

L. E. STIFFLER, Engineer, LLC
309 West Laurel Avenue
Foley, Alabama 36535

251-943-8501
251-943-8441 (FAX)
randy@lesengr.com

27 May, 2014

City of Orange Beach
PO Box 458
Orange Beach, AL 36561

RE: Orange Beach Fire Station #5

Gentleman:

The contractor EJ builders asked me to verify the foundation slab would carry the load of a 56,000 lb fire truck on a 5" slab, 3000 psi, with 6/6 W2.9/2.9 wire mesh.

I have checked the loads and find no issues with this configuration, assuming the soil has a min. capacity of between 1500 and 2000 psf.

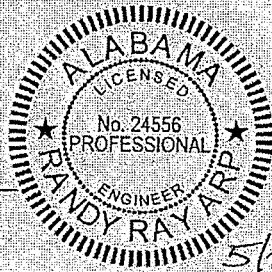
Concrete slab loads are more dependent on the the compaction and quality of the base material and soil. Also note a change from 3000 psi concrete to 4000 psi concrete will increase the factor of safety from 2.7 to 3.1.

Let me know if you have any questions.

Sincerely,



Randy Ray Arp P.E.
Alabama #24556



5/27/14

* Licensed Professional Engineer * Planner * Construction Manager * Job 140504

OB. L. W. S. 10/14

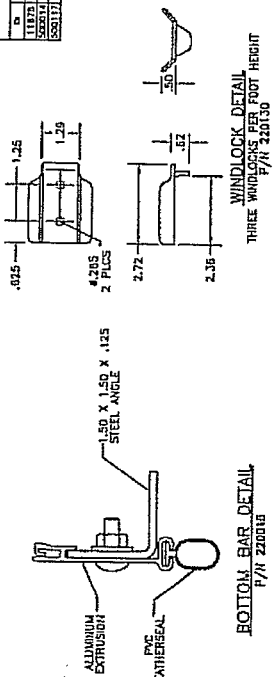
- NOTES**
- DESIGNED AND TESTED IN ACCORDANCE WITH FLORIDA BLDG CODE AND INTERNATIONAL BLDG CODE WITHIN 6 INCHES OF FLOOR.
 - PRESSURES LISTED AS DESIGN PSF.
 - CONCRETE JAMBS SHALL BE 3000 PSI CONCRETE MINIMUM.
 - WOOD JAMBS SHALL BE SOUTHERN YELLOW PINE (SP. GR. = 0.55) MINIMUM.
 - APPROVED CONCRETE ANCHORS: TAPCON, POWERS POWERBOLT, HILTI KWIBOLT 3 OR EQUIVALENT.
 - STEEL GAUGE THICKNESSES PER DASHA TDS#154.

- 8. JAMB CONSTRUCTION AND DESIGN BY OTHERS. JAMBS MUST BE DESIGNED TO WITHSTAND THE MAXIMUM DESIGN WIND AND PARALLEL FORCES IMPOSED ON THEM BY THE DOOR, WINDOW, OR FLOOR HEIGHT.**
- GUIDE 1:** MOMENT = 183 IN-LBS/FT OF DOOR HEIGHT
NORMAL = 188 LBS/FT OF DOOR HEIGHT
PARALLEL = 358 LBS/FT OF DOOR HEIGHT
- GUIDE 2:** MOMENT = 177 IN-LBS/FT OF DOOR HEIGHT
NORMAL = 248 LBS/FT OF DOOR HEIGHT
PARALLEL = 448 LBS/FT OF DOOR HEIGHT

REVISIONS

NO.	DATE	DESCRIPTION
1	8/17/04	ISSUED FOR PERMITS
2	7/27/04	ISSUED FOR PERMITS
3	7/27/04	ISSUED FOR PERMITS

John E. Seaton
 JOHN E. SEATON, P.E.
 REGISTERED PROFESSIONAL ENGINEER
 FL # 12111-RZ

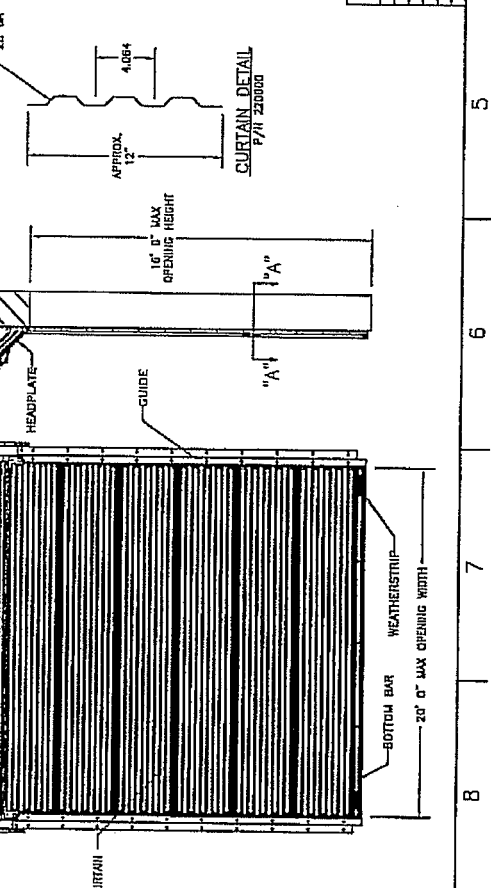
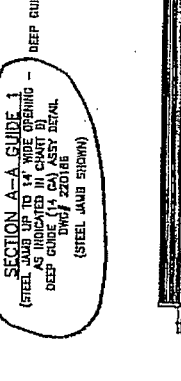
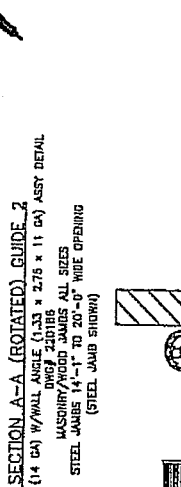


GUIDE 1 SPECIFICATION

JAMB TYPE	22-22 IN	28-28 IN	31-31 IN	41-41 IN
STEEL	S1	S1	S1	S1
CONCRETE	C1	C1	C1	C1
WOOD	W1	W1	W1	W1
STEEL	S2	S2	S2	S2
CONCRETE	C2	C2	C2	C2
WOOD	W2	W2	W2	W2
STEEL	S3	S3	S3	S3
CONCRETE	C3	C3	C3	C3
WOOD	W3	W3	W3	W3

GUIDE 2 SPECIFICATION

JAMB TYPE	22-22 IN	28-28 IN	31-31 IN	38-38 IN	41-41 IN
STEEL	S1	S1	S1	S1	S1
CONCRETE	C1	C1	C1	C1	C1
WOOD	W1	W1	W1	W1	W1
STEEL	S2	S2	S2	S2	S2
CONCRETE	C2	C2	C2	C2	C2
WOOD	W2	W2	W2	W2	W2
STEEL	S3	S3	S3	S3	S3
CONCRETE	C3	C3	C3	C3	C3
WOOD	W3	W3	W3	W3	W3



JAMB AND FASTER DEFINITIONS

PASTER:	DEFINITION
S1	1/4"-20 SELF DRILLING SCREW
S2	12" SPACING
S3	JAMB STEEL 14 GA THICK MIN.
C1	1/4"-20 SELF DRILLING SCREW
C2	12" SPACING
C3	JAMB STEEL 12 GA THICK MIN.
W1	1/4"-20 SELF DRILLING SCREW
W2	12" SPACING
W3	JAMB STEEL 12 GA THICK MIN.

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Basic Wind Speed 170 mph
Exposure Category B

Structure Information

Building Length 60 ft
Building Width 40 ft
Mean Roof Height 16 ft
Roof Angle > 10°
Enclosure Classification Enclosed

Door Information

Door Width 12 ft
Door Height 14 ft
Distance From Edge of Door to Corner of Building 6 ft

Positive Design Pressure	26.1 psf
Negative Design Pressure	-28.8 psf

L.E. Stiffler, Engineer LLC

Project : OB Fire Station
 Subject : 170 wind load
 Location : Orange Beach, AL

File : 140504
 Date : 8/15/2014
 Eng : RRA

Design Wind Pressure, p, Equation 30.4-1 (ASCE 7-10).

System Type	Structure Type	Equation
Components and Cladding (Envelope Procedure)	Low-Rise Buildings with h ≤ 60 ft Gabled & Hipped Roofs	$p = qh[(GCp) - (GCpi)]$ qh : velocity pressure at h GCp : Figures 30.4-1 & 30.4-2 $GCpi$: Table 26.11-1

Velocity Pressure Calculations:

Velocity pressure qh is calculated in accordance with section 30.3.

qh = Velocity pressure @ mean roof height (h)

$$qh = \text{Constant} \cdot K_h \cdot K_{zt} \cdot K_d \cdot V^2$$

(Eq 30.3-1)

Where : Constant = Numerical Constant (Section C27.3.2)

$$= \frac{1}{2} \cdot \left[\left(\frac{\text{Air density lb/cu ft}}{32.2 \text{ ft/s}^2} \right) \cdot \left[\left(\frac{\text{mi/h}}{5280 \text{ ft/mi}} \cdot \left(\frac{1 \text{ hr}}{3600 \text{ s}} \right) \right)^2 \right] \right]$$

$$= 0.00256$$

Mean Sea Level = 10.00 ft

Air Density @MSL = 0.0765 lb/cu ft (Table C27.3-2)

Occupancy Category = III (Table 1.5-1)

Exposure Category = B (Section 26.7.3)

α = 7.00 (Table 26.9-1)

Z_g = 1,200.00 ft (Table 26.9-1)

Basic Wind Speed = 170.00 mph (Figure 26.5-1 A-C)

Mean Roof Height = 16.00 ft

Where : K_h = Velocity pressure coefficient @ height h
 $= 2.01 \cdot (Z/Z_g)^{2/\alpha}$ for $15 \text{ ft} \leq Z \leq Z_g$ (Table 30.3-1)

$$= 2.01 \cdot (15/Z_g)^{2/\alpha} \text{ for } Z < 15 \text{ ft}$$

$$= 0.70$$

K_{zt} = Topographic factor (Figure 26.8-1)

$$= (1 + K_1 \cdot K_2 \cdot K_3)^2$$

Topography = None

$K_{zt @h}$ = 1.00

K_d = Wind directionality factor (Table 26.6-1)

$$= 0.85$$

qh = 44.06 (psf)

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Internal Pressure Coefficient, G_{Cpi} , Table 26.11-1

Enclosure Classification	G_{Cpi+}	G_{Cpi-}	A_{og} (sq. ft.)	V_i (cu. ft.)	R_i	G_{Cpi+}	G_{Cpi-}
Enclosed Buildings	0.18	-0.18	60	5,000,000	1.00	0.18	-0.18

External Pressure Coefficients, G_{Cp} , Figure 30.4-2 (roof) and Figure 30.4-1 (walls)

Zone	Area (sq. ft.)	Angle (deg)	G_{Cp+}	G_{Cp-}	G_{Cp} R. O.
1	150.00	9.76	0.30	-0.80	-
2	150.00	9.76	0.30	-1.20	-2.20
3	150.00	9.76	0.30	-2.00	-2.50
4	150.00	All	0.71	-0.80	-
5	150.00	All	0.71	-0.89	-

Values of G_{Cp} for walls (zone 4 & 5) were reduced by 10%

Design Wind Pressure, p , Equation 30.4-1.

Zone	q_h (psf)	G_{Cp+}	G_{Cp-}	G_{Cpi+}	G_{Cpi-}	p_{1+} (psf)	p_{2+} (psf)	p_{1-} (psf)	p_{2-} (psf)
1	44.06	0.30	-0.80	0.18	-0.18	5.29	21.15	-43.18	-27.32
2	44.06	0.30	-1.20	0.18	-0.18	5.29	21.15	-60.80	-44.94
3	44.06	0.30	-2.00	0.18	-0.18	5.29	21.15	-96.05	-80.18
4	44.06	0.71	-0.80	0.18	-0.18	23.49	39.35	-43.31	-27.45
5	44.06	0.71	-0.89	0.18	-0.18	23.49	39.35	-46.97	-31.11

Positive and negative values of external and internal pressures are combined to determine four possible pressures:

p_{1+} uses G_{Cp+} and G_{Cpi+} p_{1-} uses G_{Cp-} and G_{Cpi+}

p_{2+} uses G_{Cp+} and G_{Cpi-} p_{2-} uses G_{Cp-} and G_{Cpi-}

Roof Overhang Pressure, p , Equation 30.10-1.

Wind pressures acting on the roof overhang (soffit pressures not included).

Zone	q_h (psf)	G_{Cp-} (R.O.)	G_{Cpi+}	G_{Cpi-}	p_{1-} (psf)	p_{2-} (psf)
1	44.06	-1.00	0.18	-0.18	-51.99	-36.13
2	44.06	-2.20	0.18	-0.18	-104.86	-89.00
3	44.06	-2.50	0.18	-0.18	-118.07	-102.21

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Design Wind Pressure, p, Equation 28.4-1 (ASCE 7-10)

System Type	Structure Type	Equation
Main Wind Force Resisting System (Envelope Procedure)	Rigid Structures Low-Rise Buildings	$p = qh \cdot [(GCpf) - (GCpi)]$ qh : velocity pressure at h GCpf : Figure 28.4-1 GCpi : Table 26.11-1

Velocity Pressure Calculations:

Velocity pressure qh is calculated in accordance with section 28.3.2.

qh = Velocity pressure @ mean roof height (h)

$$qh = \text{Constant} \cdot K_h \cdot K_{zt} \cdot K_d \cdot V^2 \quad (\text{Eq 28.3-1})$$

Where : Constant = Numerical Constant
 = $\frac{1}{2} \cdot \left[\left(\frac{\text{Air density lb/cu ft}}{32.2 \text{ ft/s}^2} \right) \cdot \left(\frac{\text{mi/h}}{5280 \text{ ft/mi}} \cdot \left(\frac{1 \text{ hr}}{3600 \text{ s}} \right) \right)^2 \right]$ (Section C27.3.2)
 = 0.00256

Mean Sea Level = 10 ft (Table C27.3-2)

Air Density @ MSL = 0.0765 lb/cu ft (Table 1.5-1)

Occupancy Category = III (Section 26.7.3)

Exposure Category = B (Table 26.9-1)

α = 7.00 (Table 26.9-1)

Z_g = 1,200.00 ft (Table 26.9-1)

Basic Wind Speed = 170.00 mph (Figure 26.5-1 A-C)

Mean Roof Height = 16.00 ft

Where : K_h = Velocity pressure coefficient @ height h
 = $2.01 \cdot \left(\frac{Z}{Z_g} \right)^{2/\alpha}$ for $15 \text{ ft} \leq Z \leq Z_g$ (Table 28.3-1)
 = $2.01 \cdot \left(\frac{15}{Z_g} \right)^{2/\alpha}$ for $Z < 15 \text{ ft}$
 = 0.70

K_{zt} = Topographic factor (Figure 26.8-1)
 = $(1 + K_1 \cdot K_2 \cdot K_3)^2$

Topography = None

K_{zt} @ h = 1.00

K_d = Wind directionality factor (Table 26.6-1)

= 0.85

qh = 44.06 (psf)

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Internal Pressure Coefficient, GCpi, Table 26.11-1

Enclosure Classification	GCpi+	GCpi-	Ri	GCpi+	GCpi-
Enclosed Buildings	0.18	-0.18	1.00	0.18	-0.18

External Pressure Coefficient, GCpf, Figure 28.4-1 (Load Case A)

Building Surface								
Roof Angle	1	2	3	4	1E	2E	3E	4E
9.76 deg.	0.44	-0.69	-0.40	-0.33	0.67	-1.07	-0.58	-0.50

Design Wind Pressure, p, (psf) Equation 28.4-1 (Load Case A)

Building Surface	Cp	qh (psf)	GCpi +	GCpi -	p+ (psf)	p- (psf)
1	0.44	44.06	0.18	-0.18	11.51	27.37
2	-0.69	44.06	0.18	-0.18	-38.33	-22.47
3	-0.40	44.06	0.18	-0.18	-25.77	-9.91
4	-0.33	44.06	0.18	-0.18	-22.66	-6.80
1E	0.67	44.06	0.18	-0.18	21.60	37.46
2E	-1.07	44.06	0.18	-0.18	-55.07	-39.21
3E	-0.58	44.06	0.18	-0.18	-33.52	-17.66
4E	-0.50	44.06	0.18	-0.18	-29.81	-13.95

p+ uses GCpi+ p- uses GCpi-

Design Wind Pressure for Overhang, p, Section 28.4.3. (Load Case A)

The design equation has been modified to $qh - [(GCpf) - (\text{Underside GCp})]$ for overhang pressures;

0.70 is used for Underside GCp.

Roof Zone	2	2E
Pressure (psf)	-61.24	-77.98

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External Pressure Coefficient, GCpf, Figure 28.4-1 (Load Case B)

Building Surface												
Roof Angle	1	2	3	4	5	6	1E	2E	3E	4E	5E	6E
9.76 deg.	-0.45	-0.69	-0.37	-0.45	0.40	-0.29	-0.48	-1.07	-0.53	-0.48	0.61	-0.43

Design Wind Pressure, p, (psf) Equation 28.4-1 (Load Case B)

Building Surface	Cp	qh (psf)	GCpi +	GCpi -	p+ (psf)	p- (psf)
1	-0.45	44.06	0.18	-0.18	-27.76	-11.90
2	-0.69	44.06	0.18	-0.18	-38.33	-22.47
3	-0.37	44.06	0.18	-0.18	-24.23	-8.37
4	-0.45	44.06	0.18	-0.18	-27.76	-11.90
5	0.40	44.06	0.18	-0.18	9.69	25.55
6	-0.29	44.06	0.18	-0.18	-20.71	-4.85
1E	-0.48	44.06	0.18	-0.18	-29.08	-13.22
2E	-1.07	44.06	0.18	-0.18	-55.07	-39.21
3E	-0.53	44.06	0.18	-0.18	-31.28	-15.42
4E	-0.48	44.06	0.18	-0.18	-29.08	-13.22
5E	0.61	44.06	0.18	-0.18	18.94	34.81
6E	-0.43	44.06	0.18	-0.18	-26.88	-11.01

p+ uses GCpi+ p- uses GCpi-

Design Wind Pressure for Overhang, p, Section 28.4.3. (Load Case B)

The design equation has been modified to $qh \cdot [(GCpf) - (\text{Underside GCp})]$ for overhang pressures;

0.70 is used for Underside GCp.

Roof Zone	2	2E
Pressure (psf)	-61.24	-77.98