommendations only by observing actual

subsurface conditions revealed during construction. *The geotechnical engineer who developed your report cannot assume responsibility or liability for the report's recommendations if that engineer does not perform construction observation.*

A Geotechnical Engineering Report is Subject to Misinterpretation

Other design team members' misinterpretation of geotechnical engineering reports has resulted in costly problems. Lower that risk by having your geotechnical engineer confer with appropriate members of the design team after submitting the report. Also retain your geotechnical engineer to review pertinent elements of the design team's plans and specifications. Contractors can also misinterpret a geotechnical engineer participate in prebid and preconstruction conferences, and by providing construction observation.

Do Not Redraw the Engineer's Logs

Geotechnical engineers prepare final boring and testing logs based upon their interpretation of field logs and laboratory data. To prevent errors or omissions, the logs included in a geotechnical engineering report should *never* be redrawn for inclusion in architectural or other design drawings. Only photographic or electronic reproduction is acceptable, *but recognize that separating logs from the report can elevate risk.*

Give Contractors a Complete Report and Guidance

Some owners and design professionals mistakenly believe they can make contractors liable for unanticipated subsurface conditions by limiting what they provide for bid preparation. To help prevent costly problems, give contractors the complete geotechnical engineering report, *but* preface it with a clearly written letter of transmittal. In that letter, advise contractors that the report was not prepared for purposes of bid development and that the report's accuracy is limited; encourage them to confer with the geotechnical engineer who prepared the report (a modest fee may be required) and/or to conduct additional study to obtain the specific types of information they need or prefer. A prebid conference can also be valuable. *Be sure contractors have sufficient time* to perform additional study. Only then might you be in a position to give contractors the best information available to you, while requiring them to at least share some of the financial responsibilities stemming from unanticipated conditions.

Read Responsibility Provisions Closely

Some clients, design professionals, and contractors do not recognize that geotechnical engineering is far less exact than other engineering disciplines. This lack of understanding has created unrealistic expectations that

have led to disappointments, claims, and disputes. To help reduce the risk of such outcomes, geotechnical engineers commonly include a variety of explanatory provisions in their reports. Sometimes labeled "limitations" many of these provisions indicate where geotechnical engineers' responsibilities begin and end, to help others recognize their own responsibilities and risks. *Read these provisions closely*. Ask questions. Your geotechnical engineer should respond fully and frankly.

Geoenvironmental Concerns Are Not Covered

The equipment, techniques, and personnel used to perform a *geoenviron-mental* study differ significantly from those used to perform a *geotechnical* study. For that reason, a geotechnical engineering report does not usually relate any geoenvironmental findings, conclusions, or recommendations; e.g., about the likelihood of encountering underground storage tanks or regulated contaminants. *Unanticipated environmental problems have led to numerous project failures.* If you have not yet obtained your own geoenvironmental information, ask your geotechnical consultant for risk management guidance. *Do not rely on an environmental report prepared for someone else.*

Obtain Professional Assistance To Deal with Mold

Diverse strategies can be applied during building design, construction, operation, and maintenance to prevent significant amounts of mold from growing on indoor surfaces. To be effective, all such strategies should be devised for the express purpose of mold prevention, integrated into a comprehensive plan, and executed with diligent oversight by a professional mold prevention consultant. Because just a small amount of water or moisture can lead to the development of severe mold infestations, a number of mold prevention strategies focus on keeping building surfaces dry. While groundwater, water infiltration, and similar issues may have been addressed as part of the geotechnical engineering study whose findings are conveyed in this report, the geotechnical engineer in charge of this project is not a mold prevention consultant; none of the services performed in connection with the geotechnical engineer's study were designed or conducted for the purpose of mold prevention. Proper implementation of the recommendations conveyed in this report will not of itself be sufficient to prevent mold from growing in or on the structure involved.

Rely, on Your ASFE-Member Geotechncial Engineer for Additional Assistance

Membership in ASFE/The Best People on Earth exposes geotechnical engineers to a wide array of risk management techniques that can be of genuine benefit for everyone involved with a construction project. Confer with you ASFE-member geotechnical engineer for more information.



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